

59 Market St Milnsbridge



**Planning Compliance Report
Report 22155.PCR.01**

**Derek Day
59 Market Street
Milnsbridge
Huddersfield
HD3 4HZ**

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22155.TH1	Environmental Noise Time History
22155.Daytime.LA90	Statistical analysis for representative daytime L_{A90}
22155.Night-time.LA90	Statistical analysis for representative night-time L_{A90}
Appendix A	Glossary of Acoustics Terminology
Appendix B	Acoustic Calculations
Appendix C	Anti-Vibration Mounting Specification Reference Document

1.0 INTRODUCTION

KP Acoustics Ltd has been commissioned by Derek Day, 59 Market Street, Milnsbridge, Huddersfield, HD3 4HZ to undertake a noise impact assessment of a plant unit installation serving the building at 59 Market St, Milnsbridge, Huddersfield, HD3 4HZ.

A 24 hour environmental noise survey has been undertaken on site in order to prepare a noise impact assessment in accordance with BS4142:2014 *'Method for rating and assessing industrial and commercial sound'* as part of the planning requirements of Kirklees Council.

This report presents the methodology and results from the environmental survey, followed by calculations in accordance with BS4142 to provide an indication as to the likelihood of the noise emissions from the plant unit installation having an adverse impact on the closest noise sensitive receiver. Mitigation measures will be outlined as appropriate.

2.0 SITE SURVEYS

2.1 Site Description

As shown in Figure 2.1, the site is bounded by Market Street to the east, with local businesses and residential flats to all other sides.



Figure 2.1 Site Location Plan (Image Source: Google Maps)

Initial inspection of the site revealed that the background noise profile at the monitoring location was dominated by road traffic noise from the surrounding roads.

2.2 Environmental Noise Survey Procedure

Continuous automated monitoring was undertaken for the duration of the survey between 13:33 on 16/02/2021 and 12:38 on 17/02/2021.

The environmental noise measurement position, plant installation locations, and the closest noise sensitive receiver relative to the plant installations are described within Table 2.1 and shown within Figures 2.2 and 2.3.

Icon	Descriptor	Location Description
	Noise Measurement Position	The microphone was installed on a window on the 1 st floor of the rear façade, as shown in Figure 2.1. A correction of 3dB has been applied to account for non-free field conditions
	Closest Noise Sensitive Receiver	Rear façade. 1 st Floor window. Residential flat above pub
	Proposed Plant Installation Location	Proposed plant installations are outlined in Section 5.1

