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Woodhead Road, Honley

BMS Group

STAGE 1 - Flood Risk Assessment

December 2013



P1244 Rev 02



Revision Histor	У		
Initial Issue Prepared By:	20 December 2013	Checked:	ar.
	Timothy Davis	_	Graham Helme
	Director		Director

Rev No	Date	Description	Ву	Checked
0	19.12.13	Initial Issue	TD	GH
01	15.07.14	Report update to match planning layout	TD	GH
02	19.07.17	Report update to match planning layout	TD	GH



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1 INTRODUCTION

Avie Consulting Ltd has been commissioned by the BMS Group to carry out a STAGE 1 Flood Risk Assessment for the development of a Greenfield area off Woodhead Road Honley in order to support an Outline Planning Application.

The aim of this report is to allow Kirklees Council to assess the site in accordance with the National Planning Policy Framework published by the Department of Communities and Local Government.

The site lies in **Flood Zone 1**, the proposed site area is in excess of 1Ha therefore a Flood Risk Assessment is required as part of the site evaluation.

The following published reports have been utilised while undertaking the FRA:

Calder Valley SFRA undertaken by JBA Ltd November 2008

2 PROPOSED DEVELOPMENT

The site is located 1.2km South East of Honley along the Woodhead Road A6024 South East of Melton at Ordnance Survey grid reference SE146 111

The site is bounded to the West by Woodhead Road A6024

The site is bounded to the North by a wooded area.

The site is bounded to the East Tree belt and an open field beyond

The site is bounded to the south by Robinson Lane an unmade access track / footpath

The site falls East to West, the topography of the site varies between 134.01 and 113.09 AOD

The site is shown on the location plan in Appendix A, the site is approximately 2.6 Hectares in size, the topographical survey of the site is presented in Appendix H.

3 FLOOD RISK ASSESSMENT CRITERIA

The site under consideration is within Flood Zone 1 according to the latest version of the Indicative Floodplain Map (IFM) produced by the Environment Agency. As the site area exceeds 1Ha there is a need to carry out a flood risk assessment of the site.

The EA Indicative Floodplain Map is enclosed in Appendix B, also enclosed in Appendix B is the Flood Map Risk from the Calder Valley SFRA report undertaken in November 2008 by JBA which also indicates the site is not at risk of flooding and is in Flood Zone 1.

Zone 1 is defined as land assessed as having less than a 1 in 1000 annual probability of river or sea flooding in any year (0.1%).



As the site lies within Flood Zone 1 the flood risk assessment needs to consider the following:

- Flooding from other sources such as rivers ,tidal, sewers and overland flooding
- The potential for the development to increase flooding elsewhere through the addition of hard surfaces
- The effect of the new development on surface water run-off

4 HISTORICAL FLOODING

The SFRA undertaken by JBA did not highlight any historical flooding in the vicinity of the site and this was also confirmed by the email from the Kirkless Land Drainage department presented in Appendix C.

The risk of flooding from historical flood event affecting the site in future is **LOW**.

5 SOURCES OF FLOODING

As part of the flood risk assessment consideration should be given to the following sources of flooding and what effect these could have on the development.

5.1 Flooding from Rivers / Watercourses

The River Holme (EA Main River) exists to the east approx. 1.2km from the nearest site boundary site.

The River Home is approximately 8m below the eastern boundary of the site and therefore the risk of flooding from this source is considered to be **LOW**.

An existing watercourse potentially exists on the site and may be the cause due to blockage of some standing water on and near to the site.

Further investigation is required to fully understand the existing land drainage features on the site and appropriate mitigation to be proposed.

5.2 Flooding from the Sea

The site is approximately 85Km form the sea, as such the risk if flooding from this source is considered to be **LOW**.

5.3 Flooding from Land

The effect of intense rainfall needs to be considered and the local Topography of the land assessed.

The development area falls East to West by 21metres with the adjoining land falling towards the River Holme. Overland water from a westerly direction is intercepted by Woodhead Road with other adjoining areas either falling away from the site, therefore the risk of flooding from adjoining land is considered to be **LOW**.

