



**Queensberry**  
**DESIGN LIMITED**  
RESIDENTIAL AND COMMERCIAL DESIGN CONSULTANTS

**Strata and Thirteen Group**

**Land at Main Avenue, Cowlersley, Huddersfield**

**FLOOD RISK ASSESSMENT AND DRAINAGE STRATEGY**

September 2024

## ISSUE SHEET

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P01	First Issue		30.09.24
P02	Layout and drainage strategy drawing updated to current site layout		09.10.24
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This document has been prepared solely as a Flood Risk Assessment for Strata and Thirteen Group, Queensberry Design Ltd accepts no responsibility or liability for any use that is made of this document other than by the Client for which it was originally commissioned and prepared.

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## 1. Introduction

- 1.1 Queensberry Design Ltd has been commissioned by Thirteen and Strata to undertake a Flood Risk Assessment (FRA) for a proposed residential development at Main Avenue, Cowlersley, Huddersfield.
- 1.2 This FRA has been produced to demonstrate how flood risk from all sources of flooding, and flood risk to others from the development will be managed, to satisfy the requirements, set out in '*National Planning Policy Framework, and Technical Guidance to the National Planning Policy Framework*'. A full assessment of the flood risk to the site and consideration of the surface water management as a result of the development is to be considered in this investigation.
- 1.3 Consultation has been undertaken with Yorkshire Water (YW), Environment Agency (EA) and Kirklees Lead Local Flood Authority (LLFA) including inspection of their Strategic Flood Risk Assessment (SFRA). Data has also been gathered from several other sources including aerial photographs, Ordnance Survey (OS), the British Geological Society (BGS), National Soil Resources Institute (NSRI), Sewerage Sector Guidance (SSG), SuDS Manual (C753) and anecdotal evidence from the internet.

## 2. Site Description

- 2.1 The application boundary is 2.12 ha with a developed area of 1.55 ha and is located 2km west of Huddersfield town centre, with the Cowlersley area.
- 2.2 The site is irregularly shaped and is predominantly greenfield, the site is accessed from Main Avenue and Windsor Road. Garage buildings and associated hard paved access are located at the northern end of the site, large parts of the site are heavily vegetated/overgrown.
- 2.3 Boundary features around the application site are residential dwellings to the east, west, and part of the northern boundary, the southern boundary is open undeveloped land, Woodside Green Primary School forms the majority of the northern boundary.
- 2.4 The location of the development is shown in Figure 1a, and Figure 1b.

### Site Levels

- 2.5 A topographical survey was carried out during May 2024 and can be viewed in Appendix 1. Site levels generally fall from the north-west towards the south-east. The existing topography is steep with gradients up to 1 in 4.
- 2.6 Existing levels fall centrally forming a channel through the site, falling from west to east.
- 2.7 Appendix 2 provides a coloured plan showing how the existing topography falls.

### Hydrogeology

- 2.8 Bedrock underlain the site is Millstone Grit (sandstone, mudstone and siltstone), a secondary A aquifer. The site is not located in a source protection zone.

### Hydrology

- 2.9 The nearest main river is River Colne located 0.5km north of the site, the River Colne flows easterly through Huddersfield and is a tributary of the River Calder. Immediately north of River Colne is the Huddersfield Narrow Canal which follows a similar route as the River Colne to the River Calder.
- 2.10 The scheme is in the River Colne catchment and the site will not impact the main river network.
- 2.11 Information from Kirklees Council shows a culvert at the eastern edge of the site, the recorded culvert runs through the rear of the dwellings fronting Warneford Road. The culvert then discharged to a normal watercourse at the junction of Warneford Road and Manse Drive, an open channel then runs through the rear of dwellings fronting Avison Road.

- 2.12 Photographic information supplied by residents shows two large gully grates outside the site's eastern boundary, on the boundary of 66 Warneford Road, the area around these gully grates has collapsed allowing run-off to bypass the grates into the network below.
- 2.13 Drainage investigation has recorded a 225mm diameter pipe within the site boundary, this pipe has further connections which are all capped. This pipe connects to a chamber which is below the gully grates, some flow is recorded which is expected to be infiltrated surface water run-off and groundwater.
- 2.14 Based on the information available the culvert starts at the eastern edge of the development adjacent 66 Warneford Road.
- 2.15 The location of the culvert opening is directly on an existing overland flow route, discussed further in this assessment.
- 2.16 A stone culvert is located adjacent to a dry stone wall on the hillside to the south of the development site. During the site walkover, trickling water was observed within the culvert, although a ditch located further downslope was found to be dry at the time of inspection.
- 2.17 Consultation with the Lead Local Flood Authority (LLFA) and trial trenching have so far been unable to locate the outfall of the culvert. However, based on the local topography and site levels, it is anticipated that runoff from this feature is directed into the culvert to the rear of Warneford Road.
- 2.18 A saturated area was observed adjacent to the existing hardstanding. This area is densely vegetated with reed and wetland-type species, suggesting a persistently moist environment. Trial trenching in this location uncovered a subsurface void at a shallow depth, with continued ground saturation. It is therefore assumed this may represent a former culverted watercourse or a natural spring.
- 2.19 Consultation with the LLFA and a review of historic mapping have identified the likely presence of a well associated with the former Jubilee Properties. However, its exact location, dimensions, and depth remain unknown. If encountered during construction, the well should be decommissioned in accordance with the Environment Agency's guidance document: "Good Practice for Decommissioning Redundant Boreholes and Wells" (EA, 2012).
- 2.20 Extensive intrusive investigations have been carried out across the site. Aside from the features noted above, no evidence of wet ground or additional drainage infrastructure has been identified. The results of the investigations are included in Appendix 8.
- 2.21 It has been agreed further investigation of the culvert within the rear gardens of Warneford Road is not required, as the proposed run-off will not enter the culvert.

#### **Existing Drainage Infrastructure**

- 2.22 Existing public sewerage infrastructure within the site's vicinity is described below. The existing sewer records provided by Yorkshire Water can be found in Appendix 4.
- 2.23 Sewer records show an existing 450mm diameter combined sewer crossing the site from Main Avenue flowing in an eastern direction leaving the site at the eastern boundary to the rear of the existing dwellings on Warneford Road.
- 2.24 Two combined sewers are recorded entering the site from the northern boundary from Windsor Road and Jubilee Lane, these sewers connect into the 450mm diameter sewer.
- 2.25 Records also show an existing 225mm diameter sewer passing along the school boundary connecting into the 450mm diameter sewer.



2.25 Figure 1a – Site Location, Ordnance Survey



2.26 Figure 1b - Detailed Site Location

### **3. Strategic Flood Risk Documentation**

#### **Calder Catchment Strategic Flood Risk Assessment Volume 1 (2016)**

- 3.1 The Level 1 Strategic Flood Risk Assessment (SFRA) has been produced for Kirklees Council in April 2016 by JBA Consulting. The report considers the risk of flooding within the river Calder catchment as well as overview of risk from, groundwater and surface water runoff.

#### **Calder Catchment Strategic Flood Risk Assessment Volume 2 (2016)**

- 3.2 The Level 2 Strategic Flood Risk Assessment (SFRA) produced in July 2016 by JBA Consulting involves a more detailed (local) investigation. Volume 2 covers National Planning Policy and flood risk policy while assessing actual flood risk, flood risk within key communities and conclusions and recommended for further work.
- 3.3 The volume 2 assessment mapping highlights surface water flood risk crossing the site as shown in appendix 6.
- 3.4 Information available within the SFRA mapping confirms the site is outside of a critical drainage area and has a less the 25% chance of groundwater emergence.

### **4. Flood Risk Assessment**

- 4.1 When determining any planning applications, local planning authorities should ensure that flood risk is not increased elsewhere. Where appropriate, applications should be supported by a site-specific flood-risk assessment.
- 4.2 A site-specific flood risk assessment should be provided for all development in Flood Zones 2 and 3. In Flood Zone 1, an assessment should accompany all proposals involving: sites of 1 hectare or more; land which has been identified by the Environment Agency as having critical drainage problems; land identified in a strategic flood risk assessment as being at increased flood risk in future; or land that may be subject to other sources of flooding, where its development would introduce a more vulnerable use.
- 4.3 The Planning Practice Guidance was published in March 2014. The new Guidance is intended to reflect and support (but not replace) the National Planning Policy Framework (the NPPF) published in February 2019. On 25<sup>th</sup> August 2022, the Ministry of Housing, Communities & Local Government, released an updated version of the National Planning Policy Framework (NPPF).
- 4.4 In respect of flood risk, the NPPF was amended to clarify that all plans should apply a sequential, risk-based approach to the location of development, taking into account 'all sources of flood risk' and the current and future impacts of climate change.
- 4.5 If it is not possible for development to be located in zones with a lower risk of flooding, an application for the development should be considered having regard to the vulnerability of the site and development proposed. A new 'Floor Risk Vulnerability Classification' has been added to the NPPF that categorises those types of development particularly vulnerable to flood risk.

### Sources of Flooding

- 4.6 In accordance with NPPF all forms of flood risk need to be considered in relation to any development. Flood risk has been assessed from the following sources: tidal and fluvial, surface water and flooding from the land, groundwater, sewer flooding and artificial sources (i.e., canals, reservoirs etc.)

### Tidal and Fluvial Flooding

- 4.7 The Environment Agency 'Flood Map for Planning' map in figure 4.1, indicates the site is located entirely within Flood Zone 1 and so is considered to have the lowest probability of flooding from rivers and the sea, of 1 in 1000 in any one year (0.1%).



4.8 *Figure 4.1 – Environment Agency Flooding from Rivers and Sea Flood Map*

### Surface Water Flooding

- 4.9 Flooding from overland flow can become a risk to any development if flooding occurs at a higher level than the development site.
- 4.10 The Environment Agency national Risk of Surface Water Flooding (RoFSW) data set map shows the majority of the site is at a very low risk.
- 4.11 Very low risk refers to land having less than a 1 in 1000 annual exceedance probability of flooding. Low risk refers to land having between a 1 in 1000 and 1 in 100 annual exceedance probability of flooding (0.1% - 1% AEP). Medium risk refers to land having 1 in 100 and 1 in 30 annual probabilities (1% - 3.33% AEP). High risk refers to land having a greater than 1 in 30 annual exceedance probability of flooding (>3.33% AEP).
- 4.12 The RoFSW mapping shows a surface water flow route entering the development boundary where the Main Avenue carriageway ends, this flow route originates further west of the development, with Main Avenue collecting the run-off and channelling it into the development.
- 4.13 Once flows enter the development run-off is channelised by the existing site levels towards the existing properties on Warneford Road, ref appendix 2 for existing site falls diagram.
- 4.14 The risk probability and extent of flood risk then increase on the eastern boundary, it is anticipated this increase is due to the culverted watercourse discussed in section 2 not having the capacity to collect the run-off.
- 4.15 Mapping also shows a flow route entering the development's northern boundary from Windsor Road, as the flow from Main Avenue, Windsor Road is channelling exceedance run-off into the development, this run-off poses a lesser risk as it turns and follows lower-lying levels to the open space north-east of the site.
- 4.16 Although unrecorded the development will be subject to a significant amount of run-off from the land beyond the southern boundary, this run-off will also contribute to the surface water flooding entering the site from Main Avenue.
- 4.17 The development will provide a minor reduction in the cumulative run-off flowing towards the culverted watercourse, flooding at Warneford Road and adjacent open space, by collecting and attenuating run-off.
- 4.18 The design of the development must ensure the surface water flow routes entering the site are managed in a way that the site levels collect and divert the run-off to its existing location. Flow routing must pass through an adopted carriageway or managed shared drives to ensure run-off is managed for the development lifetime.
- 4.19 All new dwellings shall have 300mm freeboard from the flow route to ensure exceedance does not raise above a finished floor level – level design and exceedance routing can be viewed in appendix 9.
- 4.20 The proposed new dwellings backing onto the southern boundary will be intersecting surface water run-off from the land south of the site, and mitigation is required.
- 4.21 Due to the significant level changes across the site, a retaining wall will be required to form the southern boundary. To collect and divert the overland flow, the retaining wall is proposed to include a parapet. The parapet will stop the run-off from entering the gardens of the proposed dwellings and potentially flooding the dwellings.
- 4.22 Levels and the retaining wall design must direct the existing run-off to the shared drive serving plots 49 - 52 to allow the run-off to escape down the drive to its current flow route as the surface water mapping.
- 4.23 Details within Appendix 9 provide the mitigation principle.

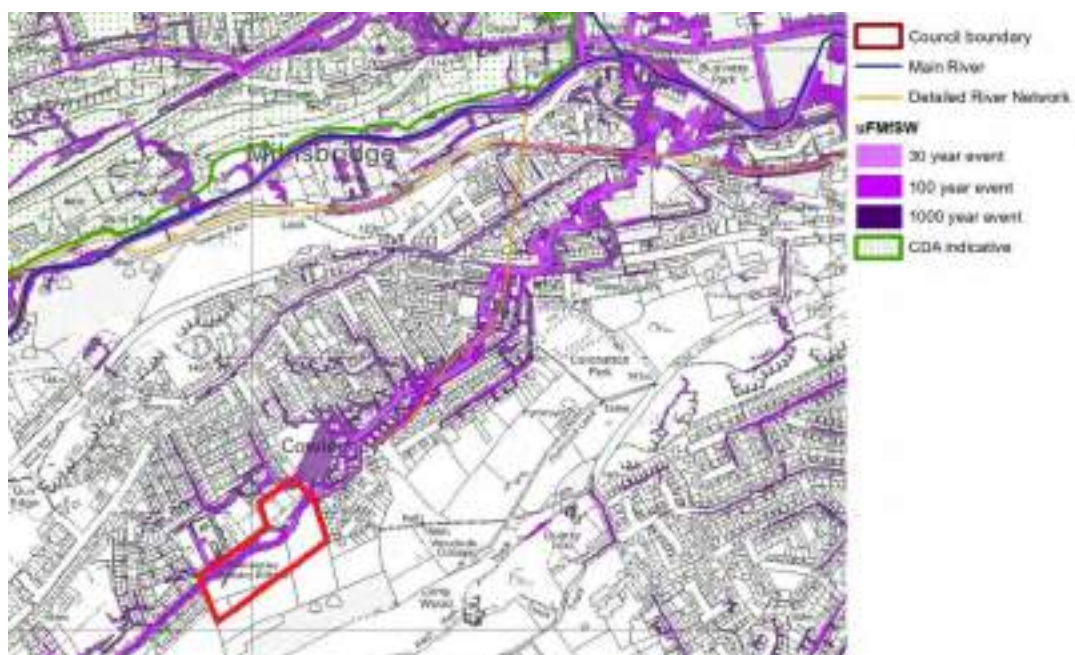
4.24 Based on the available information flood risk from this source is considered HIGH.



4.25 Figure 4.2 – Environmental Agency Surface Water Flood Risk Map



4.26 Figure 4.3 – Environment Agency Surface Water – flood depth



4.27 Figure 4.4 – Strategic Flood Risk Assessment Surface Water Flood Risk Map

### **Groundwater**

- 4.28 Groundwater flooding is caused by water originating from beneath the ground surface from permeable strata through a natural process, usually after periods of higher-than-average rainfall.
- 4.29 The SRRA identifies the site as having a 25% risk of groundwater emergence.
- 4.30 Groundwater has been recorded during the site investigation, with the groundwater being shallower in low-lying areas.
- 4.31 Based on the information from the site investigation groundwater poses a low risk to the finished development.
- 4.32 Based on the available information significant flood risk from this source is considered LOW.

### **Sewer Flooding**

- 4.33 No known sewer flood events are known, given that the scheme is to divert existing drainage to modern standards, and the new surface water network will be designed following this document and current best practice, possible future sewer flooding is limited.
- 4.34 Kirklees Council have witnessed flooding from the gullies at the end of Main Avenue and will be investigating this. If a flood event occurs from these gullies run-off will pass through the new road network.
- 4.35 Based on the available information flood risk from this source is considered LOW.

### **Land Drainage**

- 4.36 If any land drainage discovered during excavations on site, it is recommended that the drain is repaired or diverted. Should this not be possible due to layout constraints, then it is recommended that the land drain is further investigated by the development engineer, to determine if the drain is still required post development.
- 4.37 Based on the available information flood risk from this source is considered LOW.

### **Artificial Sources**

- 4.38 Environment Agency data and mapping indicates the site is not at risk of reservoir flooding.
- 4.39 Based on the available information flood risk from this source is considered LOW.

## 5. Summary of Existing Flood Risk

5.1 Table 5.1 below summarises the sources of possible flooding which have been investigated.

Table 5.1 – Summary of Flood Risk		
Flood Risk Source	Current Risk Level	Mitigation Requirement
Tidal & Fluvial Flooding	LOW	Not required
Groundwater	LOW	Not required
Sewer Flooding	LOW	Not required
Overland Flow	HIGH	Dwellings to be set 300mm higher than existing flow routes Existing flow routes are to be maintained along the southern boundary Recorded flow routes to be diverted through the site via the road network
Land Drainage	LOW	Not required
Artificial Sources	LOW	Not required

## 6. Existing Drainage Regime

6.1 The site is a mixture of permeable and impermeable surfaces, however, given the small amount of impermeable surfaces, the site is being assessed as a greenfield site.

6.2 Micro drainage rural run-off calculator (ICP SuDS for small catchments) has been used to calculate the existing greenfield run-off rates from the developed site, the results can be viewed in Table 6.1 and Appendix 7

Table 6.1 – Greenfield Run-off	
Return Period	Discharge
1 Year	7.2 l/sec
QBAR	8.3 l/sec
30 Year	14.6 l/sec
100 Year	17.7 l/sec

## 7. Proposed Development

- 7.1 Strata and Thirteen Group proposes to develop the site for residential use comprising 57 dwellings with associated landscaping, access and infrastructure works.
- 7.2 A copy of the proposed site layout can be viewed in Appendix 3.

### Planning Context

- 7.3 The EA flood maps for the region show that the development sits within Flood Zone 1, which has a low probability of flooding 1 in 1000 in any one year (0.1%). This is illustrated in Table 7.1.
- 7.4 The proposed development will comprise residential dwellings. Therefore, in accordance with NPPF Table 7.2, the development is classified as ‘more vulnerable’.
- 7.5 Thus, given that site is situated in Flood Zone 1 and the vulnerability classification in accordance with the NPPF compatibility matrix in Table 7.3, the scheme is classified as appropriate for development.

