

DESIGN CALCULATIONS FOR PROPOSED FOUL WATER PUMPING STATION FOR WHITECHAPEL ROAD, CLECKHEATON

ON BEHALF OF



PDAS Ltd

Pump Design and Services Ltd

Date: May '22
Ref: 6711



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	Project:	6711	Calcs by:	AK
	Job No:	Whitechapel Road, Cleckheaton	Chkd by:	JAK
	Client:	PDAS	Date:	02.05.22

DESIGN BRIEF

These design calculations cover the design of the wet well, inlet chamber, valve chamber and the cover slabs to the Foul Water pumping station.

The following calculations have been prepared to ensure that the inlet chamber, wet well and valve chambers do not become buoyant in certain conditions. These being in the permanent condition, when the tank may be considered empty. Long term ground water monitoring has not been undertaken therefore water is considered at worst case of being at ground level; for this condition we have assessed the tank against a factor of safety of 1.1. The chambers have also been assessed against the temporary condition during the construction phase to ensure that the chambers do not become buoyant. For the temporary condition we have assessed the chambers against a factor of safety of 1.0.

The design of the tank has been assessed to ensure that the allowable bearing capacity is not exceeded in the permanent condition with the tank 90% full of water. Ground conditions are Mudstones for deeper chambers. The allowable bearing capacity of this site has been taken as 100kPa. These values are based on Phase I and II Geo-environmental Report, Whitechapel Road, Cleckheaton, Ref: 17036/139, dated August 2018.

The cover slabs have been designed to the chambers to ensure that they do not fail under an accidental wheel load applied.

REFERENCES

- Sewers for Adoption – 6th Edition including interim technical addendum No.1
- BS 5911-6: 2004 +A1:2010 Concrete pipes and ancillary concrete products — Part 6: Specification for road gullies and gully cover slabs.
- BS 8110-1:1997 Structural use of concrete. Code of practice for design and construction
- Phase I and II Geo-environmental Report, Whitechapel Road, Cleckheaton, Ref: 17036/139, dated August 2018.



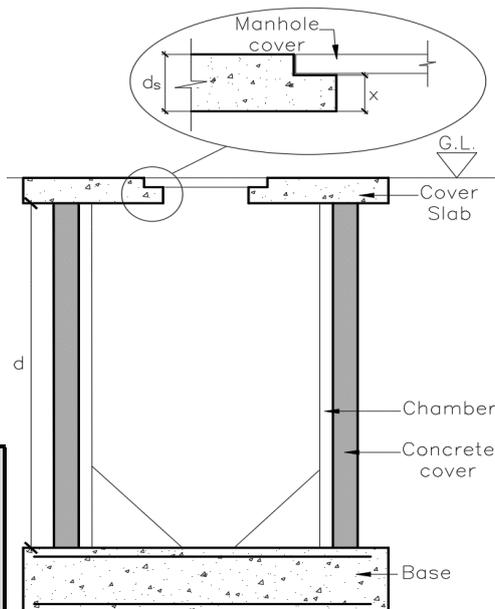
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 Job No: Whitechapel Road, Cleckheaton
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 Chkd by: JAK
 Date: 02.05.22

Wet Well Design (Worst case)

Chamber	
Wall thickness:	150 mm
Concrete cover:	200 mm
Internal diameter:	2700 mm
Depth (d):	4450 mm
Concrete γ	24 kN/m ³
Base	
Depth:	750 mm
Length:	3600 mm
Width:	3600 mm
Cover Slab	
Depth (d _s):	350 mm
Length:	3600 mm
Width:	3600 mm
Void Length:	1500 mm
Void Width:	900 mm
Void Depth (x):	210 mm
Ground Conditions	
Water Table:	0.0 m
ABP:	100 kN/m ²

Checks	
Floatation:	ACCEPTABLE (Perm)
Bearing:	ACCEPTABLE
Rebar required:	975 mm ² /m
Provide:	3 layers A393 mesh top and bottom A _{sprov} = 1179 mm ² /m



Floatation	
external diameter=	3.40 m
Volume of water displaced	= 57.8 m ³
∴ mass of water displaced	= 567.4 kN
self weight of chamber	= 702.2 kN
FoS against floatation	= $\frac{\text{self weight} \times 0.9}{\text{mass of water displaced}}$ = $\frac{632.0}{567.4}$ = 1.11
1.11 > 1.1	∴ ACCEPTABLE against floatation
Bearing	
self weight of chamber empty	= 702.2
Assuming 90% full of water	= 225.0
Total	= 927.1 kN
GBP	= 71.5 kN/m ²
71.5 < 100 kN/m ²	∴ ACCEPTABLE in bearing
Reinforcement	
ULS	= 983.1 kN
w	= 75.9 kN
M _{ult}	= 34.3 kNm
d	= 660 mm
A _s	= 126 mm ² /m
A _{smin}	= 975 mm ² /m