5.4 Flooding from Groundwater

Groundwater flooding occurs when water levels in the ground rise above surface elevations, particularly in low lying areas.

From our site inspection we did observed a wet area to the centre of the site and this could be a spring which will require incorporating onto the drainage scheme

The risk of flooding from this source is considered to be **MEDIUM**.



5.5 Flooding From Sewers

The site is a greenfield development and has NO existing sewers serving the site, the nearest Public Sewer is a combined 225 dia sewer is Banks Road, the risk of flooding from this source is considered to be **LOW**.

YW records are presented in Appendix D.

6 FLOOD RISK SUMMARY

	Risk				
Sources of Flooding	High	Medium	Low	Control Measures	
Rivers:			Х	None	
Watercourses			Х	None	
Sea			Х	None	
Land			Х	None	
Groundwater		Х		Ensure flood routes are maintained and houses are min 150mm above existing ground levels	
Existing sewers			Х		

7 INCREASE TO OFFSITE FLOODING

New development should be designed to limit the surface water run-off to existing surface water discharge flows rates or better.

Current industry practice is to reduce off site flows from brownfield developments by 30% so as to reduce the impact of the development and new drainage systems.

Therefore by reducing off site flows the risk of increasing flooding off site is mitigated.

8 FLOOD RISK VULNERABILITY

The vulnerability of the proposed development is assessed in accordance with the Technical Guidance to the National Planning Policy Framework published by the Department for Communities and Local Government in March 2012.

The report should consider if the development is acceptable for the Flood Zone Classification in accordance with Table 3 within the NPPF.



The proposed development is residential and is therefore classified as "More vulnerable"

Table 3: Flood Risk Vulnerability and Flood Zone 'Compatibility'

	/ulnerability on (from Table 2)	Essential Infrastructure	Water compatible	Highly Vulnerable	More Vulnerable	Less Vulnerable
Flood Zone	Zone 1	✓ ✓ 		✓	✓	✓
	Zone 2	✓	✓	Exception Test required	✓	✓
	Zone 3a	Exception Test required	√	×	Exception Test required	✓
	Zone 3b	Exception Test required	✓	×	×	*

[✓] Development is appropriate

<u>Utilising the Flood Zone Compatibility Table above, the development is deemed appropriate for the site and flood risk classification</u>

As part of the assessment the following development constraints require consideration and recommendation made as to how to mitigate any flood risk appropriately.

8.1 Finished Floor Levels

We recommend to mitigate against localised flooding caused by heavy / intense rainfall events, that the internal ground floor level of the residential units is set a minimum of 150mm above existing ground levels and a minimum of 300mm above road levels.

8.2 Existing Flood Volumes

No loss of existing flood volume will be experienced due to the redevelopment of the site.

8.3 Flood Routing

The site is bounded to the south west by Woodhead Road, this road is bounded on the southern kerb with a boundary wall and beyond this woodland and residential properties as such overland flows from above the site will be limited.

The site falls initially to the east towards Smithy Place then changes direction to a north westerly direction please refer to Plan 1 Appendix I. The proposed site levels will generally follow the existing gradients however properties will be 300mm above proposed road levels.

The site attenuation system will be designed to accommodate a 1 in 100 yr storm plus climate change however during exceedance events the highways and drainage easements will be used as overland flood routes thereby maintaining existing flow routes and protecting properties, please refer to Plan 2 Appendix I

[×] Development should not be permitted



Should any overland flows enter the site from Smith Place a land drainage system is proposed on the boundary should it be deemed necessary however with the site levels being maintained we do not feel this is a major concern.

8.4 Emergency Access

The site is in flood zone 1 and as such emergency access is not an issue.

9 EXISTING SITE DRAINAGE

The site does not have a formal drainage system, however Kirklees Council have commented that a possible well and watercourse adjacent to Woodhead Road possibly heads in the direction of the site. This will require further investigation and diversion if the route affects the development.

Yorkshire Water (YW) have been consulted with respect to existing drainage system in the area and their full response is presented in Appendix D.