<b>Flood Zone</b>	<b>Probability</b>	<b>Explanation</b>
<b>Flood Zone 1</b>	Low Probability	This zone comprises land assessed as having a less than 1 in 1,000 annual probability of river or sea flooding (<0.1%).
<b>Flood Zone 2</b>	Medium Probability	This zone comprises land assessed as having between a 1 in 100 and 1 in 1,000 annual probability of river flooding (1% – 0.1%), or between a 1 in 200 and 1 in 1,000 annual probability of sea flooding (0.5% – 0.1%) in any year.
<b>Flood Zone 3a</b>	High Probability	This zone comprises land assessed as having a 1 in 100 or greater annual probability of river flooding (>1%), or a 1 in 200 or greater annual probability of flooding from the sea (>0.5%) in any year.
<b>Flood Zone 3b</b>	Functional Floodplain	This zone comprises land where water has to flow or be stored in times of flood

Table 7.2 Flood Risk Vulnerability	
Category	Explanation
<b>Essential Infrastructure</b>	<ul style="list-style-type: none"> <li>• Essential transport infrastructure (including mass evacuation routes) which has to cross the area at risk.</li> <li>• Essential utility infrastructure which has to be located in a flood risk area for operational reasons.</li> <li>• Wind turbines and Solar farms.</li> </ul>
<b>Highly Vulnerable</b>	<ul style="list-style-type: none"> <li>• Police stations, Ambulance stations and Fire stations and Command Centres and telecommunications installations required to be operational during flooding.</li> <li>• Emergency dispersal points.</li> <li>• Basement dwellings.</li> <li>• Caravans, mobile homes and park homes intended for permanent residential use.</li> <li>• Installations requiring hazardous substances consent.</li> </ul>
<b>More Vulnerable</b>	<ul style="list-style-type: none"> <li>• Hospitals.</li> <li>• Residential institutions such as residential care homes, children’s homes, social services homes, prisons and hostels.</li> <li>• Buildings used for: dwelling houses; student halls of residence; drinking establishments; nightclubs; and hotels.</li> <li>• Non-residential uses for health services, nurseries and educational establishments.</li> <li>• Landfill and sites used for waste management facilities for hazardous waste.</li> <li>• Sites used for holiday or short-let caravans and camping, subject to a specific warning and evacuation plan.</li> </ul>
<b>Less Vulnerable</b>	<ul style="list-style-type: none"> <li>• Police, ambulance and fire stations which are not required to be operational during flooding.</li> <li>• Buildings used for: shops; financial, professional and other services; restaurants and cafes; hot food takeaways; offices; general industry; storage and distribution; non-residential institutions not included in ‘more vulnerable’; and assembly and leisure.</li> <li>• Land and buildings used for agriculture and forestry.</li> <li>• Waste treatment (except landfill and hazardous waste facilities).</li> <li>• Minerals working and processing (except for sand and gravel working).</li> <li>• Water treatment plants.</li> <li>• Sewage treatment plants (if adequate pollution control measures are in place).</li> <li>• Car Parks</li> </ul>
<b>Water-compatible development</b>	<ul style="list-style-type: none"> <li>• Flood control infrastructure</li> <li>• Water transmission infrastructure and pumping stations.</li> <li>• Sewage transmission infrastructure and pumping stations.</li> <li>• Sand and gravel workings.</li> <li>• Docks, marinas and wharves.</li> <li>• Navigation facilities.</li> <li>• MOD defence installations.</li> <li>• Ship building, repairing and dismantling, dockside fish processing and refrigeration and compatible activities requiring a waterside location.</li> <li>• Water-based recreation (excluding sleeping accommodation).</li> <li>• Lifeguard and coastguard stations.</li> <li>• Amenity open space, nature conservation and biodiversity, outdoor sports and recreation and essential facilities such as changing rooms.</li> <li>• Essential ancillary sleeping or residential accommodation for staff required by uses in this category, subject to a specific warning and evacuation plan.</li> </ul>

Table 7.3 Flood Risk Vulnerability Classification					
Flood Zone	Essential Infrastructure	Highly Vulnerable	More Vulnerable	Less Vulnerable	Water Compatible
<b>Zone 1</b>	Appropriate	Appropriate	Appropriate	Appropriate	Appropriate
<b>Zone 2</b>	Appropriate	Exception Test required	Appropriate	Appropriate	Appropriate
<b>Zone 3a</b>	Exception Test required	Not Permitted	Exception Test required	Appropriate	Appropriate
<b>Zone 3b</b>	Exception Test required	Not Permitted	Not Permitted	Not Permitted	Appropriate

## **8. Management of Surface Water**

### **Possible Drainage Solutions**

- 8.1 An assessment of possible drainage options has been undertaken in accordance with Building Regulations H3 Section 3 and NPPF. The disposal of surface water has been considered in the following order of priority.

*-An adequate soakaway or some other infiltration system; or, where not reasonably practicable,*

*-A watercourse, or where not reasonably practicable,*

*-A sewer*

### **Infiltration**

- 8.2 In-situ testing carried out during the site investigation has determined that the use of infiltration will not be possible.

### **Discharge to a Watercourse**

- 8.3 As this assessment, a culverted watercourse is located to the rear of the existing dwellings fronting Warneford Road, the watercourse is recorded on Local Authority records.

- 8.4 The culvert is fed by over land flow as shown on the surface water flood mapping. Investigation has shown that a 225 diameter pipe enters the development which feeds into the culverted watercourse, survey has shown this pipe to be 400mm deep, and is capped in all directions.

- 8.5 Given existing greenfield run-off from the development contributes to the culverts catchment, discharge to this watercourse is the preferred method of surface water disposal.

- 8.6 Discharge to this watercourse would follow the existing greenfield QBAR discharge rate of 8.3 litres/sec.

- 8.7 An assessment of surface water storage requirements, development layout, and outfall level has concluded a gravity connection to the 225 diameter pipe will not be possible, without pumping of flow.

- 8.8 A gravity connection to the culverted watercourse downstream may be possible (subject to further survey) however, this will require agreement from several third-party landowners.

### **Discharge to Public Sewers**

- 8.9 Due to the issue with achieving a surface water outfall to the culverted watercourse, discharge to the existing public sewers will be necessary.

- 8.10 Yorkshire Water has been contacted through the pre-development enquiry process and has confirmed an allowable discharge of 3.5 litres/sec into the existing 450 diameter combined sewer.

- 8.11 This sewer is within the development boundary and is at a suitable depth for a gravity connection.

## 9. Preferred Drainage Solution

### Storm Drainage

- 9.1 The preferred drainage solution will involve the discharge of site surface water flows to the combined sewerage within the site boundary. The proposed drainage strategy and calculations can be viewed in Appendix 9.

### Storm Drainage

- 9.2 The allowable discharge rate from Yorkshire Water is 3.5 litres/second which is a 58% reduction of the existing QBAR discharge rate.
- 9.3 Surface water modelling has been undertaken to assess up to 45% climate with no inclusion of urban creep.
- 9.4 Attenuation will be provided by means of a pre-cast attenuation tank located within the green space on the development's eastern boundary and flows will be restricted using a vortex flow control device in accordance with Yorkshire Water adoption requirements. The minimum orifice diameter shall be 75mm.
- 9.5 The attenuation is to be placed allowing suitable standoff from the adoptable highway and neighbouring boundary.
- 9.6 Given that the outfall is an existing sewer owned by Yorkshire Water, no detailed considerations are required; the connection to the sewer must be made at soffit level or higher to mitigate possible surcharge from the existing sewer.
- 9.7 All new adoptable standard surface water drainage is to be designed in accordance with 'SSG' and to ensure that no flooding occurs during the critical 1 in 30-year storm event.

### Foul Drainage

- 9.8 Foul drainage will connect into diverted sewers under Section 185 of the Water Industry Act or new foul drains under Section 104 of the Water Industry Act.
- 9.9 Flows will ultimately connect into the existing 450mm dia combined sewer at the east of the development.
- 9.10 All new adoptable foul sewerage is to be designed in accordance with 'SSG'.

### Land Drainage and Surface Water Flooding

- 9.11 Due to the surface water constraints and flood risk identified on site, a number of mitigation interventions are required to manage existing overland flows and reduce flood risk to the proposed dwellings.
- 9.12 As discussed in Section 4, the development is at risk from surface water flooding, as shown in the Environment Agency flood mapping. This risk is primarily from overland flow originating on the hillside to the south of the site, conveyed via natural ground contours, existing culverts, and informal channels.
- 9.13 Floodwater and runoff from the southern hillside will be directed along the proposed road network, flowing west to east toward the existing outfall. Runoff will be intercepted by a parapet feature incorporated into the retaining wall, which will divert flows toward a proposed stepped access route, then down a private driveway, ultimately rejoining the natural discharge route.
- 9.14 To further reduce flood risk, a land drainage network is proposed. This system will manage runoff from both the hillside culvert and the suspected spring or former culvert identified in the western part of the site.

- 9.15 To manage flows from the hillside culvert:
- A headwall will be installed at the base of the ditch or culvert pipe (whichever is lower in elevation).
  - A headwall is preferred over a direct connection to the existing culvert to ensure the wider upstream catchment (as shown on Drawing 2153-QD-XX-HD-DR-C-80-01 in Appendix 9) is captured effectively.
  - This design also ensures future visibility and maintenance access, reducing the risk of blockage in vegetated areas.
- 9.16 From the headwall, a 225mm diameter pipe will be installed:
- Passing through the rear gardens of Plots 42 and 43,
  - Entering the verge of the proposed carriageway,
  - Connecting ultimately into the existing downstream culvert.
- 9.17 As Plot 43 lies downslope of the proposed drain therefore:
- A 225mm high coping is proposed along the retaining wall that runs parallel to the pipe and the plot.
  - This feature is designed to contain exceedance flows in the event of surcharge or blockage and direct them safely toward the road fronting Plot 43, rather than toward vulnerable dwellings.
- 9.18 A spring or former culvert was observed adjacent to the existing car park in the western area of the site. Further trial pitting and trenching have not identified any active or continuous drainage feature in this location.
- 9.19 To manage any intermittent or unknown flows, a 225mm diameter land drain will be installed in the carriageway verge adjacent to this area.
- 9.20 Given the possibility of encountering additional culverts or springs, it is proposed that the land drain be extended along the full length of the carriageway verge, particularly around Plots 27–28 and the shared driveway serving Plots 29–32, where excavation works may reveal previously unrecorded drainage features.
- 9.21 An additional inspection chamber may be required at the location of SC7 within the carriageway. The final requirement will be confirmed following vegetation clearance and site level reduction.

**10. Conclusion**

**Flood Risk**

- 10.1 The flood risk assessment and drainage strategy has been prepared in accordance with the NPPF, Flood Risk and Coastal Change Planning Practice Guidance. The management of the surface water flows has also been considered in accordance with Building Regulations H3 Section 3.
- 10.2 The proposed development is classified as 'more vulnerable' and is located within Flood Zone 1 according to the SFRA and Flood Maps for Planning, therefore the development is suitable within this flood zone in accordance with NPPF.
- 10.3 The development is at risk of surface water flooding, employment of the mitigation measures stated in this report will ensure that the development will be safe and suitable in this location.
- 10.4 Flood risk from all sources have been considered and with mitigation where necessary, it has been established that these sources do not pose a residual risk to the development.

**Storm Drainage**

- 10.5 Surface water runoff will discharge to the existing combined sewerage to a rate of 3.5 litres/sec for all storm return periods.
- 10.6 Exceedance flows above the restricted rate of 3.5 litres/sec will be attenuated on-site via underground attenuation.
- 10.7 All new adoptable standard surface water drainage is to be designed in accordance with 'SSG' and to ensure that no flooding occurs during the critical 1 in 30-year storm event. A 45% increase in rainfall due to climate change has been considered.

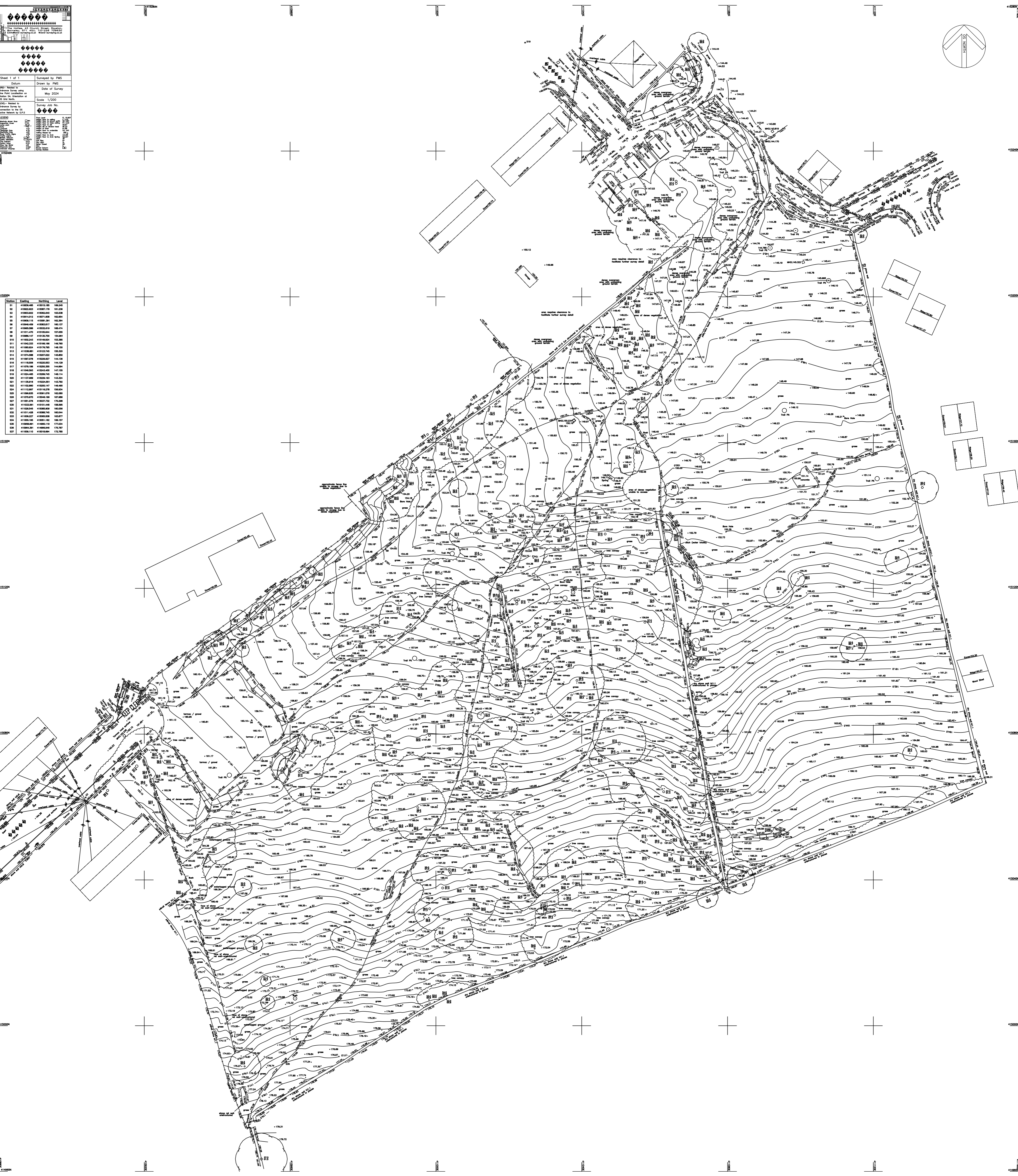
**Foul Drainage**

- 10.8 It is proposed to discharge foul flows into either diverted or new sewers.
- 10.9 All new adoptable foul sewerage is to be designed in accordance with 'SSG'.

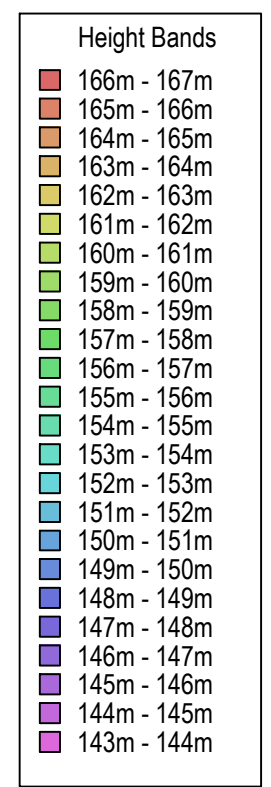
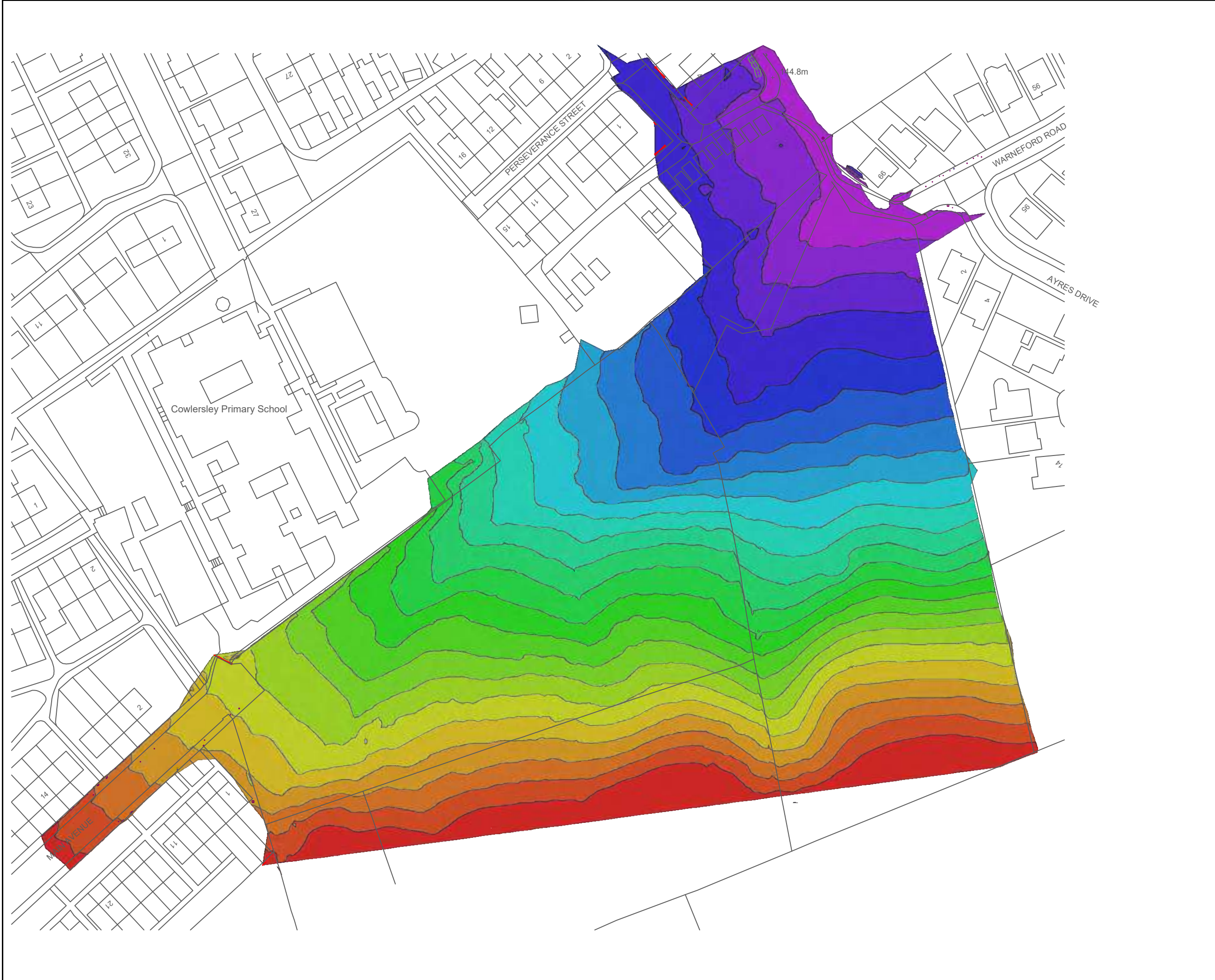
## Appendix 1 - Topographical Survey