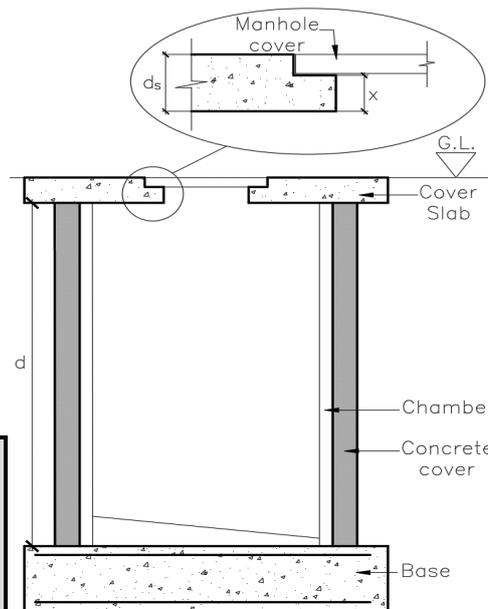
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Inlet Manhole Design

Chamber	
Wall thickness:	105 mm
Concrete cover:	150 mm
Internal diameter:	1500 mm
Depth (d):	2655 mm
Concrete γ	24 kN/m ³
Base	
Depth:	300 mm
Length:	2200 mm
Width:	2200 mm
Cover Slab	
Depth (d _s):	350 mm
Length:	2300 mm
Width:	2300 mm
Void Length:	675 mm
Void Width:	675 mm
Void Depth (x):	180 mm
Ground Conditions	
Water Table:	0.0 m
ABP:	100 kN/m ²

Checks	
Floatation:	ACCEPTABLE (Perm)
Bearing:	ACCEPTABLE
Rebar required:	390 mm ² /m
Provide:	1 layers A393 mesh top and bottom A _{sprov} = 393 mm ² /m



Floatation	
external diameter=	2.01 m
Volume of water displaced	= 12.8 m ³
∴ mass of water displaced	= 125.9 kN
self weight of chamber	= 166.9 kN
	temp = 124.4 kN
FoS against floatation	= $\frac{\text{self weight}}{\text{mass of water displaced}} = \frac{166.9}{125.9} = 1.33$
(Perm) 1.33 > 1.1	∴ ACCEPTABLE against floatation
Bearing	
self weight of chamber empty	= 166.9
Assuming 90% full of water	= 41.4
Total	= 208.3 kN
GBP	= 43.0 kN/m ²
43.0 < 100 kN/m ²	∴ ACCEPTABLE in bearing
Reinforcement	
ULS	= 233.7 kN
w	= 48.3 kN
M _{ult}	= 6.7 kNm
d	= 210 mm
A _s	= 78 mm ² /m
A _{smin}	= 390 mm ² /m



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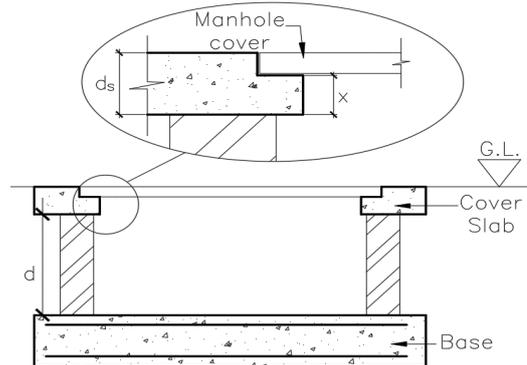
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 Chkd by: JAK
 Date: 02.05.22

Valve Chamber Design

Chamber	
Wall thickness:	215 mm
Internal diameters:	1800 mm
by	2400 mm
Depth (d):	1450 mm
Brickwork γ	22 kN/m ³
Base	
Depth:	300 mm
Length:	3000 mm
Width:	2400 mm
Cover Slab	
Depth (d _s):	350 mm
Length:	3600 mm
Width:	3000 mm
Void Length:	2400 mm
Void Width:	1800 mm
Void Depth (x):	180 mm
Ground Conditions	
Water Table:	0.0 m
ABP:	100 kN/m ²
Surcharge:	10.0 kN/m ²
ϕ' :	22 °
γ :	18 kN/m ²

Checks	
Floatation:	ACCEPTABLE (Perm)
Bearing:	ACCEPTABLE
Rebar required:	390 mm ² /m
Provide:	1 layer A393 mesh top and bottom $A_{sprov} = 393 \text{ mm}^2/\text{m}$
Masonry Panel:	ACCEPTABLE

Mortar class:	I (M12)
Masonry unit:	clay bricks (absorption <7%)



Floatation	
Volume of water displaced	= 17.3 m ³
\therefore mass of water displaced	= 169.7 kN
self weight of chamber	= 187.4 kN
temp	= 115.3 kN
FoS against floatation	= $\frac{\text{self weight}}{\text{mass of water displaced}} = \frac{187.4}{169.7} = 1.10$
(Perm)	1.10 > 1.1 \therefore ACCEPTABLE against floatation
Bearing	
self weight of chamber empty	= 187.4
Assuming 90% full of water	= <u>57.9</u>
Total	= 245.3 kN
GBP	= 34.1 kN/m ²
34.1	< 100 kN/m ² \therefore ACCEPTABLE in bearing
Reinforcement	
ULS	= 262.4 kN
w	= 36.4 kN
M _{ult}	= 13.0 kNm
d	= 210 mm
A _s	= 150 mm ² /m
A _{smin}	= 390 mm ² /m