YW have confirmed that the only available pubic sewer is a 225 dia public combined sewer recorded in Banks Road some 55 metres way from the site.

10 PROPOSED DRAINAGE

10.1 Surface Water

The proposed re development of the site will be residential, it is recommended and in accordance with good practice that the offsite surface water flows are reduced by the introduction of an attenuation system following the hierarchy as laid out in the approved document H of Building Regulations with respect to Sustainable Urban Drainage Systems (SUDS).

The use of soakaways will require investigating however from our onsite inspection standing water was evident which would suggest that the ground is not free draining however this will require verifying via an intrusive site investigation.

Should infiltration rates prove to be adequate then infiltration drainage will require incorporating into the drainage scheme and the FRA updating at the detailed design stage.

YW have commented that the site should be developed using on site separate foul and surface water systems up to the public sewer. The public sewerage network does not have capacity to accept surface discharge. Therefore with the River Holme being in closed proximity connection to this will be pursued either by a requisition agreement, private easement agreement or connection to as yet unidentified existing land drainage systems, the discharge to the River Holme will be limited to 1 in 2yr greenfield discharge.

During detailed design further consultation with respect to the connection point will be undertaken and the FRA updated appropriately.

The site total area is 2.60 Ha, with a proposed impermeable area of 0.891Ha making an impermeable area for greenfield calculations of 0.891Ha, the proposed site layout is presented is Appendix E.



Utilising the Micodrainage Windes suite of programs to calculate the "Greenfield " runoff rate produces a discharge rate of 6.1 litres per second I in 2 yr return period.

However Kirklees Council have commented that due to more efficient land drainage system the discharges should be restricted to 5 l/s/Ha meaning that a discharge rate of 4.455 l/s would be applicable.

It is intended to offer the onsite drainage to Yorkshire Water for Adoption and as such YW will require the outlet to be 100mm in diameter therefore the Attenuation System for the site should be designed so as to ensure no surcharging for a 1 in 2 yr storm, no flooding on site for a 1 in 30 yr plus 30% climate change utilising a restricted discharge of 5 litres per second and any flooding for a 1 in 100 yr storm plus climate change to remain on site but not to affect plots.

Please refer to Appendix F for runoff calculation's, methods used IH124, ICPSUDS and ADAS 345.

10.2 Outline of Attenuation Requirements

Assuming that Infiltration techniques are not appropriate then the following can be used as a guideline for the for the attenuation requirements .The Attenuation could be undertaken via a combination of different structures from swales, porous paving, soakaways, ponds and underground attenuation tanks.

Due to the excessive gradient swales would not be practicable as means of attenuation therefore an underground storage tank seems the most obvious deliverable proposal. The attenuation system will be designed to accommodate a 1 in 30 yr storm plus climate change with flood water above 1 in 30 and upto 1 in 100 yr plus climate change being contained on site.

The worst case scenario attenuation is presented in Appendix G along with the supporting calculations.

The drainage proposals will include for providing a land drain to prevent overland flows affecting Smithy Place connecting to the offsite easement pipework which discharges to the River Holme.

10.3 Foul Water

YW have indicated that the foul flows should be discharged to the 225 mm diameter combined sewer recorded in Banks Road,

Due to the site levels a foul pumping station will be required with a limited discharge of 5 litres per second. The compound for the pumping station will be 8m x 10m and at least 15m from the nearest habitable dwelling.



11 DRAINAGE IMPACT

Utilising the surface water discharge rate of 5 litres per second per hectare discharging to the River Holme will not increase flood risk significantly within the watercourse system as the flows match the pre development run off situation.

12 GENERAL REMARKS

This report is for the sole use of BMS Group and their immediate advisors in connection with the development of the subject site for residential use. It shall not be reproduced in whole or in part or relied upon by third parties for any use whatsoever without the express permission of Avie Consulting Ltd. Avie Consulting Ltd shall have no liability for any use of this report other than for the purposes for which it was originally prepared.