Table 2.1 Measurement position and description

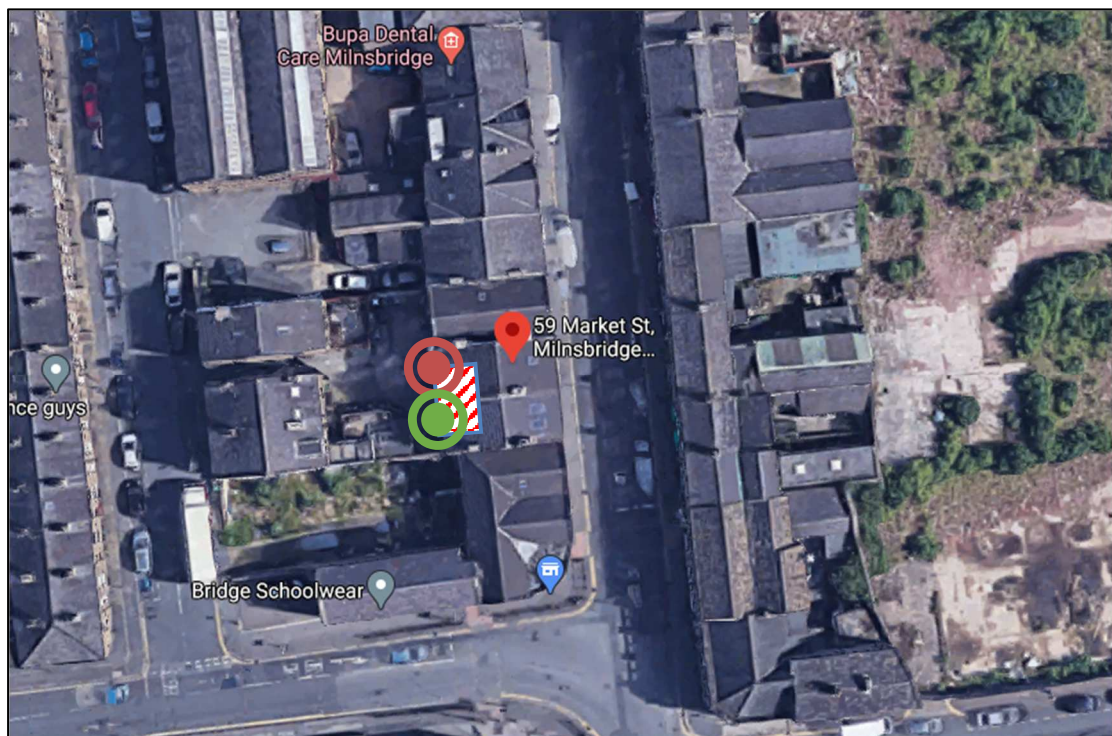


Figure 2.2 Site measurement position, identified receiver and plant unit installation (Image Source: Google Maps)



Figure 2.3 Site measurement position, identified receiver and plant unit installation (Image Source: Google Maps)

The choice of the position was based both on accessibility and on collecting representative noise data in relation to the nearest noise sensitive receiver relative to the plant installation.

Weather conditions were generally dry with light winds and therefore suitable for the measurement of environmental noise. The measurement procedure complied with ISO 1996-2:2017 Acoustics '*Description, measurement and assessment of environmental noise - Part 2: Determination of environmental noise levels*'.

2.3 Equipment

The equipment calibration was verified before and after use and no abnormalities were observed. The equipment used is described within Table 2.3.

Measurement instrumentation		Serial no.	Date	Cert no.
Noise Kit 9	Svantek Type 958A Class 1 Sound Level Meter	45578	15/07/2020	14012950
	Free-field microphone PCB 377B02	169770		
	Preamplifier PCB 426E01	128280		
	Svantek External windshield	-	-	-
Larson Davis CAL200 Class 1 Calibrator		8932	11/02/2020	04624/2

Table 2.3 Measurement instrumentation

3.0 RESULTS

The $L_{Aeq}: 5min$, $L_{Amax}: 5min$, $L_{A10}: 5min$ and $L_{A90}: 5min$ acoustic parameters were measured throughout the duration of the survey. Measured levels are shown as a time history in Figure 22155.TH1.

Representative background noise levels are shown in Table 3.1 for daytime and night-time.

It should be noted that the representative background noise level has been derived from the most commonly occurring $L_{A90,5 min}$ levels measured during the environmental noise survey undertaken on site, as shown in 22155.Daytime.LA90 and 22155.Night-time.LA90 attached.

Time Period	Representative background noise level L_{A90} dB(A)
Daytime (07:00-23:00)	49
Night-time (23:00-07:00)	35

Table 3.1 Representative background noise levels

4.0 NOISE ASSESSMENT GUIDANCE

4.1 BS4142: 2014 'Methods for rating and assessing industrial and commercial sound'

British Standard BS4142:2014 'Methods for rating and assessing industrial and commercial sound' describes a method for rating and assessing sound of an industrial and/or commercial nature, which includes:

- Sound from industrial and manufacturing processes
- Sound from fixed installations which comprise mechanical and electrical plant and equipment
- Sound from the loading and unloading of goods and materials at industrial and/or commercial premises, and
- Sound from mobile plant and vehicles that is an intrinsic part of the overall sound emanating from premises or processes.

This Standard compares the Rating Level due to the noise source/s under assessment for a one-hour period during the daytime (07:00 – 23:00 hours) and a fifteen-minute period during the night-time (23:00 – 07:00 hours) with the existing background noise level in terms of an L_{A90} when the noise source is not operating.

It should be noted that the Rating Level is the Specific Sound Level in question ($L_{Aeq, Tr}$), including any relevant acoustic feature corrections, as follows:

- **Tonality** – *‘For sound ranging from not tonal to prominently tonal the Joint Nordic Method gives a correction of between 0dB and +6dB for tonality. Subjectively, this can be converted to a penalty of 2dB for a tone which is just perceptible at the noise receptor, 4dB where it is clearly perceptible, and 6dB where it is highly perceptible’*
- **Impulsivity** – *‘A correction of up to +9dB can be applied for sound that is highly impulsive, considering both the rapidity of the change in sound level and the overall change in sound level. Subjectively, this can be converted to a penalty of 3dB for impulsivity which is just perceptible at the noise receptor, 6dB where it is clearly perceptible, and 9dB where it is highly perceptible’*
- **Intermittency** – *‘If the intermittency is readily distinctive against the residual acoustic environment, a penalty of 3dB can be applied’*
- **Other sound characteristics** – *‘Where the specific sound features characteristics that are neither tonal nor impulsive, though otherwise are readily distinctive against the residual acoustic environment, a penalty of 3dB can be applied’*