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Wall design

$$\begin{aligned}K_a &= 0.45 \\K_o &= 0.63 \\P_{a(ULS)} &= 22.9 \\P_{s(ULS)} &= \underline{10.0} \\&= 32.9 \text{ kN/m}^2 \\h/l &= 0.60 \\\mu &= 0.35 \\therefore \alpha &= 0.024\end{aligned}$$

Design bending moment for panel:

$$\begin{aligned}a) \text{ perpendicular to bed joints} &= 4.61 \text{ kNm} \\b) \text{ parallel to bed joints} &= 1.61 \text{ kNm}\end{aligned}$$

$$\begin{aligned}f_{kx} &= 2.0 \text{ N/mm}^2 \\V_m &= 3.0 \\z &= 7.7 \text{ mm}^3\end{aligned}$$

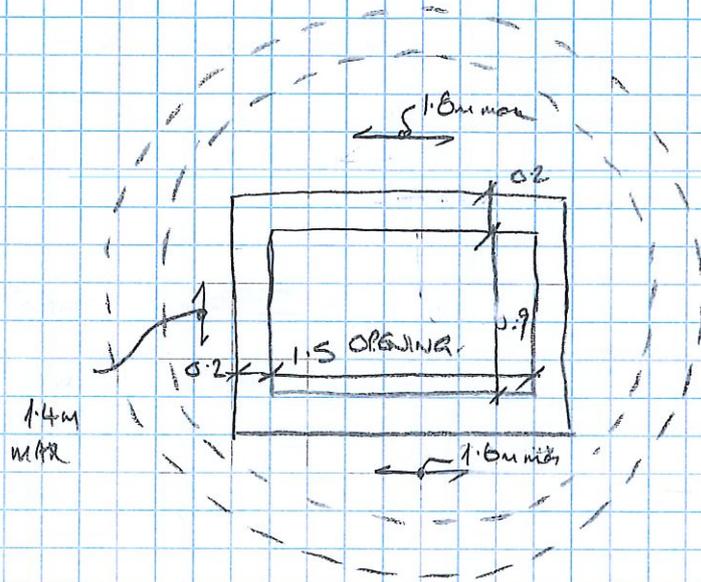
Moment resistance of panel:

$$M_R = 5.1 \text{ kNm}$$

$$5.1 > 4.61 \text{ kNm} \quad \therefore \text{ACCEPTABLE}$$

Project W...	Job No.	Date	Page No. PS/01	Rev	
Member/Location COVER SLABS		Engineer JAK	Checked		

COVER SLABS



IL: 10 kN/m² basic + A
construction loading
A = 100 kN



COVER SLAB RECESSED FOR
ACCESS LID ~ 2.0kN/m² IL

• Check shear in ribs

Assume worst case load carried on 2 opposite sides only
ult = (1.4 × 2.0 + 1.6 × 1.0) × 1.8/2 = 12.2 kN/m run each side

d = 140 - 30 - 10/2 = 105mm try H8 bars @ 100² A_{ps} = 503mm²/m

$$v = \frac{12.2 \cdot 10^3}{1000 \cdot 105} = \underline{0.12 \text{ N/mm}^2}$$

$$\frac{100 A_s}{bd} = \frac{100 \cdot 503}{1000 \cdot 105} = \underline{0.48} < 3.0 \therefore \text{OK}$$

$$\frac{400}{d} = \frac{400}{105} = \underline{3.8} \quad \left(\frac{p_{cu}}{25}\right)^{1/3} = \left(\frac{40}{25}\right)^{1/3} = \underline{1.17}$$

$$v_c = 0.79 (0.48)^{1/3} \cdot (3.8)^{1/4} \cdot \frac{1.17}{1.25}$$

$$= \underline{0.81 \text{ N/mm}^2} \gg 0.12 \text{ N/mm}^2 \therefore \text{Adequate in shear}$$

Project L3	Job No.	Date	Page No. PS/02	Rev	
	Member/Location COVER SLAB	Engineer DARK	Checked		

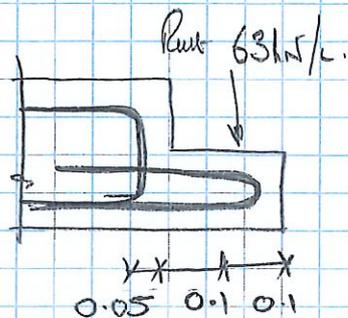
Central PL = 100kN curved on opposite edges

$$\text{ult load} = (1.6 \times 100/2 + 1.4 \times 2.0 \times 1.3/2) = \underline{82 \text{ kN}}$$

$$\text{short edge } 1.8 \text{ m lg} \Rightarrow \frac{82}{1.3} = \underline{63 \text{ kN/m equivalent line load}}$$

$$D = \frac{63 \cdot 10^3}{10^3 \times 105} = 0.6 \text{ N/mm}^2 < D_c (0.81) \therefore \text{Adequate}$$