Surveyed by PMS  
 Drawn by PMS  
 Date of Survey  
 May 2024  
 Scale 1/200  
 Surveyed on No.  
 10/20/2024  
 Stationed to No. 12.5

Station	Existing	Horizontal	Level
01	100000.00	100000.00	100.00
02	100000.00	100000.00	100.00
03	100000.00	100000.00	100.00
04	100000.00	100000.00	100.00
05	100000.00	100000.00	100.00
06	100000.00	100000.00	100.00
07	100000.00	100000.00	100.00
08	100000.00	100000.00	100.00
09	100000.00	100000.00	100.00
10	100000.00	100000.00	100.00
11	100000.00	100000.00	100.00
12	100000.00	100000.00	100.00
13	100000.00	100000.00	100.00
14	100000.00	100000.00	100.00
15	100000.00	100000.00	100.00
16	100000.00	100000.00	100.00
17	100000.00	100000.00	100.00
18	100000.00	100000.00	100.00
19	100000.00	100000.00	100.00
20	100000.00	100000.00	100.00
21	100000.00	100000.00	100.00
22	100000.00	100000.00	100.00
23	100000.00	100000.00	100.00
24	100000.00	100000.00	100.00
25	100000.00	100000.00	100.00
26	100000.00	100000.00	100.00
27	100000.00	100000.00	100.00
28	100000.00	100000.00	100.00
29	100000.00	100000.00	100.00
30	100000.00	100000.00	100.00
31	100000.00	100000.00	100.00
32	100000.00	100000.00	100.00
33	100000.00	100000.00	100.00
34	100000.00	100000.00	100.00
35	100000.00	100000.00	100.00
36	100000.00	100000.00	100.00
37	100000.00	100000.00	100.00
38	100000.00	100000.00	100.00
39	100000.00	100000.00	100.00
40	100000.00	100000.00	100.00
41	100000.00	100000.00	100.00
42	100000.00	100000.00	100.00
43	100000.00	100000.00	100.00
44	100000.00	100000.00	100.00
45	100000.00	100000.00	100.00
46	100000.00	100000.00	100.00
47	100000.00	100000.00	100.00
48	100000.00	100000.00	100.00
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91	100000.00	100000.00	100.00
92	100000.00	100000.00	100.00
93	100000.00	100000.00	100.00
94	100000.00	100000.00	100.00
95	100000.00	100000.00	100.00
96	100000.00	100000.00	100.00
97	100000.00	100000.00	100.00
98	100000.00	100000.00	100.00
99	100000.00	100000.00	100.00
100	100000.00	100000.00	100.00



## Appendix 2 – Site Fall Diagram



Rev.	Date	Revision Details	Drawn	Checked

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 LEEDS, LS25 1WB  
[www.queensberrydesign.co.uk](http://www.queensberrydesign.co.uk)

Client  
**STRATA AND THIRTEEN GROUP**

Project  
**MAIN AVENUE  
 COWLERSLEY  
 HUDDERSFIELD**

Title  
**SITE FALL DIAGRAM**

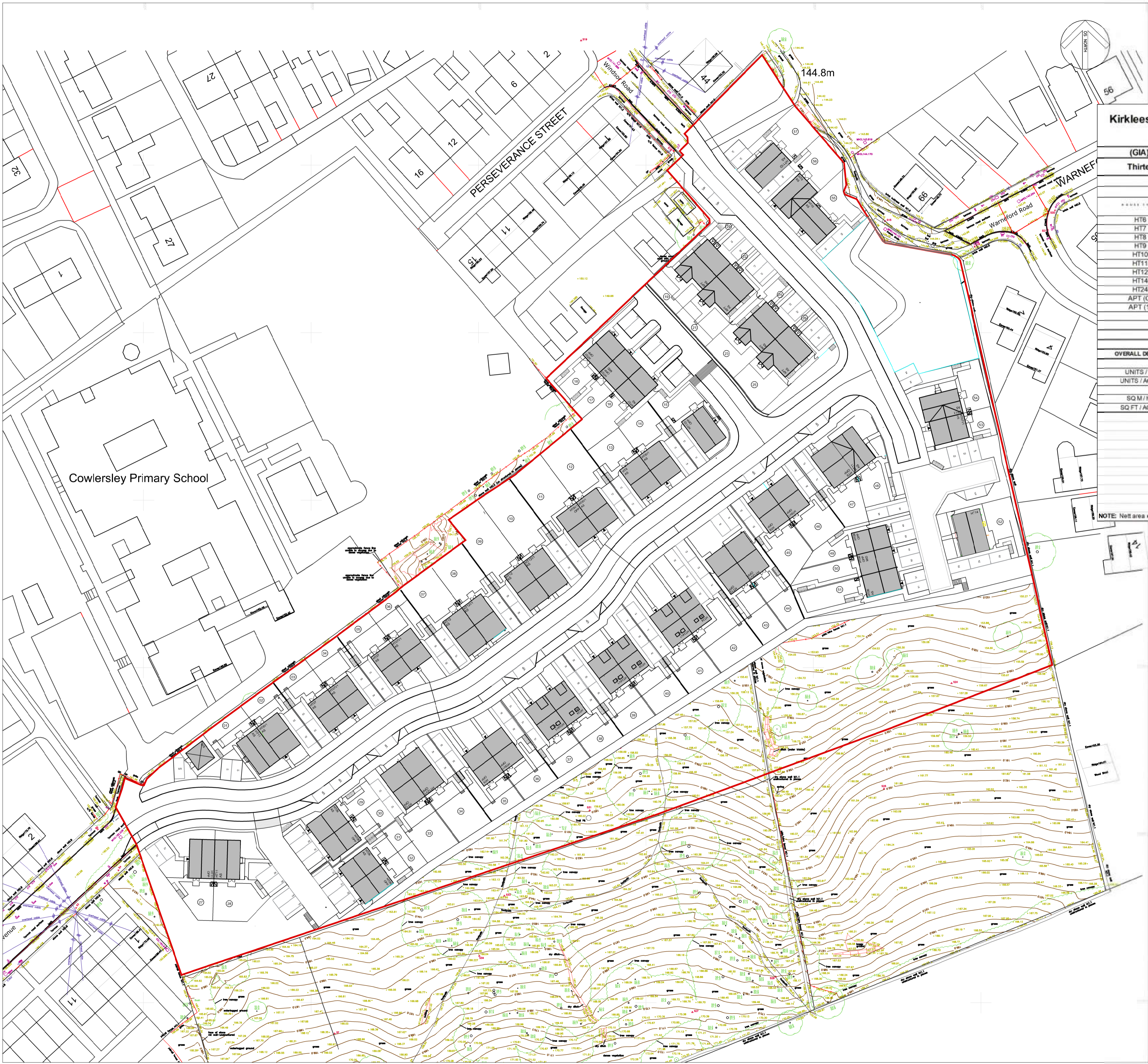
Drawn <b>ND</b>	Checked	Date
Drawing Number		
Drawing Status		Scale <b>1:1000 - A3</b>
		Rev.

## Appendix 3 – Development Layout

DO NOT SCALE  
All dimensions to be checked on site and Architect to be notified of any discrepancies prior to commencement

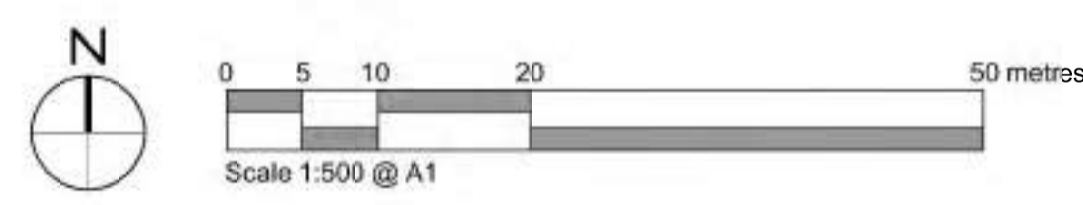
DESIGNERS RISK ASSESSMENT  
Construction (Design and Management) Regulations 2015  
RESIDUAL RISKS

REF	DATE	DESCRIPTION
P1	03.10.24	Planning Issue GP
P2	11.10.24	Apartment footprints revised. GP
P3	22.10.24	Substation location revised. GP
P4	23.10.24	Private drive arrangement altered plots 16-18. GP
P5	26.11.24	Altered following client feedback. Coordinated with levels proposals. GP
P6	26.03.25	Raised table altered at the centre of the site. GP
P7	23.05.25	Layout altered to give easement to culvert. GP



Kirklees - Main Avenue										
(GIA)										
Thirteen Group/Strata										
							GROSS SITE AREA	ha	acres	
							NET SITE AREA	1.81	5.24	
HOUSE TYPE	ROOMS	TYPE	UNIT	SIDEWALK	NO	MIX	NO	NO	NO	
HT6	2B3P	CAT M4(2)	HOUSE	2	7	12	784.69	72.9	5493	
HT7	2B4P	CAT M4(2)	HOUSE	2	8	14	877.26	81.5	7018	
HT8	3B4P	CAT M4(1)	HOUSE	2	8	14	928.92	86.3	7431	
HT9	3B5P	CAT M4(1)	HOUSE	2	3	5	1020.42	94.80	3061	
HT10	3B5P	CAT M4(2)	HOUSE	2	1	2	1020.42	94.80	1020	
HT11	3B5P	CAT M4(2)	HOUSE	2	7	12	1020.42	94.80	7143	
HT12	3B5P	CAT M4(2)	HOUSE	2	8	14	1032.26	95.90	8258	
HT14	4B6P	CAT M4(2)	HOUSE	2	1	2	1184.03	110.00	1184	
HT24	4B6P	CAT M4(1)	HOUSE	2.5	6	11	1357.33	126.10	8144	
APT (G)	2B3P	CAT M4(2)	APARTMENT	1	4	7	659.83	61.30	2639	
APT (I)	2B3P	CAT M4(2)	APARTMENT	1	4	7	731.95	68.00	2928	
<b>OVERALL TOTALS</b>							<b>57</b>	<b>100</b>	<b>54320</b>	<b>5047</b>
OVERALL DENSITY				OVERALL MIX				TOTAL		%
UNITS / ha	36.77	UNITS / ACRE	12.75	2 BED		23	40			
SQ M / ha	3256	SQ FT / ACRE	12152	3 BED		27	47			
				4 BED		7	12			
						<b>57</b>	<b>100</b>			
OVERALL MIX APPROVED DOCUMENT M				TOTAL		%				
				CAT M4(1)		17	30			
				CAT M4(2)		40	70			
				CAT M4(3)		0	0			
						<b>57</b>	<b>100</b>			

NOTE: Net area excludes all public open space and associated structural landscaping / buffer planting / half road



PROJECT / CLIENT Kirklees Cluster Sites Main Avenue, Cowlersley	PROJECT NO. N81-3084	DRAWING STATUS Planning	REV	DATE	REVISION DESCRIPTION
DRAWING TITLE Proposed Site Layout	DRAWING NO. 102				
PROJECT LEADER GP	DRAWN BY GP	CHECKED BY IDP	DRAWING REVISION P8		
SCALE 1 to 500 @ A1	DATE 22.10.2024				

idp Architecture Masterplanning Urban Design

## Appendix 4 – Yorkshire Water

**Mr N Dunwoodie**  
**Queensbury Design Ltd**  
**5 The Staithes**  
**NE11 9SN**  
**nick.dunwoodie@queensberrydesign.co.uk**

**Yorkshire Water Services**  
**Developer Services**  
**Pre-Development Team**  
**PO BOX 52**  
**Bradford**  
**BD3 7AY**

**Tel: 0345 120 8482**

**Your Ref:**  
**Our Ref: A000354**

**Email:**  
**technical.sewerage@yorkshirewater.co.uk**

**For telephone enquiries ring:**  
**Chris Roberts on 0345 120 8482**

**5th February 2024**

Dear Mr Dunwoodie,

**Main Aveune, Cowlersley, Huddesfield, HD4 5US – Pre-planning Enquiry V360332**

Thank you for your recent enquiry and remittance. Our official VAT receipt has been sent to you under separate cover. Please find enclosed a complimentary extract from the Statutory Sewer Map which indicates the recorded position of the public sewers. Please note that as of October 2011 and the private to public sewer transfer, there are many uncharted Yorkshire Water assets currently not shown on our records.

The following comments reflect our view, with regard to the public sewer network only, based on a 'desk top' study of the site and are valid for a maximum period of twelve months:

**Existing Infrastructure**

There is a 450 mm diameter public combined water sewer recorded crossing the site. No buildings, or other obstructions, are to be erected within 3.5 (three point five) metres is required at each side of the sewer centre-line, no trees planted within 5 (five) metres of this public sewer.

There is a 225 mm diameter public combined water sewer recorded crossing the site. No buildings, or other obstructions, are to be erected within 3 (three) metres is required at each side of the sewer centre-line, no trees planted within 5 (five) metres of this public sewer.

It may not be acceptable to raise or lower ground levels over the sewer, nor to restrict access to the manholes on the sewer. If you wish to have this sewer diverted under Section 185 of the Water Industry Act 1991 an application should be made in writing. To discuss this matter, please telephone 0345 120 84 82.

### **Foul Water**

Development of the site should take place with separate systems for foul and surface water drainage. The separate systems should extend to the points of discharge to be agreed.

Foul water domestic waste can discharge to the 450 mm diameter public combined sewer recorded in the northern part of site.

### **Surface Water**

The developer's attention is drawn to Requirement H3 of the Building Regulations 2010. This establishes a preferred hierarchy for surface water disposal. Consideration should firstly be given to discharge to soakaway, infiltration system and watercourse in that priority order.

Sustainable Drainage Systems (SuDS), for example the use of soakaways and/or permeable hardstanding etc, may be a suitable solution for surface water disposal appropriate in this situation. You are advised to seek comments on the suitability of SuDS in this instance from the appropriate authorities.

As a last resort and subject to providing satisfactory evidence as to why the other methods of surface water disposal have been discounted, curtilage surface water may discharge to the 450 mm diameter public combined sewer recorded in the northern part of site.

The surface water discharge from the site to be restricted to not greater than 3.5 (three point five) litres/second. This permission is not an acceptance in respect to any planning conditions imposed under the Grant of Planning Permission.

### **Other Observations**

Any new connection to an existing public sewer will require the prior approval of Yorkshire Water. You may apply on line or obtain an application form from our website - <https://www.yorkshirewater.com/developers/sewerage/sewerage-connections/>

Prospectively adoptable sewers and pumping stations must be designed and constructed in accordance with the Code for Adoption 2023/24, pursuant to an agreement under Section 104 of the Water Industry Act 1991. We are happy to offer pre-development technical advice on any prospective sites that you would like to put forward for adoption, prior to submission of your adoption application.

An application to enter into a Section 104 agreement must be made in writing prior to any works commencing on site. Please contact our Sewer Adoption, Diversion and Requisition (telephone 0345 120 84 82) or email [technical.sewerage@yorkshirewater.co.uk](mailto:technical.sewerage@yorkshirewater.co.uk) or visit - <https://www.yorkshirewater.com/developers/sewerage/sewer-adoptions/> for further information.

All the above comments are based upon the information and records available at the present time and is subject to formal planning approval agreement. The information contained in this letter together with that shown on any extract from the Statutory Sewer Map that may be enclosed is believed to be correct and is supplied in good faith.



YorkshireWater

Please note that capacity in the public sewer network is not reserved for specific future development. It is used up on a 'first come, first served' basis. You should visit the site and establish the line and level of any public sewers affecting your proposals before the commencement of any design work.