Once the Rating Level has been obtained, the representative background sound level is subtracted from the Rating Level to obtain an initial estimate of the impact, as follows:

- Typically, the greater this difference, the greater the magnitude of the impact
- A difference of around +10 dB or more is likely to be an indication of a significant adverse impact, depending on the context
- A difference of around +5 dB could be an indication of an adverse impact, depending on the context
- The lower the rating level is relative to the measured background sound level, the less likely it is that there will be an adverse impact or significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound having a low impact, depending on the context

NOTE: Adverse impacts may include but not be limited to annoyance and sleep disturbance. Not all adverse impacts will lead to complaints and not every complaint is proof of an adverse impact.

The initial estimate of the impact may then be modified by taking consideration of the context in which the sound occurs.

4.2 Local Authority Guidance

The criterion of Kirklees Council for noise emissions of new plant in this instance is as follows:

“Where the potential for noise disturbance exists, a noise impact assessment should be carried out at the façade of the closest noise sensitive premises to demonstrate that a Comparative Criterion has been met:

Recommended Maximum sound levels should be based upon a Comparative Criterion:

- *The Rating Level (calculated in accordance to BS 4142: 2014) is at least 10dB below the existing Ambient noise level (L_{Aeq});*
- *The Rating Level (calculated in accordance to BS 4142: 2014) is at least 0-5dB below the existing Background noise level (L_{A90});*
- *Between the hours of 19:00 and 07:00, the maximum noise levels (L_{AFmax}) from the guidance document shall not exceed the L_{A90} by more than 10dB; however, where the existing background noise level is 45 dB L_{A90} or less, the maximum noise levels shall not exceed 60 dB L_{AFmax} .*

Assessment methodology and evaluation shall normally follow the guidance in BS4142: 2014, ‘Method for Rating and Assessing Industrial and Commercial Sound’.”

4.3 Noise Emissions Criterion

As the plant units could be used at any time of the day or night, the criterion has been set as shown in Table 4.1 in order to comply with the above requirements.

Time period	Noise Criterion at Nearest Residential Receiver
Night-time (23:00 to 07:00)	30 dB(A)

Table 4.1 Plant noise emissions criterion

5.0 NOISE IMPACT ASSESSMENT

5.1 Plant Installations

It is understood that the plant installation is comprised of the following units:

- 1 No. Condenser Unit

The installation location for the condenser unit is at the rear façade at ground floor level, within an enclosed external area, as shown in Figure 2.2 and 2.3 above. It is understood that there is a beer chiller, which is inactive. This has not been assessed, as it is not to be used.

There is additionally a kitchen extract venting externally at the rear of the property. It is understood that this plant already has planning permission, and was assessed as part of the existing noise climate in report reference 22155.NIA.01 Rev B, dated 14/03/2021.

The noise emission levels for the units as provide by the manufacturer are shown in Table 5.1.

Unit	Descriptor	Octave Frequency Band (Hz)								Overall (dBA)
		63	125	250	500	1k	2k	4k	8k	
Condenser Unit	SPL@1m (dB)	64	59	56	55	52	49	41	53	58

Table 5.1 Plant Units Noise Emission Levels as provided by the manufacturer

5.2 Closest Noise Sensitive Receiver

The closest noise sensitive receiver to the installation location has been identified as being a 1st floor residential window of the property above the pub, located approximately 2 metres from the plant installation location, as shown in Figure 2.2 and 2.3.

5.3 Calculations

The 'Rating Level' of each plant unit installation has been calculated at 1m from the closest receiver using the noise levels shown in Table 5.1, and corrected due to different acoustic propagation features such as distance, reflective surfaces, screening elements, etc.

Acoustic feature corrections as per BS4142 have been applied for intermittency.

Detailed calculations for each plant unit installation are shown in Appendix B.

Receiver	Criterion	Noise Level at 1m From the Closest Noise Sensitive Window
Rear façade. 1 st Floor window. Residential flat above pub	30dB(A)	25dB(A)

Table 5.2 Predicted noise level and criterion at nearest noise sensitive location

As shown in Appendix B and Table 5.2, transmission of noise to the nearest sensitive windows due to the effects of the plant unit installation satisfies the emissions criterion of Kirklees Council, providing that the mitigation measures outlined in Section 6 are implemented.