Nib Bending



$$M_{ult} = 63 \times 0.15 = \underline{9.45 \text{ kNm}}$$

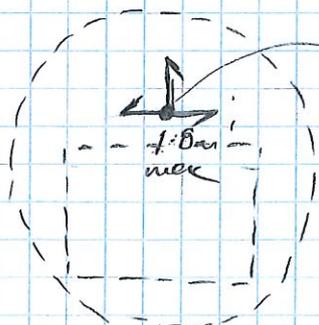
$$\frac{M}{bd^2} = \frac{9.45 \cdot 10^6}{1000 \cdot 105^2} = 0.857 \Rightarrow \underline{z = 0.95d}$$

$$A_{sreq} = \frac{9.45 \cdot 10^6}{0.87 \times 500 \times 0.95 \cdot 105} = \underline{218 \text{ mm}^2/\text{m RUA}}$$

$$A_{smin} = 0.13 \frac{bh}{100} = 182 \text{ mm}^2/\text{m} < A_{sreq}$$

$$\underline{A_{sprov} = 503 \text{ mm}^2/\text{m} > A_{sreq} \therefore \text{Adequate}}$$

Core Slab Bending



Ignore benefits of side support for general loading

$$DL = 0.3 \times 24 = 7.2 \text{ kN/m}^2$$

$$\text{ult} = (1.4 \times 7.2 + 1.6 \times 10) = \underline{26.1 \text{ kN/m}^2}$$

$$M_{ult} = 26.1 \times 1.8^2/6 \times 1 = \underline{10.6 \text{ kNm}}$$

Project	Job No.	Date	Page No. Ps) 03	Rev	
	Member/Location COVER SLAB	Engineer JMK	Checked		

Point load condition:

$$M_{ult} = 1.4 \times 7.2 \times \frac{1.8^2}{8} + 1.6 \times 100 \times \frac{1.8}{4} = 4 + 72 = \underline{76 \text{ kN}}$$

$$d = 300 - 35 - 20/2 = 255 \text{ mm}$$

$$\frac{M}{bd^2} = \frac{76 \cdot 10^6}{1000 \cdot 255^2} = \underline{1.17} \quad \Rightarrow \quad k = 0.029$$

$$\therefore z = 0.95d$$

$$A_{s, req} = \frac{76 \cdot 10^6}{0.87 \cdot 500 \cdot 0.95 \cdot 255} = \underline{721 \text{ mm}^2/\text{m}}$$

$$A_{s, min} = 0.13 \cdot 1000 \cdot \frac{255}{100} = \underline{332 \text{ mm}^2/\text{m}} < A_{s, req}$$

use 4/12 bars @ 100'c

$$\underline{A_{s, prov} = 1131 \text{ mm}^2/\text{m}} > A_{s, req} \quad \cdot \quad \text{Adequate}$$

$$f_s = \frac{2}{3} \times \frac{721}{1131} \cdot 500 = \underline{212 \text{ N/mm}^2}$$

$$m_f = 0.55 + \frac{(477 - 212)}{120(1.17 + 0.9)} = \underline{1.62}$$

$$\text{allowable } s_{p/d} = 20m_f = 20 \times 1.62 = 32$$

$$\text{actual } s_{p/d} = \frac{1800}{255} = \underline{7} < 32 \therefore \text{Adequate}$$

Shear check:

$$V_{ult} = (1.4 \times 7.2 \times \frac{1.8}{2} + 1.6 \times 100/2) = \underline{89 \text{ kN}}$$