We recognise that FSR data has been utilised in the Stage 1 FRA and not FEH data, however the design package used is industry standard and accepted by Sewerage Regulators to model site flows and adoptable storage requirements and therefore we consider the calculations are robust and appropriate for the purposes intended to support a STAGE 1 FRA.

13 RECOMMENDATIONS

- The site under consideration is located in Zone 1 latest version of the Indicative Floodplain Map (IFM)
 produced by the Environment Agency and the flood Zone map produced by JBA as presented in the
 SFRA dated November 2008.
- There are no recorded historical flooding directly on or adjacent to the site. The risk of flooding to the site / residential units is considered to be **LOW**.
- Residential Development is classified as "More Vulnerable" and is appropriate under the National Planning Policy Framework on this redevelopment site in terms of Flood Risk in flood zone 1 areas.
- It is recommended that finished floor levels to the new residential dwelling are set at a minimum of 150mm above existing ground levels in order to mitigate against localised flooding caused by heavy / intense rainfall and 300mm above road levels.
- Surface water flows from the development are to be connected to the River Holme at 5 litres per second for storm profiles up to a 1 in 30 yr plus climate change event, with any flooding above this event remaining on site up to a 1 in 100 yr storm plus climate change.
- The proposed development will not affect flood routing, and as such flows/ flood routing will be maintained as per the pre-development layout.

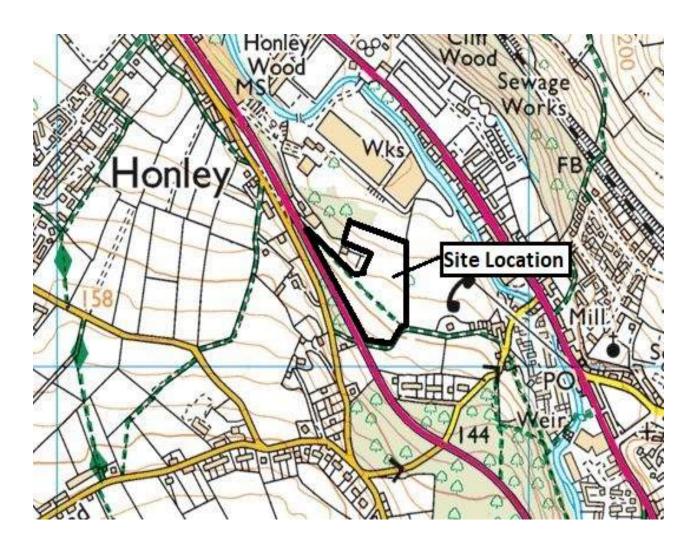


- Should infiltration rates prove to be adequate then infiltration drainage will require incorporating into the drainage scheme and the FRA updating at the detailed design stage.
- The River Holme is not directly situated next to the proposed site boundary and as such a connection to the watercourse will be provided by either a private easement agreement or a requisitioned sewer.
- Foul water discharge will require further consideration to incorporate one of the following solutions.
 - 1. Connection to the Yorkshire Water Sewer in Banks Road via a onsite pumping station with appropriate compound area and stand off from residential dwellings.
- Consideration needs to be given to overland flood routing and proof to be provided at detailed design via cross sections and levels directing water away from residential properties.
- Utilising the surface water discharge rate of 5 litres per Second discharging to the River Holme will not increase flood risk significantly within the watercourse system as the flows match the pre development run off situation.
- The Attenuation System for the site should be designed so as to ensure no surcharging for a 1 in 2 yr storm, no flooding for a 1 in 30 yr plus 30% climate change and any flooding for a 1 in 100 yr storm plus climate change to remain on site but not to affect plots.
- The drainage proposals will include for providing a land drain to prevent overland flows affecting Robinson Lane connecting to the offsite easement pipework which discharges to the River Holme.