Yours sincerely

**Chris Roberts**  
**Development Services Technician**



## Appendix 5 – Environment Agency

# Flood map for planning

Your reference  
<Unspecified>

Location (easting/northing)  
411031/415144

Created  
11 Sep 2024 9:10

**Your selected location is in flood zone 1, an area with a low probability of flooding.**

You will need to do a flood risk assessment if your site is **any of the following:**

- bigger than 1 hectare (ha)
- In an area with critical drainage problems as notified by the Environment Agency
- identified as being at increased flood risk in future by the local authority's strategic flood risk assessment
- at risk from other sources of flooding (such as surface water or reservoirs) and its development would increase the vulnerability of its use (such as constructing an office on an undeveloped site or converting a shop to a dwelling)

## Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence **which** sets out the terms and conditions for using government data. <https://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/>

Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. <https://flood-map-for-planning.service.gov.uk/os-terms>

## Flood map for planning

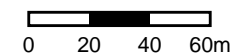
Your reference  
**<Unspecified>**

Location (easting/northing)  
**411031/415144**

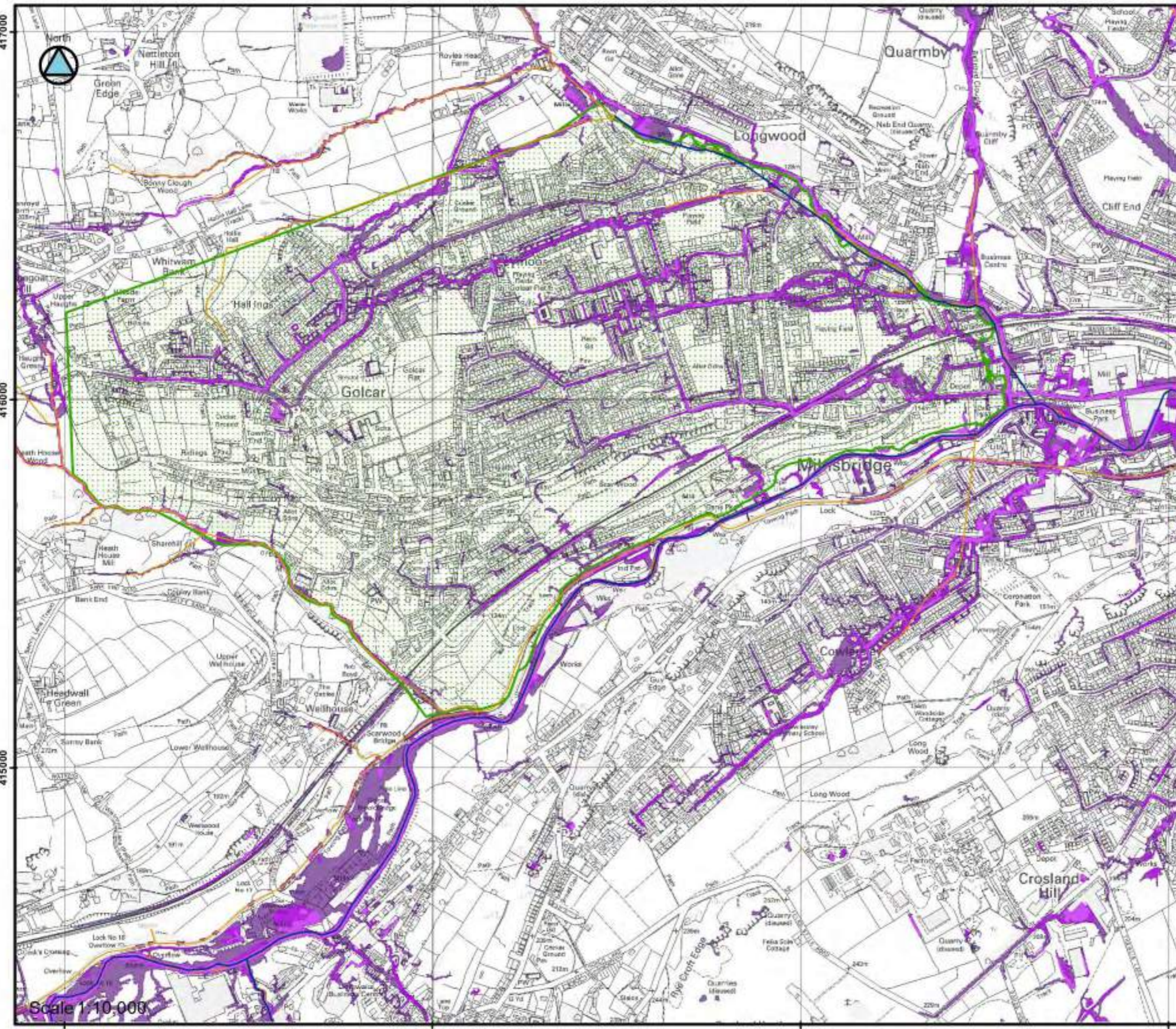
Scale  
**1:2500**

Created  
**11 Sep 2024 9:10**

-  Selected area
-  Flood zone 3
-  Flood zone 2
-  Flood zone 1
-  Flood defence
-  Main river
-  Water storage area



## Appendix 6 – Lead Local Flood Authority



**LEGEND**

- Choose Option
- Council boundary
  - Main River
  - Detailed River Network
  - uFMRSW**
  - 30 year event
  - 100 year event
  - 1000 year event
  - CDA indicative

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**STRATEGIC FLOOD RISK ASSESSMENT**  
 For  
**KIRKLEES COUNCIL**  
 MAP\_D

Scale 1:10,000

409000 410000 411000 412000

417000  
416000  
415000

**Consultation Response from KC,  
Lead Local Flood Authority**

**2024/93605 Land at, Main Avenue, Cowlersley, Huddersfield, HD4 5US**

**Erection of 57 dwellings with access from new through road connecting Main Avenue and Windsor Road, and associated works, including engineering and landscaping**

**Date Responded: 7<sup>th</sup> February 2025**

**Responding Officer: Paul Farndale**

**Responding Ref:**

**Kirklees Flood Management & Drainage acting as LLFA, requires FURTHER INFORMATION before making an initial decision on the application.**

We accept that infiltration techniques for the removal of surface water are not suitable for this development. We would object to a pumped solution to watercourse as identified would be required due to attenuation requirements and the shallow depth of the receiving system. We therefore hold no objection to discharging surface water to the public combined sewer at a restricted rate of 3.5l/s as stipulated by Yorkshire Water.

The WYCA guide to SUDS is now out of date and Kirklees climate change requirements default to NPPF and associated guidance. For this a 45% uptake is required. As the 1 in 100 year + climate change critical event is being stored, there is no requirement for urban creep. This should be analysed to provide indicative drawings, at the very least, that show that space has been made for water in the proposed layout.

We note that a survey of the watercourse running from site at the eastern boundary has been attempted indicating some capped off land drainage but with the main run obstructed. As land drainage from the site will need to connect in at this point, a full downstream survey of the culverted section of the watercourse is required to show that it is fit for purpose (this will form part of the flood risk assessment). For a site of this size, the survey should extend to the first open section located at 67 Warneford Road (see attached).

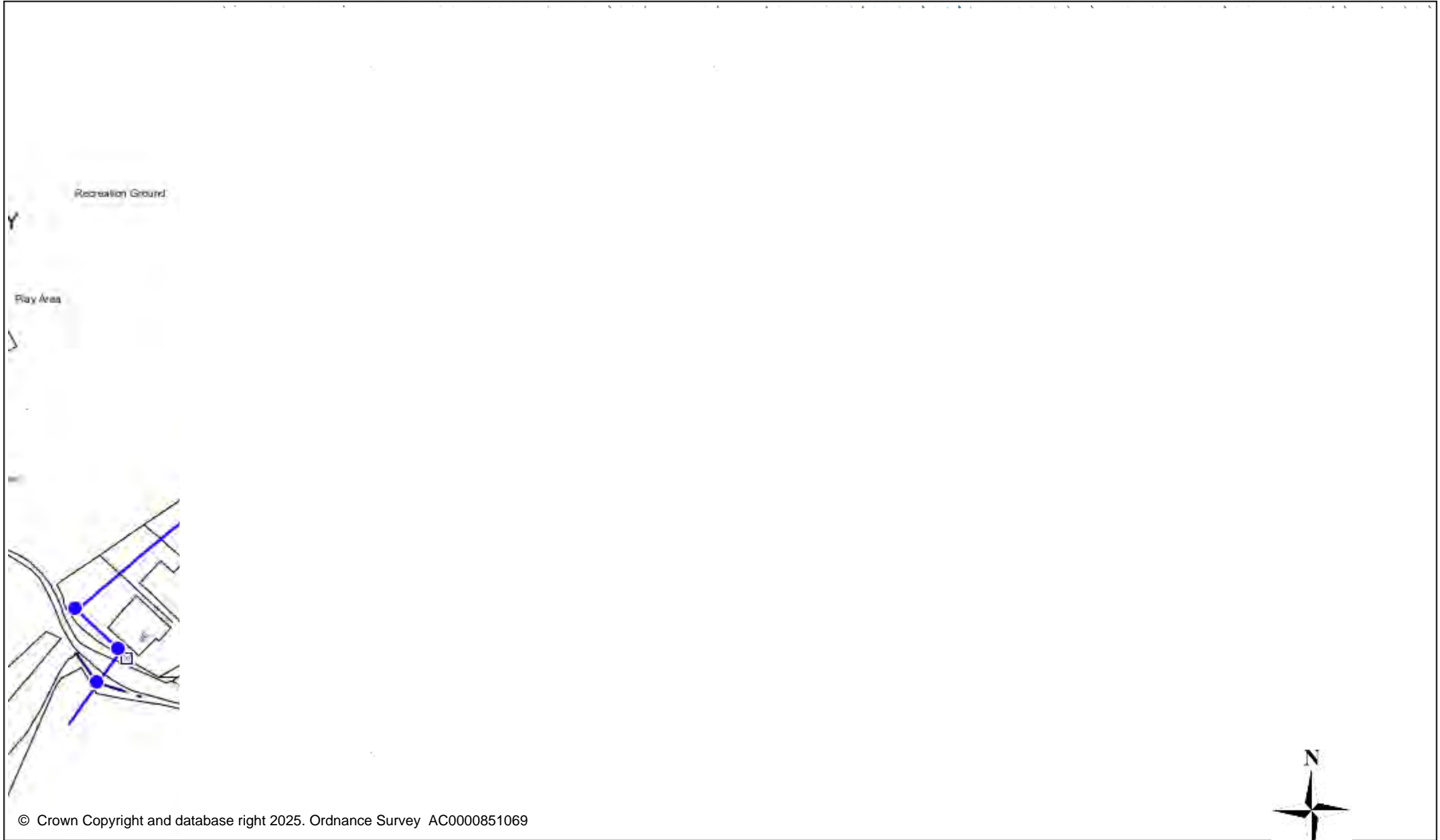
An examination of historical OS Maps shows a cluster of buildings toward the eastern boundary named 'Jubilee'. A well is clearly shown and in line with the downstream watercourse. The 1933 map is included as an example. Kirklees would like the applicant to determine the depth of the system as it leaves site and perform the excavation of slip trenches at the well location and upstream at several intervals including the western boundary with Main Avenue. Kirklees Council has previously noted overland flows (flows escaping?) along this low valley within the site in addition to water running south to north. The presence of existing systems must be fully investigated.

Kirklees Council has also witnessed flooding from gullies at the end of Main Avenue and will investigate this ourselves to ascertain what system they are connected to. There is anecdotal evidence of a culvert in a verge in Main Avenue and an abandoned manhole independent of the combined public sewer is still present within the road itself.

The LLFA is concerned about levels to the south of the development with a clear valley running toward retaining walls. This low spot does not coincide with the step identified as flow route. A layout review is required as should be the potential to include positive land drainage from the perimeter of the site.

Some plots on the northern side of the access road may need lifting slightly to ensure all driveways fall back toward to the road, in the interests of safe flood routing.

# warneford road



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Scale = 1:952.560

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Ordnance Survey AC0000851069.  
(maps@kirklees.gov.uk)

Print Date : 10-Feb-2025



1933 Map - -Well



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Scale = 1:1905.120

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Ordnance Survey AC0000851069.  
(maps@kirklees.gov.uk)

Print Date : 10-Feb-2025



## Appendix 7 – Greenfield Run-off Calculation

North East (Head Office)  
5 Staithes, The Watermark  
Gateshead, NE11 9SN

Main Ave  
Greenfield Run-off



Date 23/09/2024 08:28  
File

Designed by nick.dunwoodie  
Checked by

Innovyze Source Control 2020.1.3

ICP SUDS Mean Annual Flood

Input

Return Period (years)	1	Soil	0.450
Area (ha)	1.550	Urban	0.000
SAAR (mm)	831	Region Number	Region 3

**Results 1/s**

QBAR Rural	8.3
QBAR Urban	8.3




Q1 year 7.2

Q1 year	7.2
Q30 years	14.6
Q100 years	17.3

## Appendix 8 – Drainage Investigation

# CCTV Drainage Inspection Report.

WRc MSCC Fifth Edition

Control			
	Prepared By	Reviewed By	Authorised By
	Curtis Hobson-Clarke Centara Ltd Principle CCTV Surveyor	Tom Peart Centara Ltd Survey Manager	Neil Beaumont Centara Ltd Director of Operations
Signed			
Client	Strata Homes		
Location	Cowersley, Kirklees		
Requirements	To carry out a CCTV Drainage Condition survey showing connectivity		
Distribution List			
Issued to Strata		03/07/24	
Revision Control			
00 – Issued – 03/07/24 - CHC			

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## Executive Summary.

Further to our recent commission to carry out an investigative survey and provide a condition report of the underground drainage system at: **138 Main Ave, Cowersley, Kirklees.**

This report should be viewed in conjunction with the individual MP4 Files included in the report.

Each Folder contains the MP4 files for the individual pipes associated with the Coded Manhole. E.g., MH01, MH101 etc.

### Issues Encountered on Site:

We were unable to complete a full survey for the reasons listed below:

MH105 Pipe B was unable to be surveyed as it would require man access to place the camera unit in the pipe

MH105A Was unable to be raised (UTR)

### General Considerations

The drainage system consists of mostly (PVC) Polyvinylchloride, (CO) Concrete. The drains surveyed are in good condition.

### Recommendations

Centara are not able to make recommendations for remedial works or indeed whether this is feasible. However, in its current state the drainage is flowing, reparative measures will most likely be needed in the short term.

### Survey Drawing

Each manhole is referenced in the report using a unique code e.g., MH01 etc. This report should be read in conjunction with the AutoCAD drawing provided as an appendix to this report.

# CCTV Drainage Survey Code List.

B	BROKEN PIPE AT..... (OR FROM... TO...) O'CLOCK
BR	BRANCH MAJOR
CC	CRACK CIRCUMFERENTIAL FROM ... TO ... O'CLOCK
CL	CRACK LONGITUDINAL AT ... O'CLOCK
CM	CRACK'S MULTIPLE FROM ... TO ... O'CLOCK
CN	CONNECTIONS AT ... O'CLOCK, DIAMETER ... MM
CNI	CONNECTION AT ... O'CLOCK, DIAMETER ...MM, INTRUSION ... MM
CU	CAMERA UNDER WATER
CX	CONNECTION DEFECTIVE AT ... O'CLOCK, DIAMETER ... MM
CXI	CONNECTION DEFECTIVE AT ... O'CLOCK, DIAMETER ... MM, INTRUSION
D	DEFORMED SEWER ... %
DB	DISPLACED BRICKS AT ... (OR FROM ... TO ...) O'CLOCK
DC	DIMENSION OF SEWER CHANGES, NEW DIMENSION ... MM
DE	DEBRIS ...% CROSS-SECTIONAL AREA LOSS
DEG	DEBRIS GREASE ...% CROSS-SECTIONAL AREA LOSS
DES	DEBRIS SILT ...% CROSS-SECTIONAL AREA LOSS
DI	DROPPED INVERT, GAP ...MM
EH	ENCRUSTATION HEAVY FROM ... TO ... O'CLOCK ...% CROSS-SECTIONAL AREA LOSS
EHJ	ENCRUSTATION HEAVY FROM ... TO ... O'CLOCK ...% CROSS-SECTIONAL AREA LOSS AT JOINT
EN	ENCRUSTATION LIGHT FROM ... TO ... O'CLOCK
ELJ	ENCRUSTATION LIGHT FROM ... TO ... O'CLOCK AT JOINT
EM	ENCRUSTATION MEDIUM FROM ... TO ... O'CLOCK ...% CROSS-SECTIONAL AREA LOSS
EMJ	ENCRUSTATION MEDIUM FROM ... TO ... O'CLOCK ...% CROSS-SECTIONAL AREA LOSS
ESH	SCALE HEAVY FROM ... TO ... O'CLOCK ...%
ESL	SCALE LIGHT ...% CROSS-SECTIONAL AREA LOSS FROM ... TO ... O'CLOCK
ESM	SCALE MEDIUM ...% CROSS-SECTIONAL AREA LOSS FROM ... TO ... O'CLOCK
FC	FRACTURE CIRCUMFERENTIAL FROM ... TO ... O'CLOCK
FH	FINISH SURVEY
FL	FRACTURE LONGITUDINAL AT ... O'CLOCK
FM	FRACTURES MULTIPLE FROM ... TO ... O'CLOCK
GO	GENERAL OBSERVATION AT THIS POINT
GP	GENERAL PHOTOGRAPH NUMBER ... TAKEN AT THIS POINT
H	HOLE IN SEWER AT ... (OR FROM ... TO ...) O'CLOCK
ID	INFILTRATION DRIPPER AT ... (OR FROM ... TO ...) O'CLOCK
IDJ	INFILTRATION DRIPPER AT ... (OR FROM ... TO ...) O'CLOCK AT JOINT
IG	INFILTRATION GUSHER AT ... (OR FROM ... TO ...) O'CLOCK
IGJ	INFILTRATION GUSHER AT ... (OR FROM ... TO ...) O'CLOCK AT JOINT
IR	INFILTRATION RUNNER AT ... (OR FROM ... TO ...) O'CLOCK

IRJ	INFILTRATION RUNNER AT ... (OR FROM ... TO ...) O'CLOCK AT JOINT
IS	INFILTRATION SEEPER AT ... (OR FROM ... TO ...) O'CLOCK
ISJ	INFILTRATION SEEPER AT ... (OR FROM ... TO ...) O'CLOCK AT JOINT
JDL	JOINT DISPLACED LARGE
JDM	JOINT DISPLACED MEDIUM
JN	JUNCTION AT ... O'CLOCK, DIAMETER ...MM
JX	JUNCTION DEFECTIVE AT ... O'CLOCK, DIAMETER ...MM
LC	LINING OF SEWER CHANGES/START/FINISHES AT THIS POINT
LD	LINE OF SEWER DEVIATES DOWN
LL	LINE OF SEWER DEVIATES LEFT
LN	LINING DEFECT AT ... (OR FROM ... TO ...) O'CLOCK
LR	LINE OF SEWER DEVIATES RIGHT
LU	LINE OF SEWER DEVIATES UP
MB	MISSING BRICKS AT ... (OR FROM ... TO ...) O'CLOCK
MC	MATERIAL OF SEWER CHANGES AT THIS POINT
MH	MANHOLE/NODE
MM	MORTAR MISSING MEDIUM AT ... (OR FROM ... TO ...) O'CLOCK
MS	MORTAR MISSING SURFACE AT ... (OR FROM ... TO ...) O'CLOCK
MT	MORTAR MISSING TOTAL AT ... (OR FROM ... TO ...) O'CLOCK
OB	OBSTRUCTION ...% HEIGHT/DIAMETER LOSS
OJL	OPEN JOINT LARGE
OJM	OPEN JOINT MEDIUM
PC	LENGTH OF PIPE FORMING SEWER CHANGES AT THIS POINT, NEW LENGTH ...MM
RF	ROOTS FINE
RFJ	ROOTS MASS ...% CROSS-SECTIONAL AREA LOSS
RMJ	ROOTS MASS ...% CROSS-SECTIONAL AREA LOSS AT JOINT
RT	ROOTS TAP
RTJ	ROOTS TAP AT JOINT
SA	SURVEY ABANDONED
SC	SHAPE OF SEWER CHANGES AT THIS POINT
SSL	SURFACE DAMAGE, SPALLING LARGE AT ... (OR FROM ... TO ...) O'CLOCK
SSM	SURFACE DAMAGE, SPALLING MEDIUM AT ... (OR FROM ... TO ...) O'CLOCK
SSS	SURFACE DAMAGE, SPALLING SLIGHT AT ... (OR FROM ... TO ...) O'CLOCK
ST	START OF SURVEY
SWL	SURFACE DAMAGE, WEAR LARGE AT ... (OR FROM ... TO ...) O'CLOCK
SWM	SURFACE DAMAGE, WEAR MEDIUM AT ... (OR FROM ... TO ...) O'CLOCK
SWS	SURFACE DAMAGE, WEAR SLIGHT AT ... (OR FROM ... TO ...) O'CLOCK
V	VERMIN (RATS AND MICE)
WL	WATER LEVEL ...% HEIGHT/DIAMETER
X	SEWER COLLAPSED ...% CROSS-SECTIONAL AREA LOSS