$$V = \frac{89 \cdot 10^3}{1000 \cdot 255} = \underline{0.34 \text{ N/mm}^2}$$

$$v_c = 0.79 (0.44)^{1/3} \cdot (1.57)^{1/4} \cdot \frac{1.17}{1.25}$$

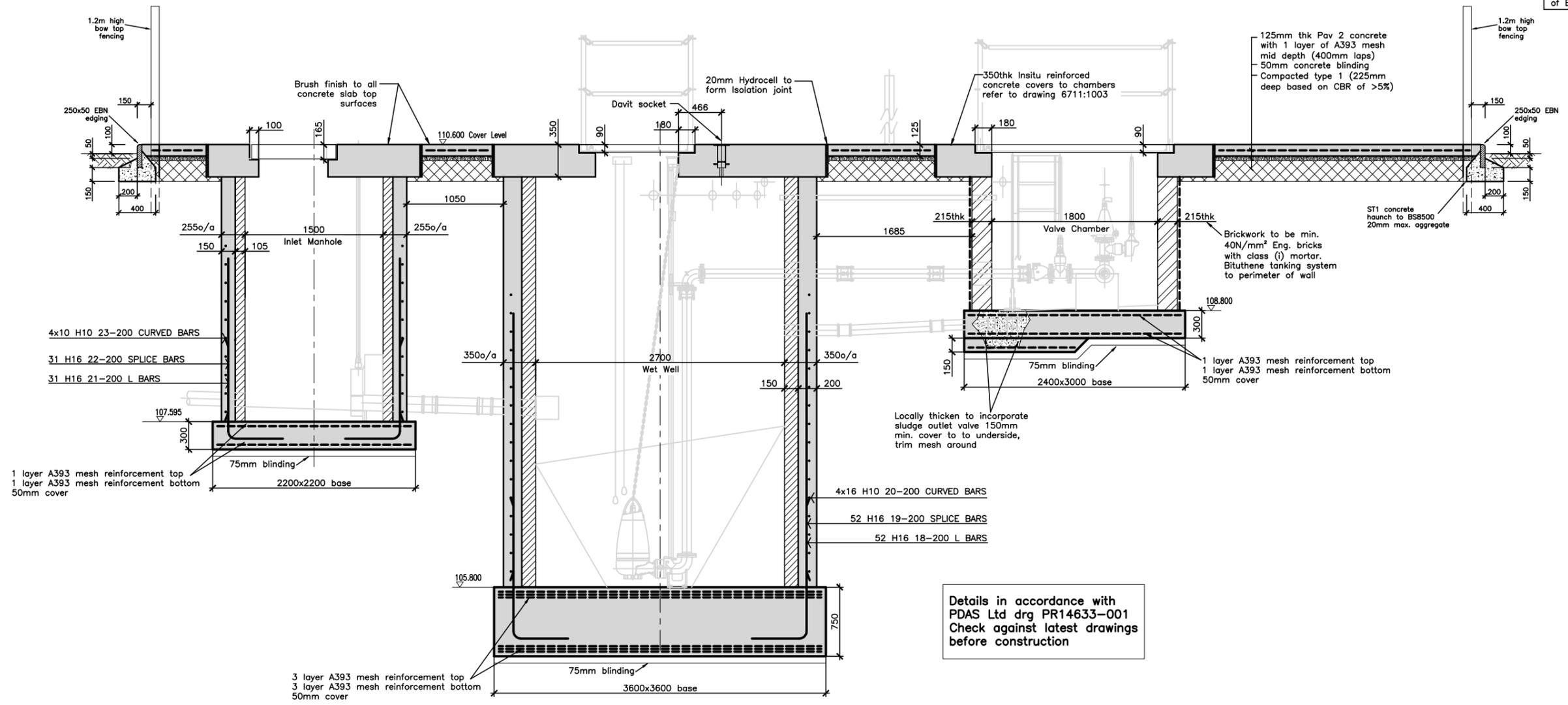
$$= \underline{0.63 \text{ N/mm}^2} > 0.34 \text{ N/mm}^2 \therefore \text{Adequate for shear}$$

Pumping equipment as specified and detailed by PDAS Ltd.

Minimum Laps for Reinforcement

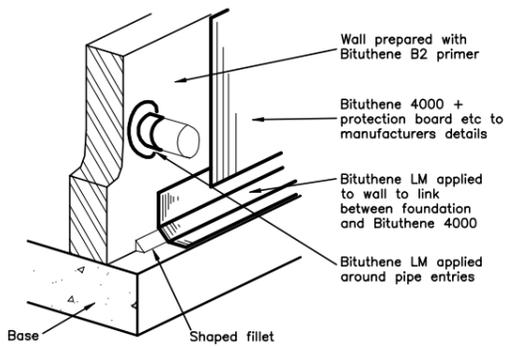
Bar Dia	Lap Lengths
H8	325 mm
H10	400 mm
H12	475 mm
H16	625 mm
H20	1050 mm
H25	1300 mm
H32	1675 mm

All minimum laps to reinforcement are to comply with the requirements of BS 8110.