6.0 NOISE CONTROL MEASURES

In order to achieve the specific sound level and subsequent rating level shown in the assessment above, the following noise control strategy should be adopted.

6.1 Condenser Unit Installed

The unit is currently in a wooden structure, with some holes at the top, between the stairs to the residential units above the pub and the unit. In order to control the noise emissions from the condenser unit installed we would recommend that the structure is made good with timber of at least 12kg/m³, so that there are no gaps in the structure directly above the unit, and there is no line of sight to the window from the unit. The structure, when made good in this way will be sufficient to control the plant noise levels.

7.0 CONCLUSION

An environmental noise survey has been undertaken at 59 Market St, Milnsbridge, Huddersfield, HD3 4HZ by KP Acoustics Ltd between 13:33 on 16/02/2021 and 12:38 on 17/02/2021. The results of the survey have enabled a representative background noise level to be set.

Manufacturer's noise data of plant units has been used to obtain Specific and Rated Noise Level at the nearest noise sensitive receiver in accordance with British Standard BS4142:2014 for compliance with Kirklees Council requirements.

The rating level was compared with the representative background noise level to assess the likelihood of impact considering the environmental noise context of the area as per the requirements of BS4142:2014.

It has been concluded that noise emissions from the plant units would not have an adverse impact on the nearest residential receivers provided that the noise control strategy presented in Section 6 is followed.

59 Market St, Milnsbridge, Huddersfield, HD3 4HZ
Environmental Noise Time History
From 16 February 2021 To 17 February 2021