APPENDIX A

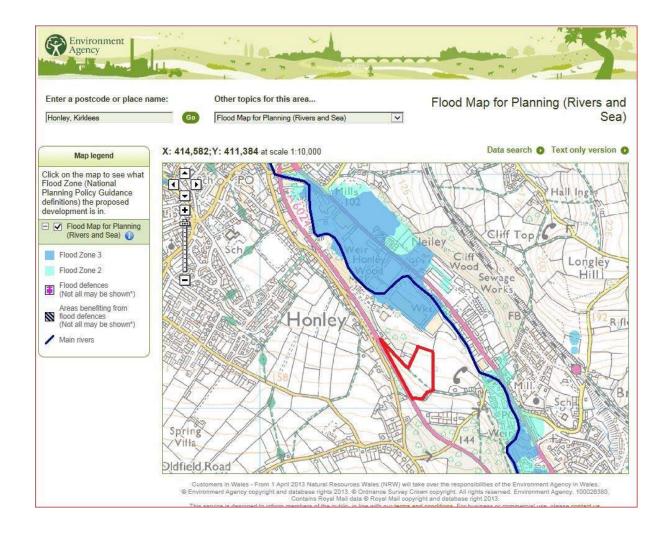
Location Plan



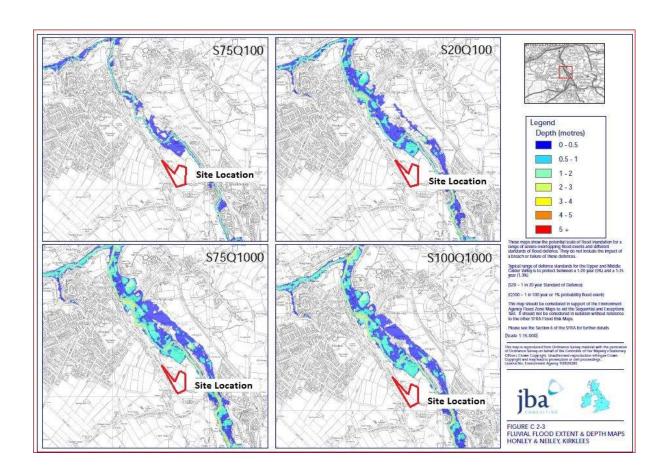


APPENDIX B

EA Flood Maps/ SFRA Flood Zones









APPENDIX C

Historical Flooding / Kirklees Council Response

Hello Tim,

The site is in Flood Zone 1. Everything falls to the river. It will be ok in principle to discharge to the river at 5l/s per hectare, i.e. the parts you are making impermeable in hectares x 5. If any perimeter drainage is required, this will have to be off-set within the road/house drainage restriction (3.5l/s/ha is suggested)

Just a note that whoever owns the land at the bank has a say in the right to discharge. Never been a problem until last week but I've found that crossing 3rd party land via sewer requisition doesn't cover the outfall within YW's powers, if you need to go down this route (had the landowner object).

No known flood incidents on site but don't take this as a comprehensive report as the Council is unlikely to be contacted for flooding in fields.

We have some records of minor flooding incidents to driveways and gardens from the public highway on Smithy Place Lane and Banks Road in extreme rainfall conditions. We have concluded that these incidents have not directly affected the site in question.

1st and second generation surface water flood maps do not indicate any potential issues on site. Historical plans do show a mill race running through land to the north. A mill pond was located to the north-west of the red line boundary 1893 and latterly 1907 what appears to be a boating like for a tourist destination. A mill race/watercourse from the outfall from these features crossed land to the north in an open section. Part of this section is still visible on the 1955 plans with the outfall section still showing on modern day plans.

There are some wells shown on historical plans in the vicinity of the site. The 1893 plan shows a well and possible watercourse adjacent to Woodhead Road heading in the direction of the site (and possibly beyond to features described above). Further investigation is advised. The 1854 plan shows an uneven field boundary in this area which can be associated with a natural feature, i.e. minor watercourse. This could of course now be culverted. Suitable routing any ordinary watercourse will have to be agreed with the Council.

The site layout will have to accommodate a flood routing plan for blockage scenarios for any minor watercourse and the on site designed drainage. 2D modelling will not be required but the I would expect the FRA to clearly evidence that this has been considered in the layout so the flood route avoids property for certain and gardens if practicable. Detailed sections involving kerbs etc can of course come later. We basically need to know the principle is workable. Future development to the north will have to be taken into account for flood routing.