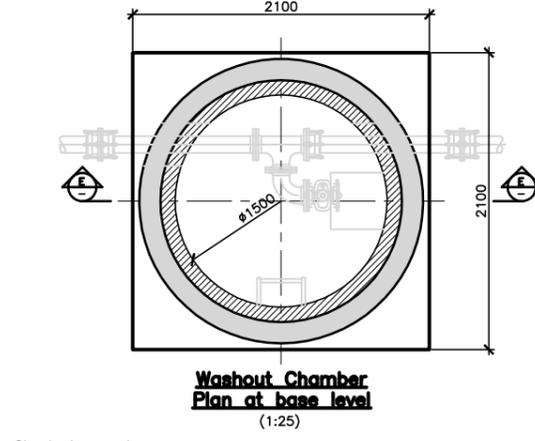
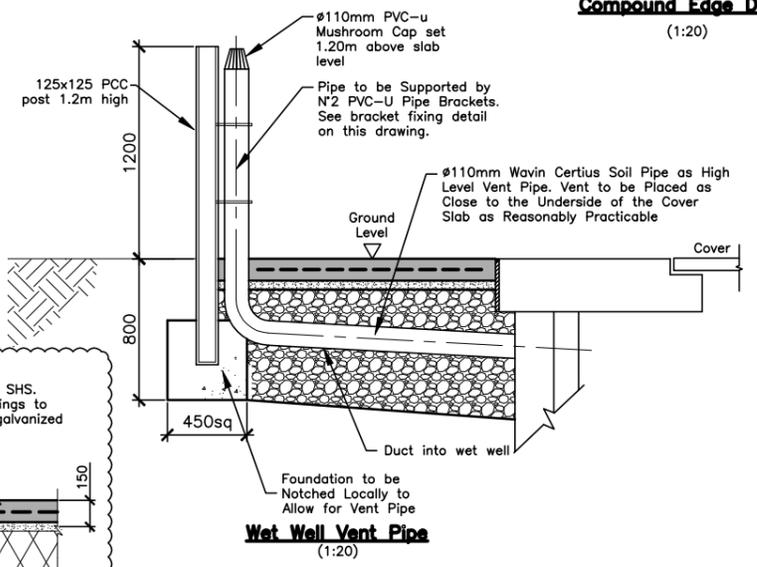
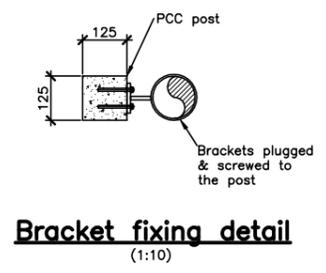
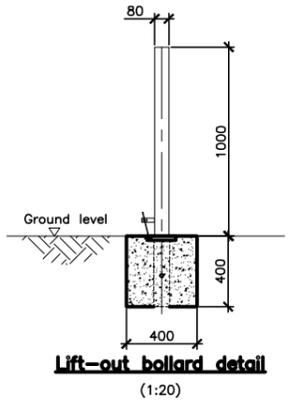
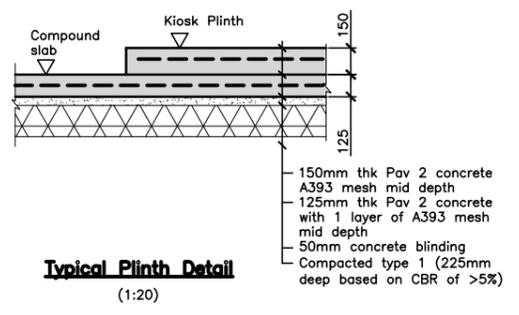
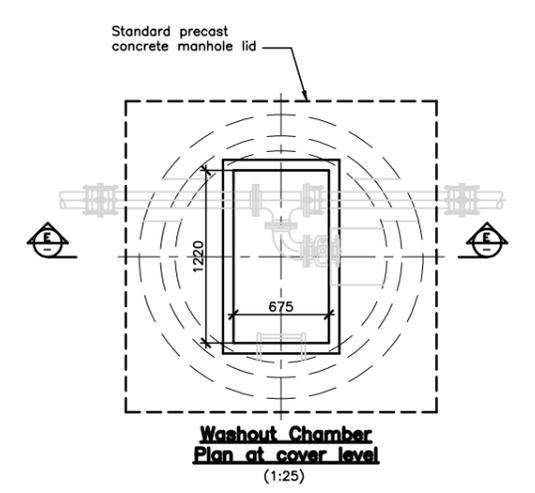
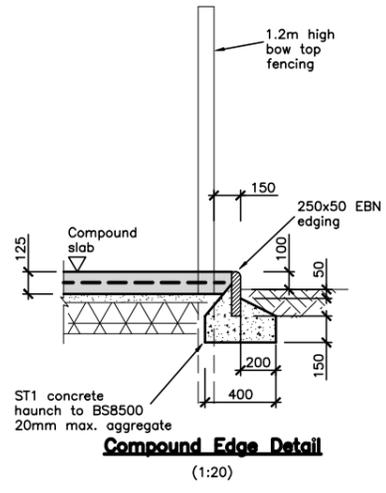
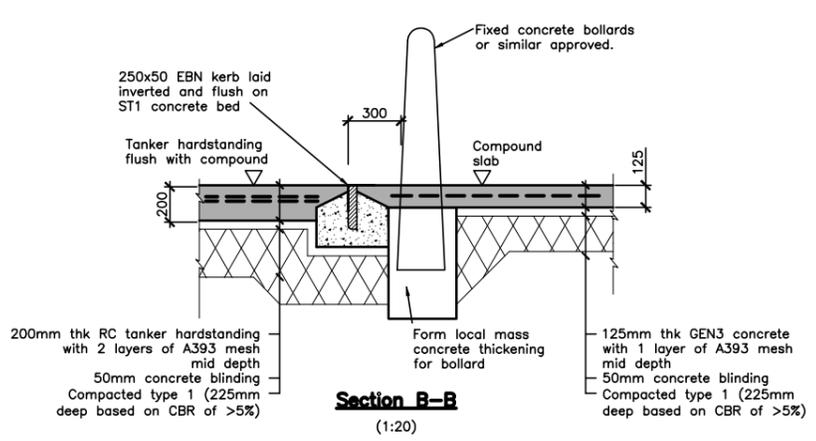
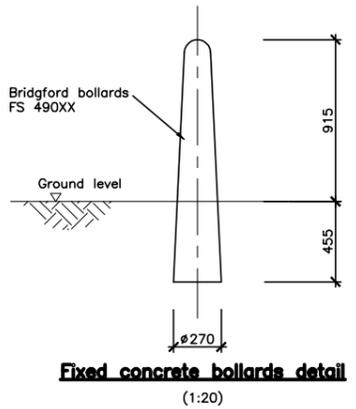
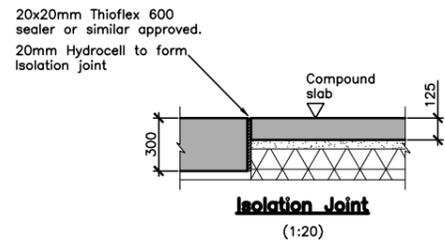
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Details in accordance with PDAS Ltd drg PR14633-001 Check against latest drawings before construction