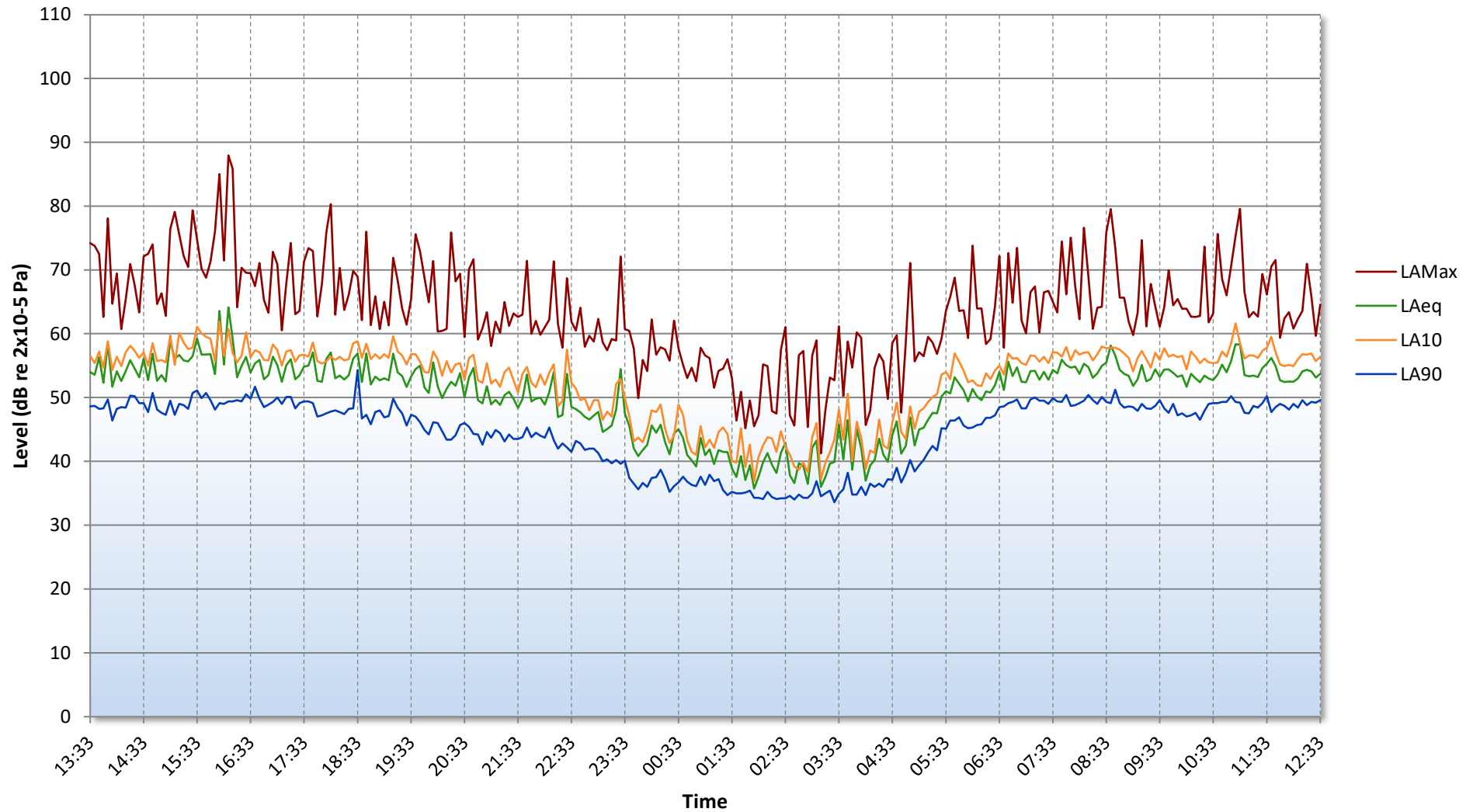


Figure 22155.TH2

59 Market St, Milnsbridge, Huddersfield, HD3 4HZ
Representative Daytime Background Noise Level
From 16 February 2021 To 17 February 2021