MANHOLE NODE:  
Combined Water

MH  
101


PHOTOGRAPHIC PLAN

EXTERNAL PHOTOGRAPH:



INTERNAL PHOTOGRAPH:



<b>MANHOLE NODE:</b> Combined Water	<b>MH</b> 102	<b>PHOTOGRAPHIC PLAN</b>
<p style="text-align: center;">EXTERNAL PHOTOGRAPH:</p> 		
<p style="text-align: center;">INTERNAL PHOTOGRAPH:</p>		

MANHOLE NODE: Combined Water	MH 103	PHOTOGRAPHIC PLAN
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EXTERNAL PHOTOGRAPH:



INTERNAL PHOTOGRAPH:



MANHOLE NODE: Combined Water	MH 104	PHOTOGRAPHIC PLAN
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EXTERNAL PHOTOGRAPH:



INTERNAL PHOTOGRAPH:



MANHOLE NODE: Combined Water	MH 105	PHOTOGRAPHIC PLAN
---------------------------------	-----------	-------------------

EXTERNAL PHOTOGRAPH:



INTERNAL PHOTOGRAPH:



MANHOLE NODE: Combined Water	MH 105A	PHOTOGRAPHIC PLAN
---------------------------------	------------	-------------------

EXTERNAL PHOTOGRAPH:



INTERNAL PHOTOGRAPH:

MANHOLE NODE:  
Surface Water

MH 01

PHOTOGRAPHIC PLAN

EXTERNAL PHOTOGRAPH:



INTERNAL PHOTOGRAPH:

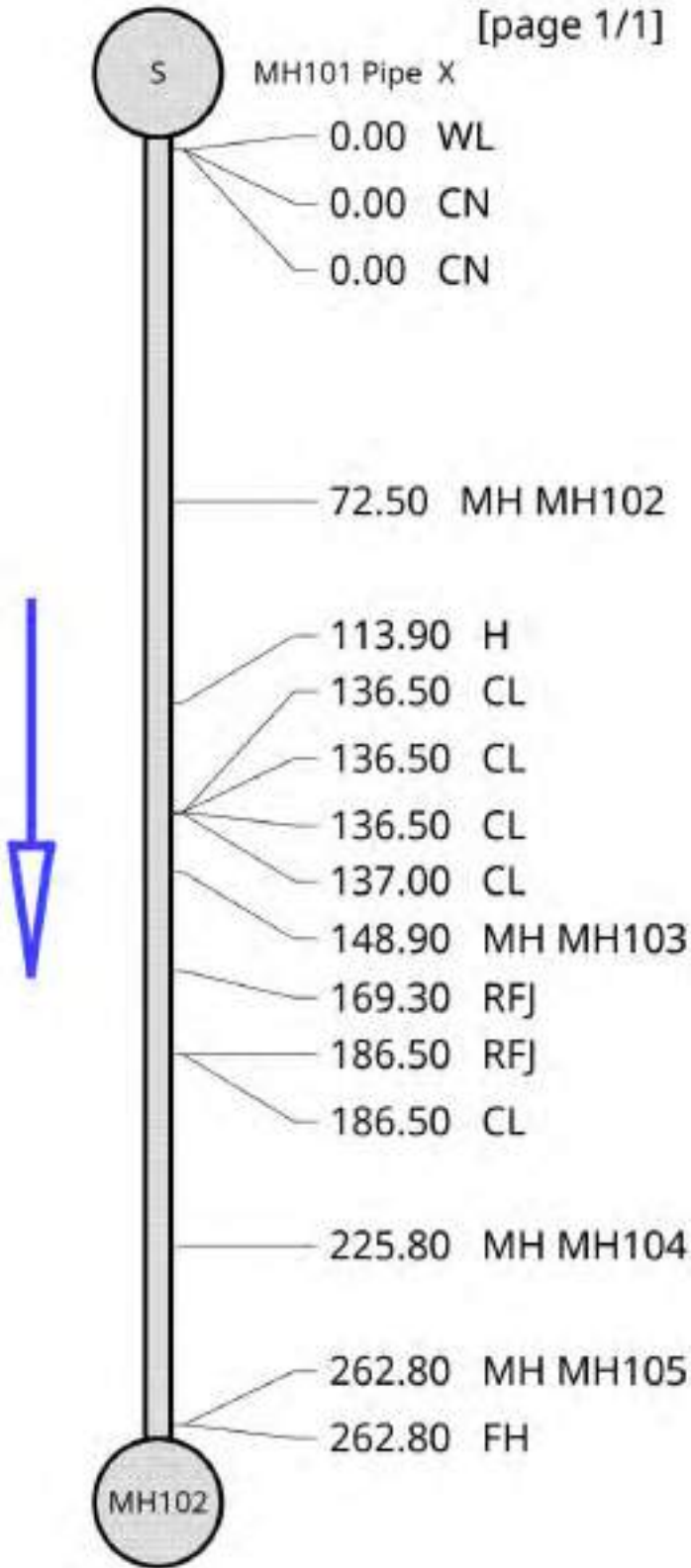


# 1 MH101 Pipe X Drain / Sewer Survey

## 1.1 Survey Header

1.1.1	Surveyed by (Operator)	Hobson-Clarke
1.1.2	Contract no.	N/A
1.1.3	Job no.	109726
1.1.4	Catchment (Drainage area)	N/A
1.1.5	Division	N/A
1.1.6	District	N/A
1.1.7	Pipeline length ref	N/AA
1.1.8	Date	200624
1.1.9	Time	09:41
1.1.10	Location	Cowersley
1.1.11	Start manhole no.	MH101 Pipe X
1.1.12	Start depth	1.96m
1.1.13	Start cover level	N/A
1.1.14	Start invert level	N/A
1.1.15	Finish manhole no.	MH102
1.1.16	Finish depth	N/Am
1.1.17	Finish cover level	N/A
1.1.18	Finish invert level	N/A
1.1.19	Use of Drain	(C) Combined
1.1.20	Direction	(D) Survey downstream (camera pointing with flow)
1.1.21	Size 1 (diameter/height)	500mm
1.1.22	Size 2 (width)	500mm
1.1.23	Shape	(C) Circular
1.1.24	Material	(CO) Concrete
1.1.25	Lining	
1.1.26	Pipe length	N/Am
1.1.27	Total length	N/Am
1.1.28	Year laid	N/A
1.1.29	Video cassette number	N/A
1.1.30	Comments: General	
1.1.31	Purpose	(F) Sample survey to determine asset condition
1.1.32	Sewer category	(Z) Not Known
1.1.33	Pre-cleaning	(N) No
1.1.34	Weather	(1) Dry
1.1.35	Location code	(C) Light road (rural roads with light traffic, town and city back streets, estate roads and parking areas)
1.1.36	Further location details	




1.2 Diagram



### 1.3 Observations

Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
0.0	(WL) Water level ...% height/diameter Percentage: 10%	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_45_18_839.jpg 
		0:00:00
0.0	(CN) Connection at ... o'clock, diameter ...mm Clock At/From: 01 Diameter/Dimension: 150	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_45_24_162.jpg 
01		0:00:02
0.0	(CN) Connection at ... o'clock, diameter ...mm Clock At/From: 12 Diameter/Dimension: 225	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_45_57_062.jpg 
12		0:00:18
72.5	(MH) Manhole/node  MH102	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_50_32_074.jpg 
		0:04:01
113.9	(H) Hole in sewer at ... (OR from ... to ...) o'clock Clock At/From: 11 Clock To: 01 Diameter/Dimension: 100	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_53_23_273.jpg 
11 - 01		0:06:23
136.5	(CL) Crack longitudinal at ... o'clock Clock At/From: 12	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_55_39_319.jpg 
12		0:08:29

Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
136.5	(CL) Crack longitudinal at ... o'clock Clock At/From: 03	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_55_48_056.jpg 
03		0:08:30
136.5	(CL) Crack longitudinal at ... o'clock Clock At/From: 07	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_55_56_667.jpg 
07		0:08:30
137.0	(CL) Crack longitudinal at ... o'clock Clock At/From: 06	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_56_37_525.jpg 
06		0:08:56
148.9	(MH) Manhole/node	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_57_27_563.jpg 
	MH103	0:09:43
169.3	(RFJ) Roots fine at joint	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_58_42_603.jpg 
		0:10:50
186.5	(RFJ) Roots fine at joint	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-09_59_56_593.jpg 
		0:11:53

Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
186.5	(CL) Crack longitudinal at ... o'clock Clock At/From: 06	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-10_00_02_209.jpg 
06		0:11:53
225.8	(MH) Manhole/node	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-10_02_19_714.jpg 
	MH104	0:14:05
262.8	(MH) Manhole/node	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-10_16_22_651.jpg 
	MH105	0:18:45
262.8	(FH) Finish survey	./MH101-Pipe---X/MH101-Pipe---X_2024_06_20-10_16_41_854.jpg 
		0:18:50

### 1.4 Photographs

(WL) Water level ...% height/diameter ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (CN) Connection at ... o'clock, diameter ...mm ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(CN) Connection at ... o'clock, diameter ...mm ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (MH) Manhole/node ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(H) Hole in sewer at ... (OR from ... to ...) ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (CL) Crack longitudinal at ... o'clock ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(CL) Crack longitudinal at ... o'clock ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (CL) Crack longitudinal at ... o'clock ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(CL) Crack longitudinal at ... o'clock ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (MH) Manhole/node ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(RFJ) Roots fine at joint ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (RFJ) Roots fine at joint ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(CL) Crack longitudinal at ... o'clock ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (MH) Manhole/node ./.MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-



(MH) Manhole/node

./MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20- (FH) Finish survey

./MH101-Pipe---X/MH101-Pipe---X\_2024\_06\_20-

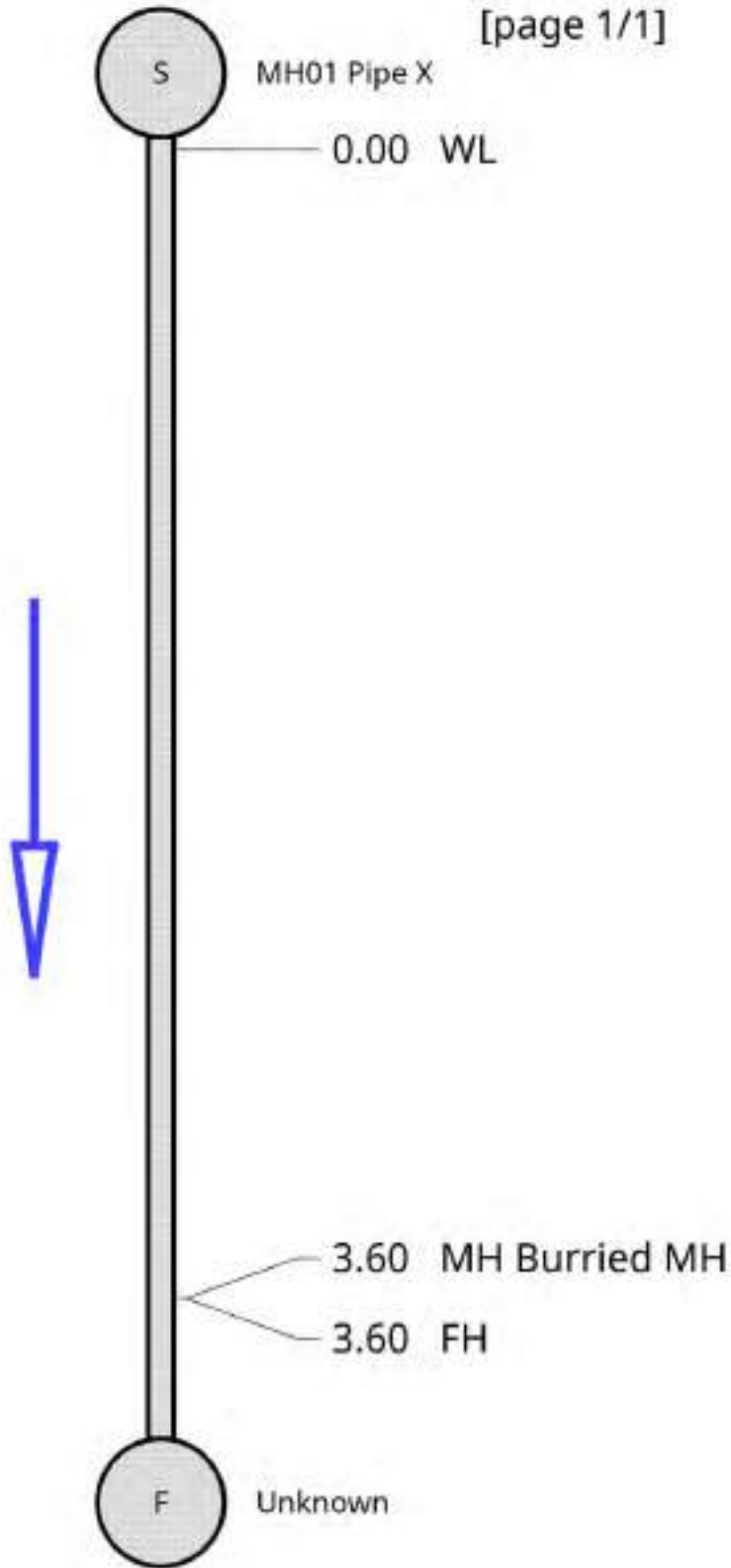


## 2 MH01 Pipe X Drain / Sewer Survey




### 2.1 Survey Header

2.1.1	Surveyed by (Operator)	Hobson-Clarke
2.1.2	Contract no.	N/A
2.1.3	Job no.	109726
2.1.4	Catchment (Drainage area)	N/A
2.1.5	Division	N/A
2.1.6	District	N/A
2.1.7	Pipeline length ref	N/AA
2.1.8	Date	200624
2.1.9	Time	11:46
2.1.10	Location	Cowersley
2.1.11	Start manhole no.	MH01 Pipe X
2.1.12	Start depth	0.82m
2.1.13	Start cover level	N/A
2.1.14	Start invert level	N/A
2.1.15	Finish manhole no.	Unknown
2.1.16	Finish depth	N/Am
2.1.17	Finish cover level	N/A
2.1.18	Finish invert level	N/A
2.1.19	Use of Drain	(S) Surface Water
2.1.20	Direction	(D) Survey downstream (camera pointing with flow)
2.1.21	Size 1 (diameter/height)	225mm
2.1.22	Size 2 (width)	225mm
2.1.23	Shape	(C) Circular
2.1.24	Material	(CO) Concrete
2.1.25	Lining	
2.1.26	Pipe length	N/Am
2.1.27	Total length	N/Am
2.1.28	Year laid	N/A
2.1.29	Video cassette number	N/A
2.1.30	Comments: General	
2.1.31	Purpose	(F) Sample survey to determine asset condition
2.1.32	Sewer category	(Z) Not Known
2.1.33	Pre-cleaning	(N) No
2.1.34	Weather	(1) Dry
2.1.35	Location code	(C) Light road (rural roads with light traffic, town and city back streets, estate roads and parking areas)
2.1.36	Further location details	

2.2 Diagram



### 2.3 Observations

Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
0.0	(WL) Water level ...% height/diameter Percentage: 5%	./MH01-Pipe-----X/MH01-Pipe-----X_2024_06_20-11_49_03_667.jpg 
		0:00:00
3.6	(MH) Manhole/node	./MH01-Pipe-----X/MH01-Pipe-----X_2024_06_20-11_52_01_920.jpg 
	Burried MH	0:02:38
3.6	(FH) Finish survey	./MH01-Pipe-----X/MH01-Pipe-----X_2024_06_20-11_52_10_717.jpg 
		0:02:38

## 2.4 Photographs

(WL) Water level ...% height/diameter

./MH01-Pipe-----X/MH01-Pipe-----X\_2024\_06\_20-

(MH) Manhole/node

./MH01-Pipe-----X/MH01-Pipe-----X\_2024\_06\_20-



(FH) Finish survey

./MH01-Pipe-----X/MH01-Pipe-----X\_2024\_06\_20-

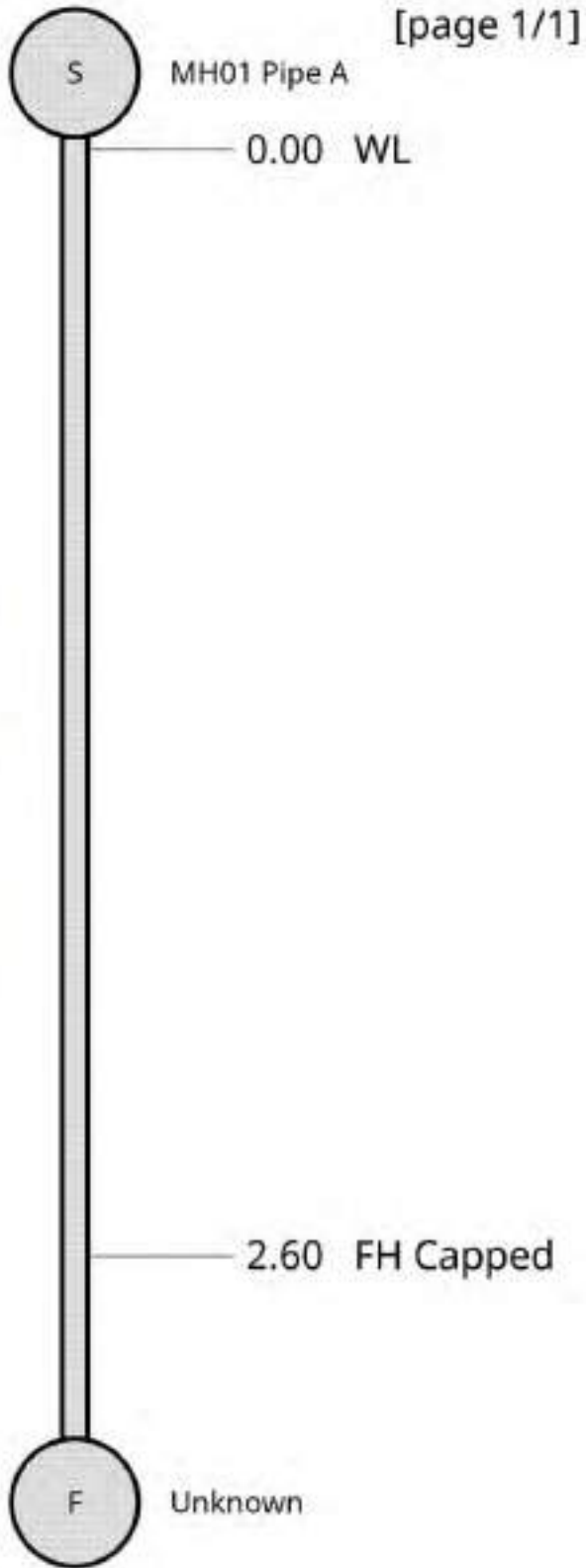


### 3 MH01 Pipe A Drain / Sewer Survey



#### 3.1 Survey Header

3.1.1	Surveyed by (Operator)	Hobson-Clarke
3.1.2	Contract no.	N/A
3.1.3	Job no.	109726
3.1.4	Catchment (Drainage area)	N/A
3.1.5	Division	N/A
3.1.6	District	N/A
3.1.7	Pipeline length ref	N/AA
3.1.8	Date	200624
3.1.9	Time	11:54
3.1.10	Location	Cowersley
3.1.11	Start manhole no.	MH01 Pipe A
3.1.12	Start depth	0.32m
3.1.13	Start cover level	N/A
3.1.14	Start invert level	N/A
3.1.15	Finish manhole no.	Unknown
3.1.16	Finish depth	N/Am
3.1.17	Finish cover level	N/A
3.1.18	Finish invert level	N/A
3.1.19	Use of Drain	(S) Surface Water
3.1.20	Direction	(U) Survey upstream (camera pointing against flow)
3.1.21	Size 1 (diameter/height)	150mm
3.1.22	Size 2 (width)	150mm
3.1.23	Shape	(C) Circular
3.1.24	Material	(PVC) Polyvinyl chloride
3.1.25	Lining	
3.1.26	Pipe length	N/Am
3.1.27	Total length	N/Am
3.1.28	Year laid	N/A
3.1.29	Video cassette number	N/A
3.1.30	Comments: General	
3.1.31	Purpose	(F) Sample survey to determine asset condition
3.1.32	Sewer category	(Z) Not Known
3.1.33	Pre-cleaning	(N) No
3.1.34	Weather	(1) Dry
3.1.35	Location code	(C) Light road (rural roads with light traffic, town and city back streets, estate roads and parking areas)
3.1.36	Further location details	