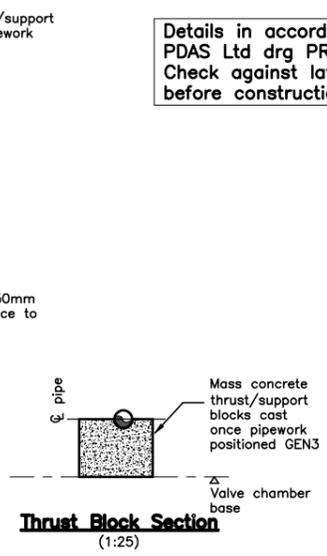
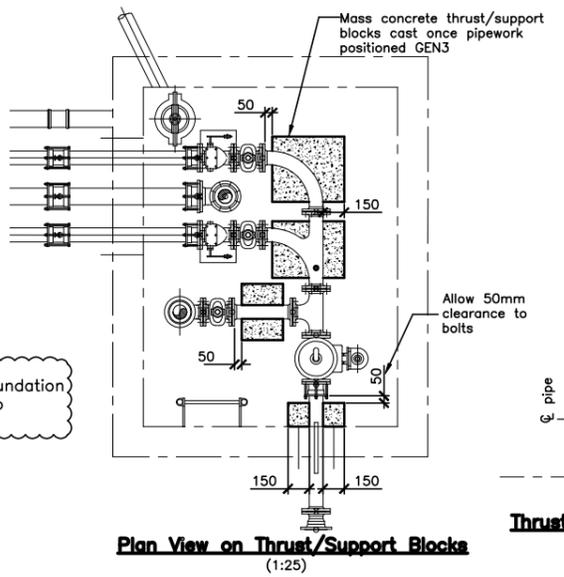
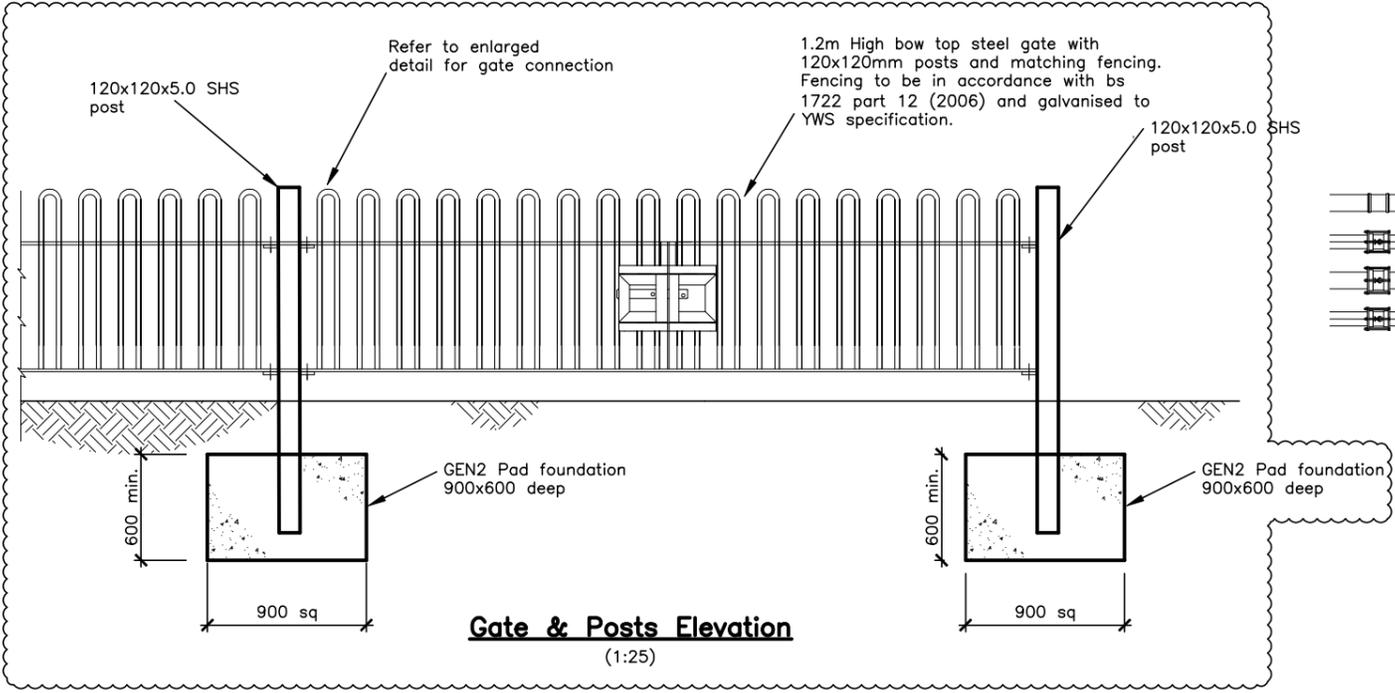
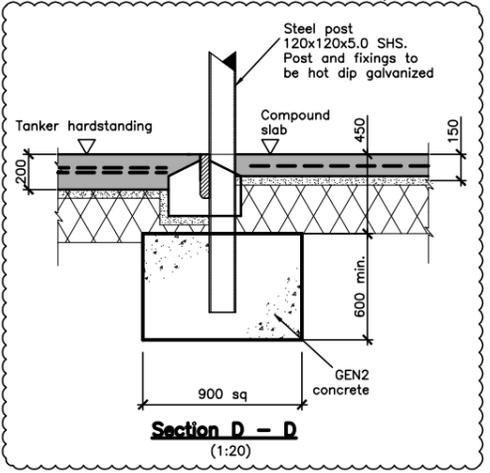
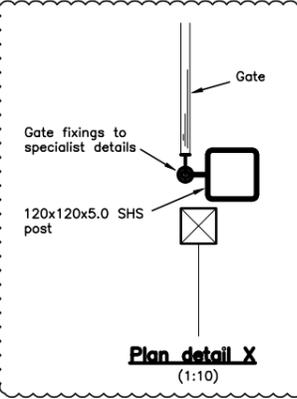
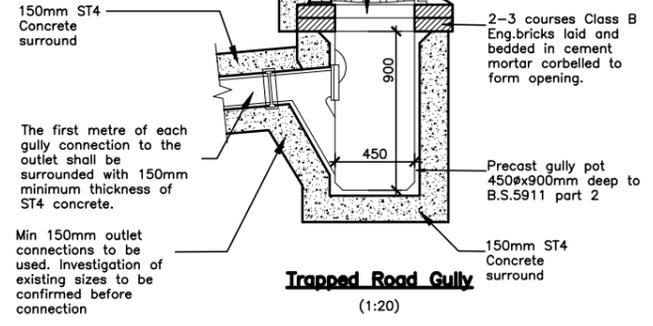
Isometric view on valve chamber wall