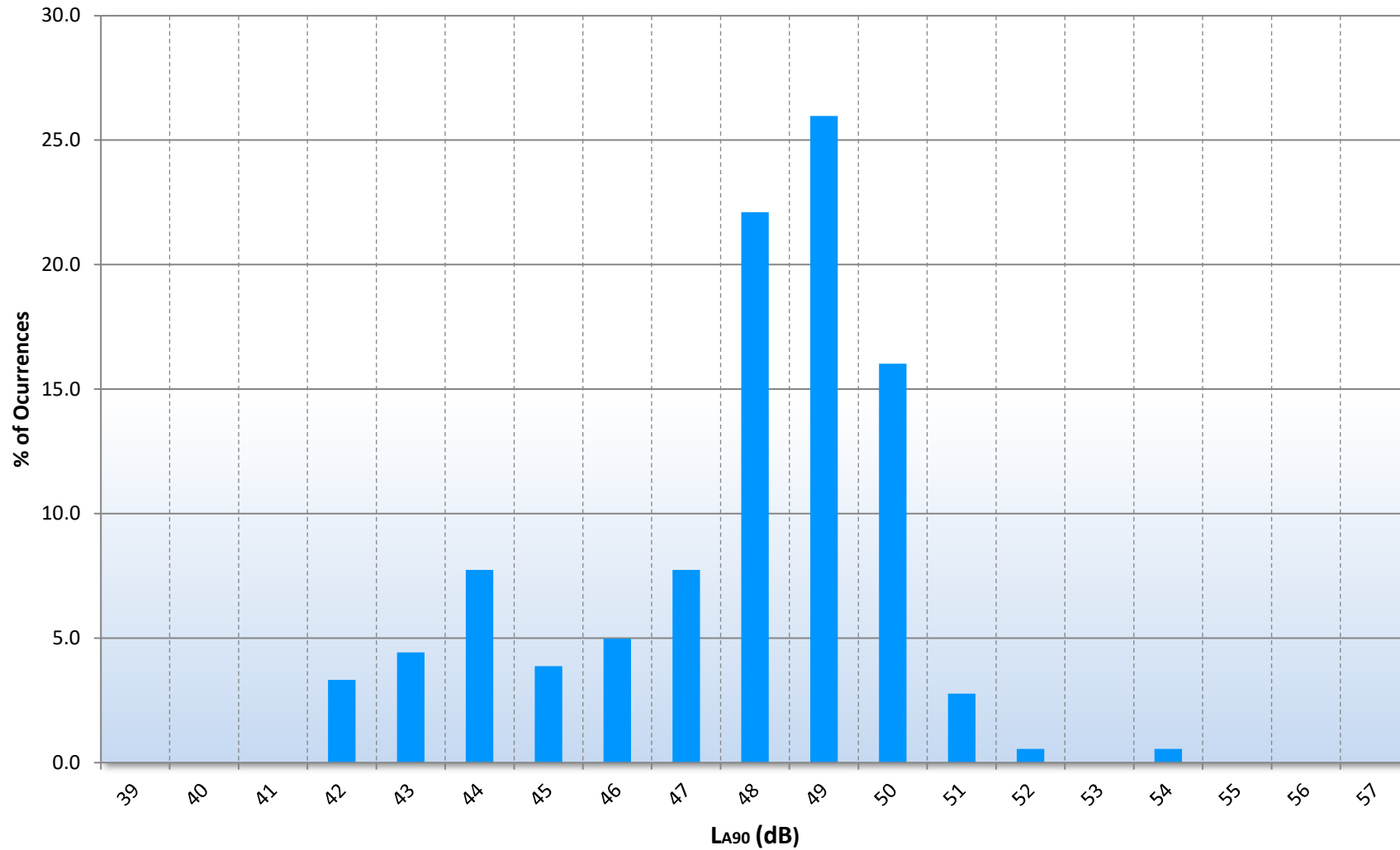


Figure 22155.L90

59 Market St, Milnsbridge, Huddersfield, HD3 4HZ
Representative Night-time Background Noise Level
From 16 February 2021 To 17 February 2021

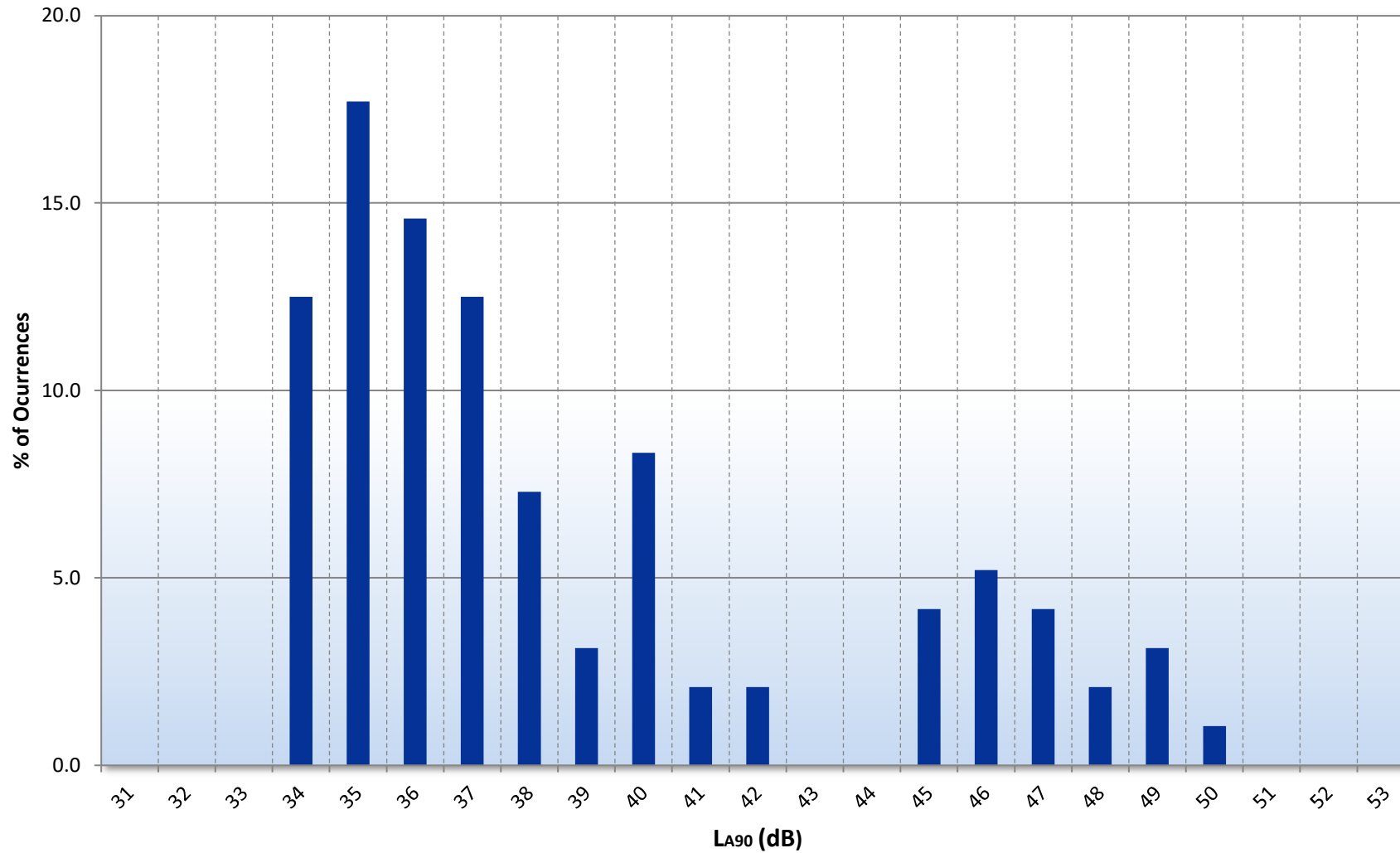


Figure 22155.L90

GENERAL ACOUSTIC TERMINOLOGY

Decibel scale - dB

In practice, when sound intensity or sound pressure is measured, a logarithmic scale is used in which the unit is the 'decibel', dB. This is derived from the human auditory system, where the dynamic range of human hearing is so large, in the order of 10^{13} units, that only a logarithmic scale is the sensible solution for displaying such a range.