3.2 Diagram



### 3.3 Observations

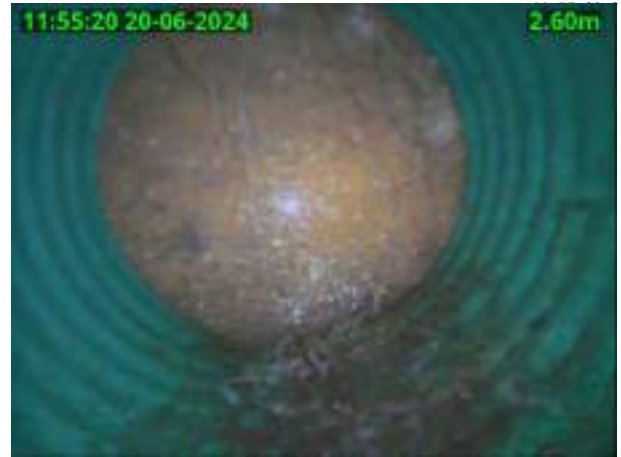
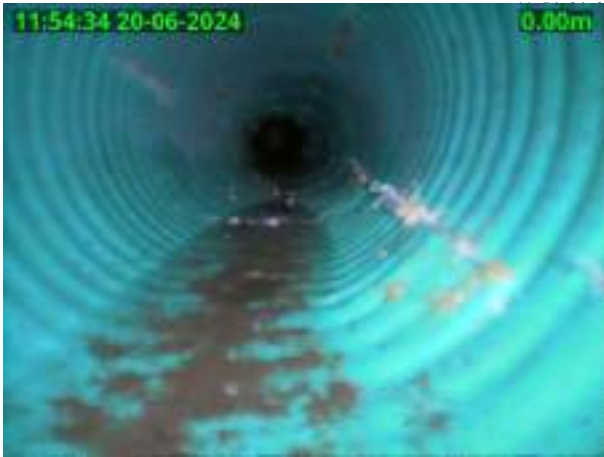
Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
0.0	(WL) Water level ...% height/diameter Percentage: 5%	./MH01-Pipe---A/MH01-Pipe---A_2024_06_20-11_54_34_686.jpg 
		0:02:39
2.6	(FH) Finish survey	./MH01-Pipe---A/MH01-Pipe---A_2024_06_20-11_55_20_368.jpg 
	Capped	0:00:42

### 3.4 Photographs

(WL) Water level ...% height/diameter

.MH01-Pipe---A/MH01-Pipe---A\_2024\_06\_20- (FH) Finish survey

.MH01-Pipe---A/MH01-Pipe---A\_2024\_06\_20-

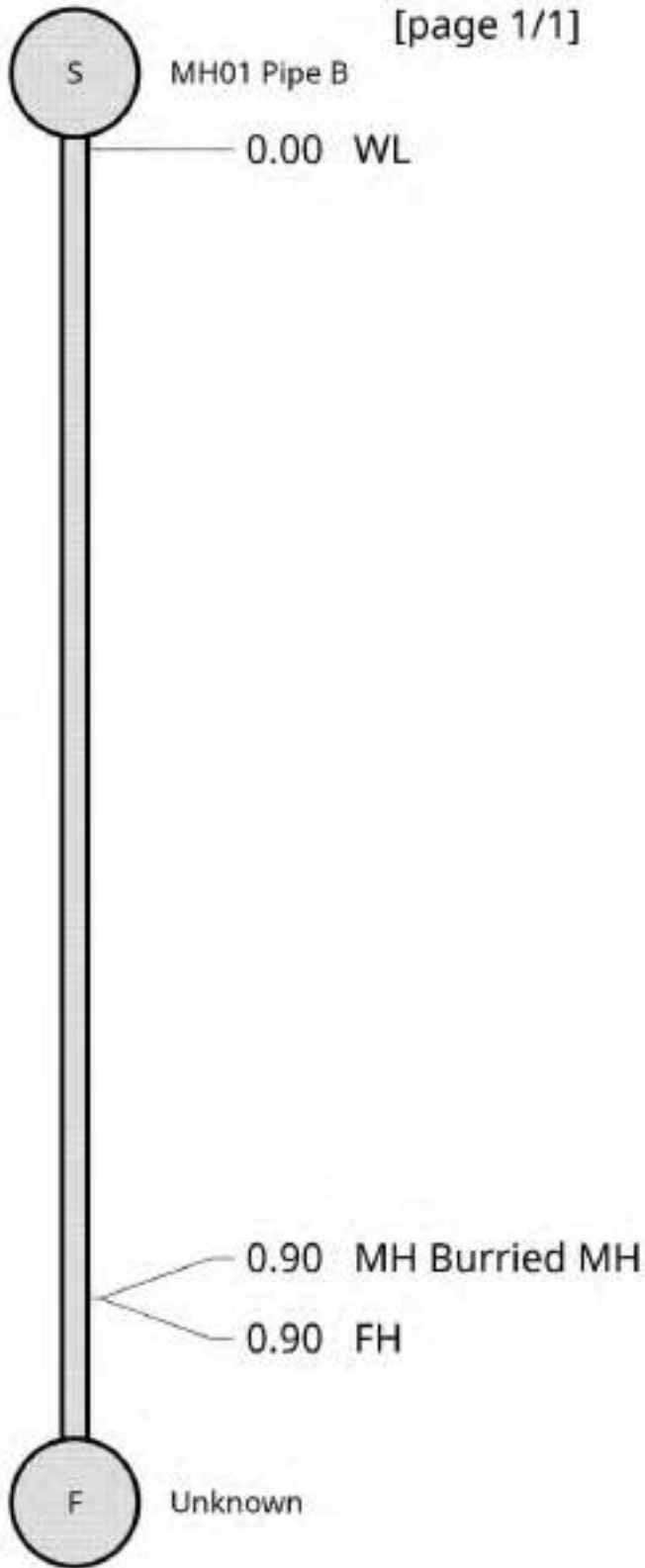


## 4 MH01 Pipe B Drain / Sewer Survey




### 4.1 Survey Header

4.1.1	Surveyed by (Operator)	Hobson-Clarke
4.1.2	Contract no.	N/A
4.1.3	Job no.	109726
4.1.4	Catchment (Drainage area)	N/A
4.1.5	Division	N/A
4.1.6	District	N/A
4.1.7	Pipeline length ref	N/AA
4.1.8	Date	200624
4.1.9	Time	11:57
4.1.10	Location	Cowersley
4.1.11	Start manhole no.	MH01 Pipe B
4.1.12	Start depth	0.80m
4.1.13	Start cover level	N/A
4.1.14	Start invert level	N/A
4.1.15	Finish manhole no.	Unknown
4.1.16	Finish depth	N/Am
4.1.17	Finish cover level	N/A
4.1.18	Finish invert level	N/A
4.1.19	Use of Drain	(S) Surface Water
4.1.20	Direction	(U) Survey upstream (camera pointing against flow)
4.1.21	Size 1 (diameter/height)	225mm
4.1.22	Size 2 (width)	225mm
4.1.23	Shape	(C) Circular
4.1.24	Material	(PVC) Polyvinyl chloride
4.1.25	Lining	
4.1.26	Pipe length	N/Am
4.1.27	Total length	N/Am
4.1.28	Year laid	N/A
4.1.29	Video cassette number	N/A
4.1.30	Comments: General	
4.1.31	Purpose	(F) Sample survey to determine asset condition
4.1.32	Sewer category	(Z) Not Known
4.1.33	Pre-cleaning	(N) No
4.1.34	Weather	(1) Dry
4.1.35	Location code	(C) Light road (rural roads with light traffic,town and city back streets,estate roads and parking areas)
4.1.36	Further location details	

4.2 Diagram



### 4.3 Observations

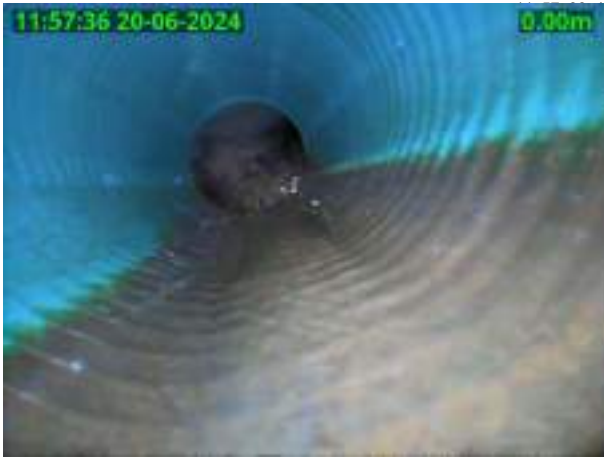
Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
0.0	(WL) Water level ...% height/diameter Percentage: 5%	./MH01-Pipe---B/MH01-Pipe---B_2024_06_20-11_57_36_478.jpg 
		0:00:02
0.9	(MH) Manhole/node	./MH01-Pipe---B/MH01-Pipe---B_2024_06_20-11_59_12_213.jpg 
	Burried MH	0:00:53
0.9	(FH) Finish survey	./MH01-Pipe---B/MH01-Pipe---B_2024_06_20-11_59_20_206.jpg 
		0:00:54

### 4.4 Photographs

(WL) Water level ...% height/diameter

.MH01-Pipe--B/MH01-Pipe--B\_2024\_06\_20- (MH) Manhole/node

.MH01-Pipe--B/MH01-Pipe--B\_2024\_06\_20-



(FH) Finish survey

.MH01-Pipe--B/MH01-Pipe--B\_2024\_06\_20-

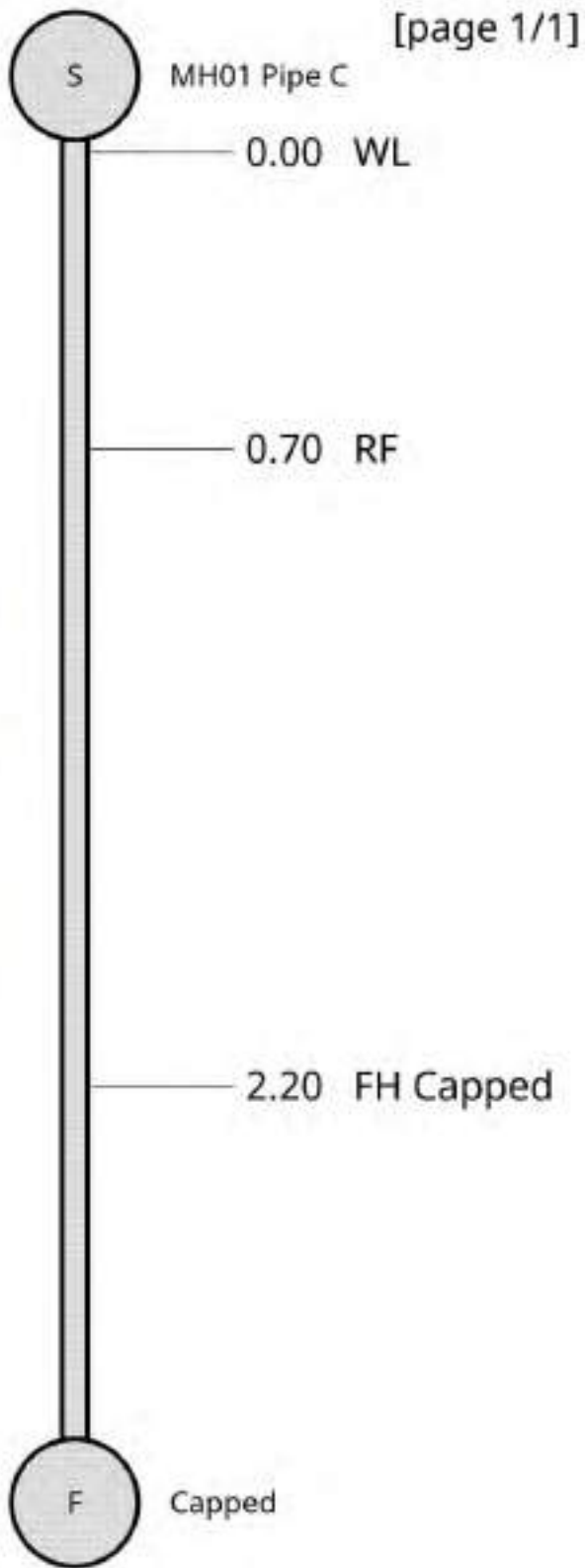


## 5 MH01 Pipe C Drain / Sewer Survey




### 5.1 Survey Header

5.1.1	Surveyed by (Operator)	Hobson-Clarke
5.1.2	Contract no.	N/A
5.1.3	Job no.	109726
5.1.4	Catchment (Drainage area)	N/A
5.1.5	Division	N/A
5.1.6	District	N/A
5.1.7	Pipeline length ref	N/AA
5.1.8	Date	200624
5.1.9	Time	11:59
5.1.10	Location	Cowersley
5.1.11	Start manhole no.	MH01 Pipe C
5.1.12	Start depth	0.33m
5.1.13	Start cover level	N/A
5.1.14	Start invert level	N/A
5.1.15	Finish manhole no.	Capped
5.1.16	Finish depth	N/Am
5.1.17	Finish cover level	N/A
5.1.18	Finish invert level	N/A
5.1.19	Use of Drain	(S) Surface Water
5.1.20	Direction	(U) Survey upstream (camera pointing against flow)
5.1.21	Size 1 (diameter/height)	150mm
5.1.22	Size 2 (width)	150mm
5.1.23	Shape	(C) Circular
5.1.24	Material	(PVC) Polyvinyl chloride
5.1.25	Lining	
5.1.26	Pipe length	N/Am
5.1.27	Total length	N/Am
5.1.28	Year laid	N/A
5.1.29	Video cassette number	N/A
5.1.30	Comments: General	
5.1.31	Purpose	(F) Sample survey to determine asset condition
5.1.32	Sewer category	(Z) Not Known
5.1.33	Pre-cleaning	(N) No
5.1.34	Weather	(1) Dry
5.1.35	Location code	(C) Light road (rural roads with light traffic,town and city back streets,estate roads and parking areas)
5.1.36	Further location details	

5.2 Diagram



### 5.3 Observations

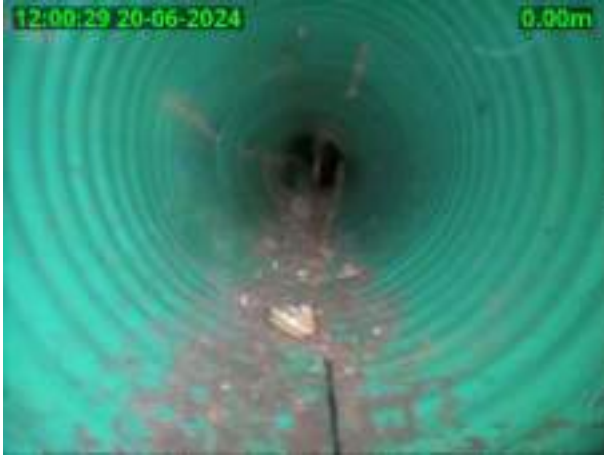
Distance	Condition code and attributes	Photo Ref
Cont. Defect		
Clock (At - To)		
Junta	Remarks	Video Ref
0.0	(WL) Water level ...% height/diameter Percentage: 5%	./MH01-Pipe-C/MH01-Pipe-C_2024_06_20-12_00_29_935.jpg 
		0:00:55
0.7	(RF) Roots fine	./MH01-Pipe-C/MH01-Pipe-C_2024_06_20-12_00_47_766.jpg 
		0:00:15
2.2	(FH) Finish survey	./MH01-Pipe-C/MH01-Pipe-C_2024_06_20-12_01_20_276.jpg 
	Capped	0:00:43