P1	05/05/22	Preliminary Issue.	AK	JAK
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Client		<p>PDAS Ltd Ipsum Court, 24 The Quadrant, Abingdon Science Park, Abingdon Oxon, OX14 3YS Tel: 01235 555173 Email: mail@mjaconsulting.co.uk</p>	<p>MJA CONSULTING CIVIL & STRUCTURAL ENGINEERS</p>	
Project				
Title		Pump Station GA & RC Details Sheet 2	Scale: As shown@A1	Status: PRELIMINARY
Drawn: AK	Project Engineer: JAK	MJA Project No: 6711	Date: 04/05/2022	Rev: P1
Drawing Number: 6711-MJA-SW-XX-DR-S-1001				

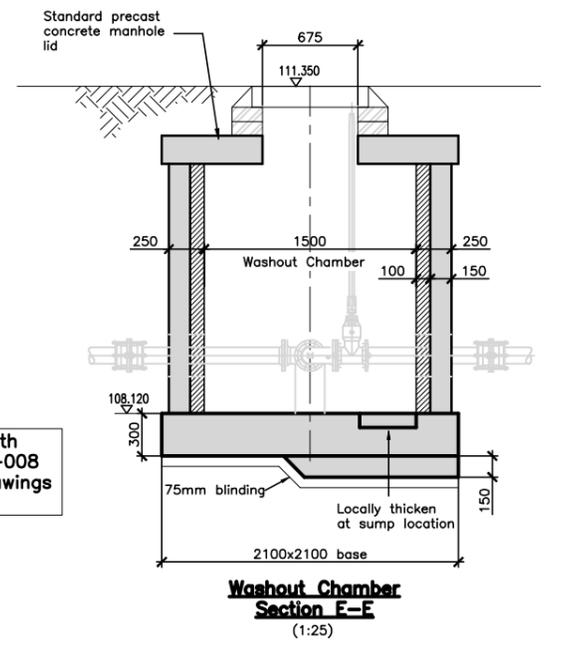


Class D400 end hinged captive Gully grating and frame to B.S.EN 124 Ref.GA2-450 bedded 10-12 Designation (i) cement mortar series 2400.

Any gullies in shared surfaces to have pedestrian grating. Gully Gully grating to be set 15mm below road at kerb face and 5mm at front of grating.



Details in accordance with PDAS Ltd drg PR14633-008 Check against latest drawings before construction



P2	11/02/22	Gate and fence details updated.	AK	JAK
P1	05/05/22	Preliminary Issue.	AK	JAK
REV. No.	DATE	DESCRIPTION	DRAWN	CHECKED
			AK	JAK
Client				
Project		Whitechapel Road, Cleckheaton		
Title		Pump Station GA & RC Details Sheet 3		
Scale:	As shown	Status:	PRELIMINARY	
Drawn:	AK	Project Engineer:	JAK	MJA Project No:
Drawing Number:	6711-MJA-SW-XX-DR-S-1002	Date:	04/05/2022	Rev:
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