Decibel scale, 'A' weighted - dB(A)

The human ear is less sensitive at frequency extremes, below 125Hz and above 16Khz. A sound level meter models the ears variable sensitivity to sound at different frequencies. This is achieved by building a filter into the Sound Level Meter with a similar frequency response to that of the ear, an A-weighted filter where the unit is dB(A).

L_{eq}

The sound from noise sources often fluctuates widely during a given period of time. An average value can be measured, the equivalent sound pressure level L_{eq} . The L_{eq} is the equivalent sound level which would deliver the same sound energy as the actual fluctuating sound measured in the same time period.

L_{10}

This is the level exceeded for no more than 10% of the time. This parameter is often used as a "not to exceed" criterion for noise.

L_{90}

This is the level exceeded for no more than 90% of the time. This parameter is often used as a descriptor of "background noise" for environmental impact studies.

L_{max}

This is the maximum sound pressure level that has been measured over a period.

Octave Bands

In order to completely determine the composition of a sound it is necessary to determine the sound level at each frequency individually. Usually, values are stated in octave bands. The audible frequency region is divided into 11 such octave bands whose centre frequencies are defined in accordance with international standards. These centre frequencies are: 16, 31.5, 63, 125, 250, 500, 1000, 2000, 4000, 8000 and 16000 Hertz.

Environmental noise terms are defined in BS7445, *Description and Measurement of Environmental Noise*.

APPLIED ACOUSTIC TERMINOLOGY

Addition of noise from several sources

Noise from different sound sources combines to produce a sound level higher than that from any individual source. Two equally intense sound sources operating together produce a sound level which is 3dB higher than a single source and 4 sources produce a 6dB higher sound level.

Attenuation by distance

Sound which propagates from a point source in free air attenuates by 6dB for each doubling of distance from the noise source. Sound energy from line sources (e.g. stream of cars) drops off by 3dB for each doubling of distance.

Subjective impression of noise

Hearing perception is highly individualised. Sensitivity to noise also depends on frequency content, time of occurrence, duration of sound and psychological factors such as emotion and expectations. The following table is a guide to explain increases or decreases in sound levels for many scenarios.

Change in sound level (dB)	Change in perceived loudness
1	Imperceptible
3	Just barely perceptible
6	Clearly noticeable
10	About twice as loud

Transmission path(s)

The transmission path is the path the sound takes from the source to the receiver. Where multiple paths exist in parallel, the reduction in each path should be calculated and summed at the receiving point. Outdoor barriers can block transmission paths, for example traffic noise. The effectiveness of barriers is dependent on factors such as its distance from the noise source and the receiver, its height and construction.

Ground-borne vibration

In addition to airborne noise levels caused by transportation, construction, and industrial sources there is also the generation of ground-borne vibration to consider. This can lead to structure-borne noise, perceptible vibration, or in rare cases, building damage.

Sound insulation - Absorption within porous materials

Upon encountering a porous material, sound energy is absorbed. Porous materials which are intended to absorb sound are known as absorbents, and usually absorb 50 to 90% of the energy and are frequency dependent. Some are designed to absorb low frequencies, some for high frequencies and more exotic designs being able to absorb very wide ranges of frequencies. The energy is converted into both mechanical movement and heat within the material; both the stiffness and mass of panels affect the sound insulation performance.