## 5.4 Photographs

(WL) Water level ...% height/diameter

/MH01-Pipe-C/MH01-Pipe-C\_2024\_06\_20- (RF) Roots fine

/MH01-Pipe-C/MH01-Pipe-C\_2024\_06\_20-



(FH) Finish survey

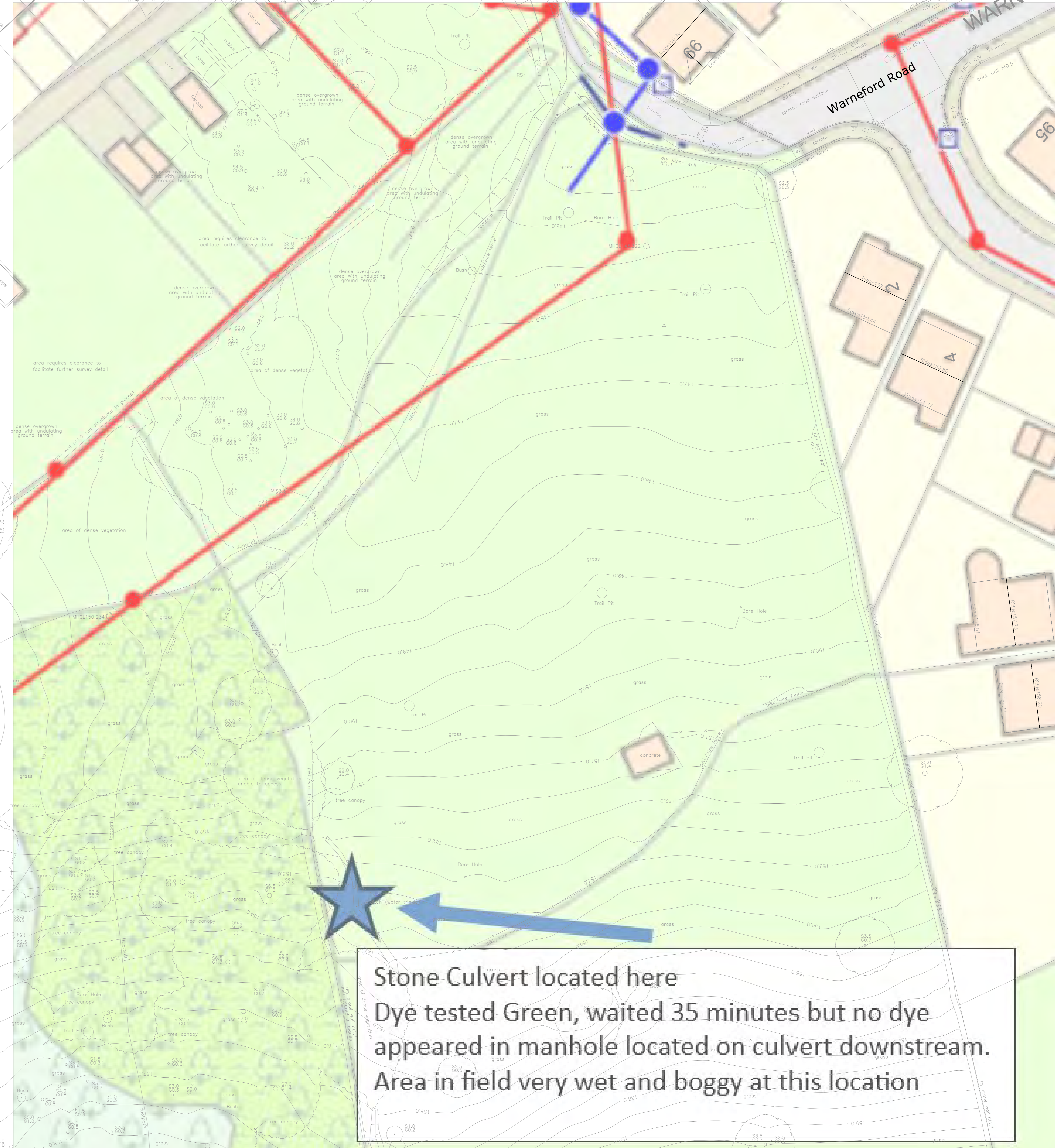
/MH01-Pipe-C/MH01-Pipe-C\_2024\_06\_20-



PERSEVERANCE STREET

WARNEFORD ROAD

Warneford Road



Stone Culvert located here  
 Dye tested Green, waited 35 minutes but no dye  
 appeared in manhole located on culvert downstream.  
 Area in field very wet and boggy at this location



SPRING NOTED ON TOPO BUT NOT LOCATED ON DATE OF WALKOVER

WATER FEATURE LOCATED APPROX. WHERE \* IS. VISIBLE TRICKLING WATER. GROUND DRY IMMEDIATELY DOWNSTREAM

DITCH DRY ON DATE OF WALKOVER

WATER FEATURE WITH STONE CAP LOCATED. VISIBLE TRICKLING WATER. GROUND DRY IMMEDIATELY DOWNSTREAM

BOGGY GROUND NOTED ON TOPO - DRY ON DATE OF WALKOVER

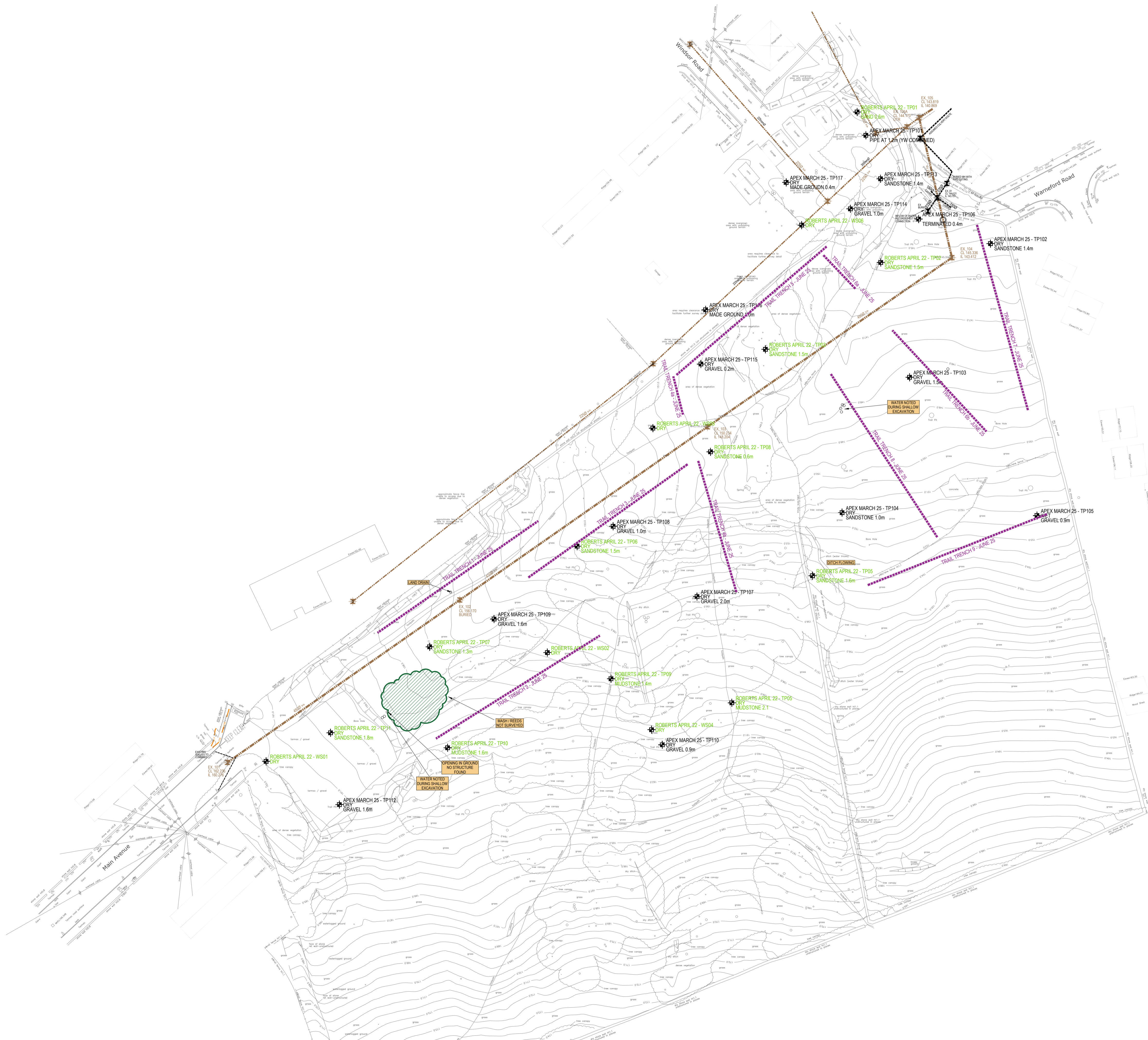
Warnerford Road

Possible spring or former culvert



- CONSTRAINTS PLAN**
- THIS DRAWING IS TO BE READ IN CONJUNCTION WITH:  
ALL EXISTING UTILITIES RECORDS.  
TOPOGRAPHICAL SURVEY.  
TRIAL HOLE INVESTIGATIONS IF AVAILABLE.
  - SERVICES INDICATED ON THIS DRAWING ARE INTERPOLATED FROM EXISTING RECORDS. ADDITIONAL SERVICES MAY BE PRESENT THAT ARE NOT IDENTIFIED ON RECORDS.
  - EXISTING SERVICES ARE TO BE LOCATED BY HAND PRIOR COMMENCEMENT OF ADJACENT EXCAVATION WORKS.
  - SUPPLIES TO EXISTING BUILDINGS ARE TO BE TERMINATED BACK TO MAIN BY RELEVANT UTILITY COMPANY PRIOR TO DEMOLITION WORKS.
  - ANY DISCREPANCIES ARE TO BE REPORTED TO ENGINEER, IF IN DOUBT ASK.

- EXISTING COMBINED SEWER
- EXISTING COMBINED SEWER TO BE SURVEYED
- EXISTING SURFACE WATER
- SURFACE WATER FLOODING
- SURFACE WATER FLOW ROUTES



Rev	Date	Revision Details	Drawn	Checked

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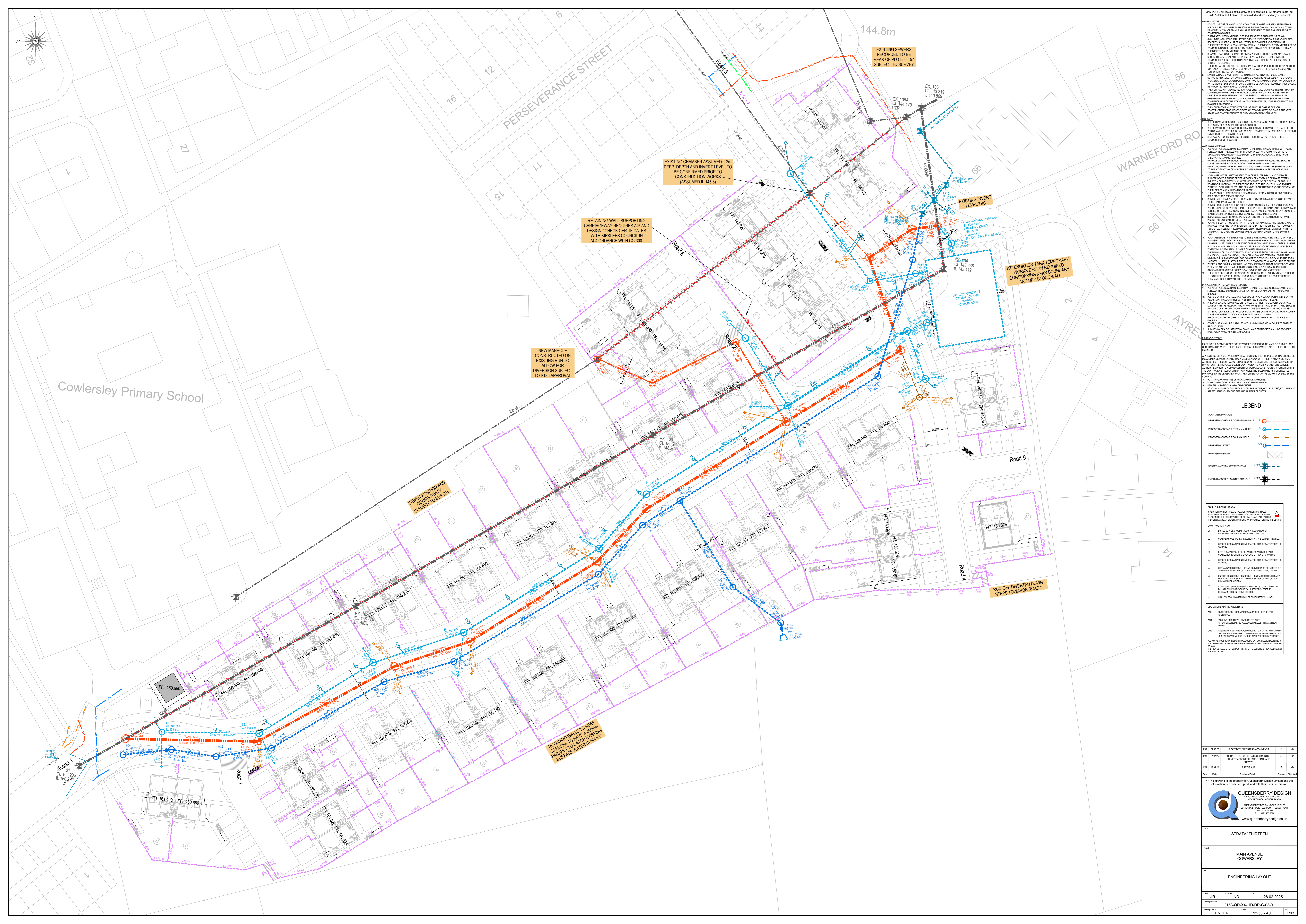
Client: **STRATA / THIRTEEN**

Project: **MAIN AVEUNE  
COWERSLEY**

Title: **INVESTIGATION RESULTS**

Drawn	Checked	Date
ND		24.07.2025
Drawing Number: -		
Drawing Status: <b>INFORMATION</b>	Scale: 1:500 - A1	Rev: -

## Appendix 9 – Drainage Strategy









### Design Settings

Rainfall Methodology FSR Return Period (years) 1 Additional Flow (%) 0 FSR Region England and Wales M5-60 (mm) 19.000 Ratio-R 0.330 CV 0.750 Time of Entry (mins) 5.00	Maximum Time of Concentration (mins) 30.00 Maximum Rainfall (mm/hr) 50.0 Minimum Velocity (m/s) 1.00 Connection Type Level Soffits Minimum Backdrop Height (m) 0.200 Preferred Cover Depth (m) 1.200 Include Intermediate Ground ✓ Enforce best practice design rules ✓
---	--

### Nodes

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
S1	0.041	5.00	160.593	1200	410932.657	415088.862	1.650
S2	0.102	5.00	158.989	1200	410954.724	415090.494	1.562
S3	0.053	5.00	156.779	1350	410979.156	415108.764	1.425
S4	0.086	5.00	155.228	1350	410999.080	415117.416	1.444
S5	0.099	5.00	152.628	1500	411028.141	415139.166	1.608
S6	0.046	5.00	151.458	1350	411037.773	415152.382	2.073
S14	0.046	5.00	149.101	1200	411057.116	415189.737	1.621
S7	0.150	5.00	148.747	1500	411068.056	415175.249	2.385
S8	0.108	5.00	146.735	1200	411064.067	415227.901	1.425
S9	0.120	5.00	147.987	1200	411098.720	415184.037	1.977
S11	0.042	5.00	147.325	1800	411093.637	415194.565	2.859
S12			147.377	1500	411097.912	415196.822	2.923
TANK			147.403	1200	411099.317	415197.507	4.209
1		5.00	145.800	2100	411101.868	415215.539	2.650
S13FC			145.300	2400	411101.233	415218.138	2.175

### Links

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.000	S1	S2	22.127	0.600	158.943	157.502	1.441	15.4	150	5.14	46.7
1.001	S2	S3	30.508	0.600	157.427	155.354	2.073	14.7	225	5.29	46.1
1.002	S3	S4	21.722	0.600	155.354	153.803	1.551	14.0	225	5.39	45.8
1.003	S4	S5	36.299	0.600	153.784	151.020	2.764	13.1	300	5.53	45.3
1.004	S5	S6	16.354	0.600	151.020	149.385	1.635	10.0	300	5.59	45.1
1.005	S6	S7	37.946	0.600	149.385	146.512	2.873	13.2	300	5.73	44.6
2.000	S14	S7	18.154	0.600	147.480	146.587	0.893	20.3	225	5.10	46.8
1.006	S7	S11	32.056	0.600	146.362	144.616	1.746	18.4	450	5.85	44.2

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)	Pro Depth (mm)	Pro Velocity (m/s)
1.000	2.583	45.7	5.2	1.500	1.337	0.041	0.0	34	1.728
1.001	3.428	136.3	17.9	1.337	1.200	0.143	0.0	55	2.396
1.002	3.514	139.7	24.3	1.200	1.200	0.196	0.0	63	2.646
1.003	4.360	308.2	34.6	1.144	1.308	0.282	0.0	67	2.911
1.004	4.998	353.3	46.6	1.308	1.773	0.381	0.0	73	3.498
1.005	4.348	307.3	51.6	1.773	1.935	0.427	0.0	83	3.264
2.000	2.915	115.9	5.8	1.396	1.935	0.046	0.0	34	1.530
1.006	4.761	757.3	74.7	1.935	2.259	0.623	0.0	94	3.082

Links

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
3.000	S8	S11	44.573	0.600	145.310	145.049	0.261	170.8	225	5.74	44.6
4.000	S9	S11	11.691	0.600	146.010	144.841	1.169	10.0	225	5.05	47.1
1.007	S11	S12	4.833	0.600	144.466	144.454	0.012	402.8	600	5.91	44.0
1.008	S12	TANK	2.015	0.600	144.454	144.450	0.004	503.8	600	5.94	43.9
1.009	1	S13FC	2.909	0.600	143.150	143.125	0.025	116.4	600	5.02	47.1

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)	Pro Depth (mm)	Pro Velocity (m/s)
3.000	0.997	39.7	13.0	1.200	2.051	0.108	0.0	88	0.894
4.000	4.161	165.5	15.3	1.752	2.259	0.120	0.0	46	2.632
1.007	1.207	341.3	106.5	2.259	2.323	0.893	0.0	229	1.072
1.008	1.078	304.8	106.3	2.323	2.353	0.893	0.0	244	0.986
1.009	2.256	638.0	0.0	2.050	1.575	0.000	0.0	0	0.000

Pipeline Schedule

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1.000	22.127	15.4	150	Circular	160.593	158.943	1.500	158.989	157.502	1.337
1.001	30.508	14.7	225	Circular	158.989	157.427	1.337	156.779	155.354	1.200
1.002	21.722	14.0	225	Circular	156.779	155.354	1.200	155.228	153.803	1.200
1.003	36.299	13.1	300	Circular	155.228	153.784	1.144	152.628	151.020	1.308
1.004	16.354	10.0	300	Circular	152.628	151.020	1.308	151.458	149.385	1.773
1.005	37.946	13.2	300	Circular	151.458	149.385	1.773	148.747	146.512	1.935
2.000	18.154	20.3	225	Circular	149.101	147.480	1.396	148.747	146.587	1.935
1.006	32.056	18.4	450	Circular	148.747	146.362	1.935	147.325	144.616	2.259
3.000	44.573	170.8	225	Circular	146.735	145.310	1.200	147.325	145.049	2.051
4.000	11.691	10.0	225	Circular	147.987	146.010	1.752	147.325	144.841	2.259
1.007	4.833	402.8	600	Circular	147.325	144.466	2.259	147.377	144.454	2.323
1.008	2.015	503.8	600	Circular	147.377	144.454	2.323	147.403	144.450	2.353
1.009	2.909	116.4	600	Circular	145.800	143.150	2.050	145.300	143.125	1.575