APPENDIX B

59 Market St, Milnsbridge, Huddersfield, HD3 4HZ

PLANT NOISE EMISSIONS CALCULATIONS

Source: Plant at Rear of Pub Use	Frequency, Hz								dB(A)
Receiver: 1st Floor Window Above Pub	63	125	250	500	1k	2k	4k	8k	
Fujitsu AOYG14LMCA (Sound Pressure Level @1m)	33	37	48	48	45	43	39	28	50
Minimum attenuation provided by distance (2m), dB	-6	-6	-6	-6	-6	-6	-6	-6	
Attenuation provided by proposed acoustic enclosure, dB	-12	-15	-18	-21	-24	-25	-25	-25	
BS4142 Acoustic Feature Corrections									
Tonality	0	0	0	0	0	0	0	0	
Impulsivity	0	0	0	0	0	0	0	0	
Intermittency	3	3	3	3	3	3	3	3	
Sound Pressure Level at Receiver due to All Units, dB	18	19	27	24	18	15	11	0	25

Design Criterion	30
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ANTI-VIBRATION MOUNTING SPECIFICATION REFERENCE DOCUMENT

1.0 General

- 1.1 All mountings shall provide the static deflection, under the equipment weight, shown in the schedules. Mounting selection should allow for any eccentric load distribution or torque reaction, so that the design deflection is achieved on all mountings under the equipment, under operating conditions.
- 1.2 It is the supplier's responsibility to ensure that all mountings offered are suitable for the loads, operating and environmental conditions which will prevail. Particular attention should be paid to mountings which will be exposed to atmospheric conditions to prevent corrosion.
- 1.3 All mountings shall be colour coded, or otherwise marked, to indicate their load capacity, to facilitate identification during installation.

Where use of resilient supports allows omission of pipe flexible connections for vibration/noise isolation, it shall be the Mechanical Service Consultant's or Contractor's responsibility to decide whether such devices are required to compensate for misalignment or thermal strain.

2.1 Type A Mounting (Caged Spring Type)

- 2.1.1 Each mounting shall consist of cast or fabricated telescopic top and bottom housings enclosing one or more helical steel springs as the principle isolation elements, and shall incorporate a built-in levelling device. The housing should be designed to permit visual inspection of the springs after installation, i.e. the spring must not be totally enclosed.
- 2.1.2 The springs shall have an outside diameter of not less than 75% of the operating height, and be selected to have at least 50% overload capacity before becoming coil-bound.
- 2.1.3 The bottom plate of each mounting shall have bonded to it a rubber/neoprene pad designed to attenuate any high frequency energy transmitted by the springs.
- 2.1.4 Mountings incorporating snubbers or restraining devices shall be designed so that the snubbing, damping or restraining mechanism is capable of being adjusted to have no significant effect during the normal running of the isolated machine.
- 2.1.5 All nuts, bolts or other elements used for adjustment of a mounting shall incorporate locking mechanisms to prevent the isolator going out of adjustment as a result of vibration or accidental or unauthorised tampering.

2.2 Type B Mounting (Open Spring Type)

- 2.2.1 Each mounting shall consist of one or more helical steel springs as the principal isolation elements, and shall incorporate a built-in levelling device.
- 2.2.2 The springs shall be fixed or otherwise securely located to cast or fabricated top and bottom plates, shall have an outside diameter of not less than 75% of the operating height, and shall be selected to have at least 50% overload capacity before becoming coil-bound.
- 2.2.3 The bottom plate shall have bonded to it a rubber/ neoprene pad designed to attenuate any high frequency energy transmitted by the springs.

2.3 Type C Mounting (Rubber/Neoprene Type)

Each mounting shall consist of a steel top plate and base plate completely embedded in oil resistant rubber/neoprene. Each mounting shall be capable of being fitted with a levelling device, and should have bolt holes in the base plate and a threaded metal insert in the top plate so that they can be bolted to the floor and equipment where required.

3.0 Plant Bases

3.1 Type A Bases (A.V. Rails)

An A.V. Rail shall comprise a steel beam with two or more height-saving brackets. The steel sections must be sufficiently rigid to prevent undue strain in the equipment and if necessary should be checked by the Structural Engineer.

3.2 Type B Bases (Steel Plant Bases)

Steel plant bases shall comprise an all-welded steel framework of sufficient rigidity to provide adequate support for the equipment, and fitted with isolator height saving brackets. The frame depth shall be approximately 1/10 of the longest dimension of the equipment with a minimum of 150 mm. This form of base may be used as a composite A.V. rail system.

3.3 Type C Bases (Concrete Inertia Base: for use with steel springs)

These shall consist of an all-welded steel pouring frame-work with height saving brackets, and a frame depth of approximately 1/12 of the longest dimension of the equipment, with a minimum of 100 mm. The bottom of the pouring frame should be blanked off, and concrete (2300 kg/m³) poured in over steel reinforcing rods positioned 35 mm above the bottom. The inertia base should be sufficiently large to provide support for all parts of the equipment, including any components which over-hang the equipment base, such as suction and discharge elbows on centrifugal pumps.