Link	US Node	Dia (mm)	Node Type	MH Type	DS Node	Dia (mm)	Node Type	MH Type
1.000	S1	1200	Manhole	Adoptable	S2	1200	Manhole	Adoptable
1.001	S2	1200	Manhole	Adoptable	S3	1350	Manhole	Adoptable
1.002	S3	1350	Manhole	Adoptable	S4	1350	Manhole	Adoptable
1.003	S4	1350	Manhole	Adoptable	S5	1500	Manhole	Adoptable
1.004	S5	1500	Manhole	Adoptable	S6	1350	Manhole	Adoptable
1.005	S6	1350	Manhole	Adoptable	S7	1500	Manhole	Adoptable
2.000	S14	1200	Manhole	Adoptable	S7	1500	Manhole	Adoptable
1.006	S7	1500	Manhole	Adoptable	S11	1800	Manhole	Adoptable
3.000	S8	1200	Manhole	Adoptable	S11	1800	Manhole	Adoptable
4.000	S9	1200	Manhole	Adoptable	S11	1800	Manhole	Adoptable
1.007	S11	1800	Manhole	Adoptable	S12	1500	Manhole	Adoptable
1.008	S12	1500	Manhole	Adoptable	TANK	1200	Manhole	Adoptable
1.009	1	2100	Manhole	Adoptable	S13FC	2400	Manhole	Adoptable

### Simulation Settings

Rainfall Methodology	FSR	Analysis Speed	Normal
FSR Region	England and Wales	Skip Steady State	x
M5-60 (mm)	19.000	Drain Down Time (mins)	60
Ratio-R	0.330	Additional Storage (m <sup>3</sup> /ha)	0.0
Summer CV	0.750	Check Discharge Rate(s)	x
Winter CV	0.840	Check Discharge Volume	x

### Storm Durations

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
2	0	0	0
30	0	0	0
100	45	0	0

### Node S13FC Online StormBrake™ Control

Flap Valve	x	Design Flow (l/s)	3.5
Replaces Downstream Link	✓	Product Code	FPM-SB1-02300-00350-1100
Invert Level (m)	143.125	Min Outlet Diameter (m)	0.100
Design Depth (m)	2.300	Min Node Diameter (mm)	1200

### Node 1 Flow through Pond Storage Structure

Base Inf Coefficient (m/hr)	0.00000	Porosity	1.00	Main Channel Length (m)	22.000
Side Inf Coefficient (m/hr)	0.00000	Invert Level (m)	143.150	Main Channel Slope (1:X)	500.0
Safety Factor	2.0	Time to half empty (mins)		Main Channel n	0.600

### Inlets

TANK

Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )
0.000	300.0	0.0	2.000	300.0	0.0	2.001	0.0	0.0

### Other (defaults)

Entry Loss (manhole)	0.250	Entry Loss (junction)	0.000	Apply Recommended Losses	x
Exit Loss (manhole)	0.250	Exit Loss (junction)	0.000	Flood Risk (m)	0.300

### Rainfall

Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)
1 year 15 minute summer	97.427	27.568	1 year 180 minute summer	23.288	5.993
1 year 15 minute winter	68.370	27.568	1 year 180 minute winter	15.138	5.993
1 year 30 minute summer	65.213	18.453	1 year 240 minute summer	18.832	4.977
1 year 30 minute winter	45.763	18.453	1 year 240 minute winter	12.511	4.977
1 year 60 minute summer	45.726	12.084	1 year 360 minute summer	14.747	3.795
1 year 60 minute winter	30.379	12.084	1 year 360 minute winter	9.586	3.795
1 year 120 minute summer	29.443	7.781	1 year 480 minute summer	11.830	3.126
1 year 120 minute winter	19.561	7.781	1 year 480 minute winter	7.860	3.126

Rainfall

Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)
1 year 600 minute summer	9.836	2.690	30 year 180 minute summer	53.400	13.742
1 year 600 minute winter	6.720	2.690	30 year 180 minute winter	34.711	13.742
1 year 720 minute summer	8.880	2.380	30 year 240 minute summer	42.212	11.155
1 year 720 minute winter	5.968	2.380	30 year 240 minute winter	28.045	11.155
1 year 960 minute summer	7.450	1.962	30 year 360 minute summer	32.279	8.307
1 year 960 minute winter	4.935	1.962	30 year 360 minute winter	20.982	8.307
1 year 1440 minute summer	5.581	1.496	30 year 480 minute summer	25.473	6.732
1 year 1440 minute winter	3.750	1.496	30 year 480 minute winter	16.923	6.732
2 year 15 minute summer	126.058	35.670	30 year 600 minute summer	20.893	5.715
2 year 15 minute winter	88.462	35.670	30 year 600 minute winter	14.275	5.715
2 year 30 minute summer	84.152	23.812	30 year 720 minute summer	18.644	4.997
2 year 30 minute winter	59.054	23.812	30 year 720 minute winter	12.530	4.997
2 year 60 minute summer	58.092	15.352	30 year 960 minute summer	15.343	4.040
2 year 60 minute winter	38.595	15.352	30 year 960 minute winter	10.163	4.040
2 year 120 minute summer	36.747	9.711	30 year 1440 minute summer	11.157	2.990
2 year 120 minute winter	24.414	9.711	30 year 1440 minute winter	7.498	2.990
2 year 180 minute summer	28.735	7.394	100 year +45% CC 15 minute summer	446.880	126.452
2 year 180 minute winter	18.678	7.394	100 year +45% CC 15 minute winter	313.600	126.452
2 year 240 minute summer	23.035	6.088	100 year +45% CC 30 minute summer	303.454	85.867
2 year 240 minute winter	15.304	6.088	100 year +45% CC 30 minute winter	212.950	85.867
2 year 360 minute summer	17.901	4.607	100 year +45% CC 60 minute summer	210.766	55.699
2 year 360 minute winter	11.636	4.607	100 year +45% CC 60 minute winter	140.028	55.699
2 year 480 minute summer	14.289	3.776	100 year +45% CC 120 minute summer	131.943	34.869
2 year 480 minute winter	9.493	3.776	100 year +45% CC 120 minute winter	87.660	34.869
2 year 600 minute summer	11.831	3.236	100 year +45% CC 180 minute summer	101.403	26.094
2 year 600 minute winter	8.084	3.236	100 year +45% CC 180 minute winter	65.915	26.094
2 year 720 minute summer	10.643	2.852	100 year +45% CC 240 minute summer	79.749	21.075
2 year 720 minute winter	7.153	2.852	100 year +45% CC 240 minute winter	52.983	21.075
2 year 960 minute summer	8.877	2.338	100 year +45% CC 360 minute summer	60.567	15.586
2 year 960 minute winter	5.880	2.338	100 year +45% CC 360 minute winter	39.370	15.586
2 year 1440 minute summer	6.590	1.766	100 year +45% CC 480 minute summer	47.557	12.568
2 year 1440 minute winter	4.429	1.766	100 year +45% CC 480 minute winter	31.596	12.568
30 year 15 minute summer	238.477	67.481	100 year +45% CC 600 minute summer	38.848	10.626
30 year 15 minute winter	167.352	67.481	100 year +45% CC 600 minute winter	26.543	10.626
30 year 30 minute summer	160.302	45.360	100 year +45% CC 720 minute summer	34.545	9.258
30 year 30 minute winter	112.492	45.360	100 year +45% CC 720 minute winter	23.217	9.258
30 year 60 minute summer	110.635	29.238	100 year +45% CC 960 minute summer	28.262	7.442
30 year 60 minute winter	73.503	29.238	100 year +45% CC 960 minute winter	18.722	7.442
30 year 120 minute summer	69.224	18.294	100 year +45% CC 1440 minute summer	20.369	5.459
30 year 120 minute winter	45.991	18.294	100 year +45% CC 1440 minute winter	13.689	5.459

**Results for 1 year Critical Storm Duration. Lowest mass balance: 80.96%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute winter	S1	10	158.977	0.034	5.1	0.0388	0.0000	OK
15 minute winter	S2	10	157.482	0.055	17.8	0.0618	0.0000	OK
15 minute winter	S3	10	155.419	0.065	24.3	0.0933	0.0000	OK
15 minute winter	S4	10	153.852	0.068	34.8	0.0967	0.0000	OK
15 minute winter	S5	10	151.095	0.075	47.0	0.1326	0.0000	OK
15 minute winter	S6	10	149.470	0.085	52.5	0.1221	0.0000	OK
15 minute winter	S14	10	147.515	0.035	5.8	0.0392	0.0000	OK
15 minute winter	S7	10	146.457	0.095	76.3	0.1677	0.0000	OK
15 minute winter	S8	11	145.400	0.090	13.5	0.1020	0.0000	OK
15 minute winter	S9	10	146.058	0.048	15.1	0.0540	0.0000	OK
15 minute winter	S11	11	144.737	0.271	109.0	0.6895	0.0000	OK
15 minute winter	S12	11	144.702	0.247	108.6	0.4373	0.0000	OK
600 minute winter	TANK	480	143.590	0.396	14.0	0.4474	0.0000	OK
600 minute winter	1	480	143.590	0.440	8.5	1.5228	0.0000	OK
600 minute winter	S13FC	480	143.590	0.465	6.2	2.1019	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute winter	S1	1.000	S2	5.0	1.685	0.110	0.0661	
15 minute winter	S2	1.001	S3	17.7	2.094	0.130	0.2586	
15 minute winter	S3	1.002	S4	24.0	2.584	0.172	0.2018	
15 minute winter	S4	1.003	S5	34.6	2.704	0.112	0.4648	
15 minute winter	S5	1.004	S6	46.7	3.090	0.132	0.2472	
15 minute winter	S6	1.005	S7	51.9	3.220	0.169	0.6119	
15 minute winter	S14	2.000	S7	5.7	1.505	0.049	0.0690	
15 minute winter	S7	1.006	S11	75.9	2.770	0.100	0.9363	
15 minute winter	S8	3.000	S11	13.1	0.895	0.330	0.6523	
15 minute winter	S9	4.000	S11	15.0	2.528	0.091	0.0695	
15 minute winter	S11	1.007	S12	108.6	0.932	0.318	0.5632	
15 minute winter	S12	1.008	TANK	108.9	1.101	0.357	0.1995	
600 minute winter	TANK	Flow through pond	1	8.5	0.007	0.005	125.2958	
600 minute winter	1	1.009	S13FC	6.2	0.290	0.010	0.6625	
600 minute winter	S13FC	StormBrake™		2.8				83.0

**Results for 2 year Critical Storm Duration. Lowest mass balance: 80.96%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute winter	S1	10	158.982	0.039	6.7	0.0446	0.0000	OK
15 minute winter	S2	10	157.489	0.062	23.2	0.0706	0.0000	OK
15 minute winter	S3	10	155.429	0.075	31.7	0.1077	0.0000	OK
15 minute winter	S4	10	153.861	0.077	45.3	0.1106	0.0000	OK
15 minute winter	S5	10	151.106	0.086	61.1	0.1527	0.0000	OK
15 minute winter	S6	10	149.483	0.098	68.2	0.1405	0.0000	OK
15 minute winter	S14	10	147.519	0.039	7.5	0.0446	0.0000	OK
15 minute winter	S7	10	146.470	0.108	99.0	0.1911	0.0000	OK
15 minute winter	S8	11	145.414	0.104	17.5	0.1180	0.0000	OK
15 minute winter	S9	10	146.065	0.055	19.5	0.0618	0.0000	OK
15 minute winter	S11	11	144.778	0.312	141.3	0.7951	0.0000	OK
15 minute winter	S12	11	144.738	0.284	140.4	0.5013	0.0000	OK
600 minute winter	TANK	570	143.723	0.529	16.9	0.5986	0.0000	OK
600 minute winter	1	570	143.723	0.573	10.1	1.9857	0.0000	OK
600 minute winter	S13FC	585	143.723	0.598	5.6	2.7049	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute winter	S1	1.000	S2	6.6	1.820	0.145	0.0805	
15 minute winter	S2	1.001	S3	23.1	2.247	0.169	0.3140	
15 minute winter	S3	1.002	S4	31.3	2.773	0.224	0.2451	
15 minute winter	S4	1.003	S5	45.0	2.896	0.146	0.5648	
15 minute winter	S5	1.004	S6	60.7	3.301	0.172	0.3009	
15 minute winter	S6	1.005	S7	67.3	3.453	0.219	0.7412	
15 minute winter	S14	2.000	S7	7.4	1.619	0.064	0.0830	
15 minute winter	S7	1.006	S11	98.5	2.797	0.130	1.2911	
15 minute winter	S8	3.000	S11	17.0	0.957	0.428	0.7898	
15 minute winter	S9	4.000	S11	19.4	2.709	0.117	0.0837	
15 minute winter	S11	1.007	S12	140.4	1.005	0.411	0.6752	
15 minute winter	S12	1.008	TANK	140.8	1.190	0.462	0.2387	
600 minute winter	TANK	Flow through pond	1	10.1	0.008	0.006	165.3873	
600 minute winter	1	1.009	S13FC	5.6	0.273	0.009	0.8126	
600 minute winter	S13FC	StormBrake™		2.8				80.4

**Results for 30 year Critical Storm Duration. Lowest mass balance: 80.96%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute winter	S1	10	158.998	0.055	12.6	0.0624	0.0000	OK
15 minute winter	S2	10	157.514	0.087	43.8	0.0984	0.0000	OK
15 minute winter	S3	10	155.463	0.109	59.8	0.1553	0.0000	OK
15 minute winter	S4	10	153.892	0.108	85.6	0.1548	0.0000	OK
15 minute winter	S5	10	151.144	0.124	115.6	0.2193	0.0000	OK
15 minute winter	S6	10	149.526	0.141	129.0	0.2020	0.0000	OK
15 minute winter	S14	10	147.535	0.054	14.1	0.0616	0.0000	OK
15 minute winter	S7	10	146.512	0.150	187.7	0.2652	0.0000	OK
15 minute winter	S8	10	145.468	0.158	33.2	0.1790	0.0000	OK
15 minute winter	S9	10	146.086	0.076	36.8	0.0861	0.0000	OK
15 minute winter	S11	10	144.920	0.453	268.4	1.1541	0.0000	OK
15 minute winter	S12	11	144.857	0.403	266.8	0.7122	0.0000	OK
960 minute winter	TANK	930	144.332	1.138	21.2	1.2868	0.0000	OK
960 minute winter	1	930	144.332	1.182	11.9	4.0931	0.0000	SURCHARGED
960 minute winter	S13FC	930	144.331	1.206	6.2	5.4549	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute winter	S1	1.000	S2	12.5	2.163	0.273	0.1275	
15 minute winter	S2	1.001	S3	43.6	2.634	0.320	0.5049	
15 minute winter	S3	1.002	S4	59.2	3.257	0.424	0.3948	
15 minute winter	S4	1.003	S5	85.2	3.385	0.276	0.9143	
15 minute winter	S5	1.004	S6	114.9	3.827	0.325	0.4912	
15 minute winter	S6	1.005	S7	127.7	4.065	0.415	1.1931	
15 minute winter	S14	2.000	S7	14.0	1.938	0.121	0.1309	
15 minute winter	S7	1.006	S11	187.0	2.832	0.247	2.5641	
15 minute winter	S8	3.000	S11	32.1	1.108	0.811	1.2928	
15 minute winter	S9	4.000	S11	36.8	3.140	0.223	0.1410	
15 minute winter	S11	1.007	S12	266.8	1.240	0.782	1.0385	
15 minute winter	S12	1.008	TANK	266.4	1.463	0.874	0.3665	
960 minute winter	TANK	Flow through pond	1	11.9	0.008	0.007	347.9232	
960 minute winter	1	1.009	S13FC	6.2	0.287	0.010	0.8194	
960 minute winter	S13FC	StormBrake™		2.8				137.5

**Results for 100 year +45% CC Critical Storm Duration. Lowest mass balance: 80.96%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute winter	S1	10	159.023	0.080	23.6	0.0900	0.0000	OK
15 minute winter	S2	10	157.552	0.125	82.1	0.1412	0.0000	OK
15 minute winter	S3	10	155.522	0.168	112.2	0.2406	0.0000	OK
15 minute winter	S4	10	153.939	0.155	160.4	0.2222	0.0000	OK
15 minute winter	S5	10	151.206	0.186	216.8	0.3291	0.0000	OK
15 minute winter	S6	10	149.601	0.216	242.0	0.3096	0.0000	OK
15 minute winter	S14	10	147.556	0.076	26.5	0.0863	0.0000	OK
15 minute winter	S7	10	146.574	0.212	352.1	0.3739	0.0000	OK
15 minute winter	S8	11	145.845	0.535	62.1	0.6050	0.0000	SURCHARGED
15 minute winter	S9	10	146.111	0.101	69.0	0.1138	0.0000	OK
15 minute winter	S11	10	145.151	0.685	501.4	1.7441	0.0000	SURCHARGED
1440 minute summer	S12	1020	145.472	1.018	202.5	1.7988	0.0000	SURCHARGED
720 minute winter	TANK	525	145.090	1.896	361.0	2.1448	0.0000	OK
720 minute winter	1	525	145.095	1.945	99.7	6.7361	0.0000	SURCHARGED
720 minute winter	S13FC	510	145.096	1.971	15.8	8.9162	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute winter	S1	1.000	S2	23.4	2.534	0.512	0.2042	
15 minute winter	S2	1.001	S3	81.7	2.988	0.600	0.8303	
15 minute winter	S3	1.002	S4	110.9	3.694	0.794	0.6515	
15 minute winter	S4	1.003	S5	159.8	3.860	0.518	1.5016	
15 minute winter	S5	1.004	S6	215.5	4.289	0.610	0.8206	
15 minute winter	S6	1.005	S7	239.5	4.640	0.779	1.9615	
15 minute winter	S14	2.000	S7	26.3	2.297	0.227	0.2079	
15 minute winter	S7	1.006	S11	351.1	2.724	0.464	3.7131	
15 minute winter	S8	3.000	S11	59.5	1.497	1.499	1.7163	
15 minute winter	S9	4.000	S11	68.9	3.232	0.416	0.3329	
15 minute winter	S11	1.007	S12	497.7	1.767	1.458	1.3595	
1440 minute summer	S12	1.008	TANK	97.2	0.824	0.319	0.5673	
720 minute winter	TANK	Flow through pond	1	99.7	0.011	0.058	576.0635	
720 minute winter	1	1.009	S13FC	15.8	0.305	0.025	0.8194	
720 minute winter	S13FC	StormBrake™		3.3				124.9