An assessment of the drainage on the unadopted road, Smithy Place, which is a public right of way will have to form part of the report incorporating how this may affect or be affected by the development.

Please note this is a desktop study and additional comments may arise from any site visit when an application has been submitted.

Regards,

Paul Farndale Principal Engineer Flood Management & Drainage Investment & Regeneration Service Kirklees Council 01484 225377

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APPENDIX D

Yorkshire Water consultation



1 B DEC 2013

Yorkshire Water Services **Developer Services** Sewerage Technical Team **PO BOX 52** Bradford BD3 7AY

> Tel: 0845 120 8482 Fax: (01274) 372 834

> > Email:

Technical.Sewerage@yorkshirewater.co.uk

For telephone enquiries ring:

Kashif Khan on (0845)120 8482

17th December 2013

Avie Consulting Ltd The Sugar Refinery; Suite 55 Oakhurst Avenue **Dewsbury Road** Leeds **LS117HL**

FAO Tim Davis

Your Ref:

Our Ref: P017806

Dear Sir,

Woodhead Road, Honley - Pre-Planning Sewerage Enquiry on P282595

Thank you for your enquiry received 3rd December 2013. Our charge of £67.00 (plus VAT) will be added to your account with us, reference ACE105. You will receive an invoice for your account in due course. Please find enclosed a complimentary extract from the Statutory Sewer Map which indicates the recorded position of the public sewers. The following comments reflect our view, with regard to the public sewer network only, based on a 'desk top' study of the site:

Development of the site should take place with separate systems for foul and surface water drainage. The separate system should extend to the public sewer.

Foul water domestic waste should discharge to the 225 mm diameter public combined sewer recorded in Banks Road, at a point approximately 55 metres from the site.

From the information supplied, it is not possible to determine if the whole site will drain by gravity to the public sewer network. If the site, or part of it, will not drain by gravity, then it is likely that a sewage pumping station will be required to facilitate connection to the public sewer network. If sewage pumping is required foul water discharge must not exceed 5 (five) litres per second.

The developer's attention is drawn to Requirement H3 of the Building Regulations 2000. This establishes a preferred hierarchy for surface water disposal. Consideration should firstly be given to discharge to soakaway, infiltration system and watercourse in that priority order.

Sustainable Drainage Systems (SUDS), for example the use of soakaways and/or permeable hardstanding etc, may be a suitable solution for surface water disposal appropriate in this situation. You are advised to seek comments on the suitability of SUDS in this instance from the appropriate authorities.

Where appropriate, soakaways, swales and infiltration trenches (SUDS) may be adopted as part of the public sewer network. Further information may be seen in the DEFRA publication 'Interim Code of Practice for Sustainable Drainage Systems' (ISBN 0-86017-904-4). If the developer is considering adoption of SUDS they should contact our Developer Services Team on 0845 120 84 82.

The local public sewer network does not have capacity to accept any discharge of surface water from the proposal site. The developer is advised to contact the Environment Agency/local Land Drainage Authority with a view to establishing a suitable watercourse for discharge.





It is understood that a watercourse is located to the east of the site. This appears to be the obvious place for surface water disposal.

Please note further restrictions on surface water disposal from the site may be imposed by other parties. You are strongly advised to seek advice/comments from the Environment Agency/Land Drainage Authority, with regard to surface water disposal from the site.

Prospectively adoptable sewers and pumping stations must be designed and constructed in accordance with the WRc publication "Sewers for Adoption - a design and construction guide for developers" 6th Edition as supplemented by Yorkshire Water's requirements, pursuant to an agreement under Section 104 of the Water Industry Act 1991. An application to enter into a Section 104 agreement must be made in writing prior to any works commencing on site. Please contact our Developer Services Team (telephone 0845 120 84 82) for further information.

The public sewer network is for domestic sewage purposes. This generally means foul water for domestic purposes and, where a suitable surface water or combined sewer is available, surface water from the roofs of buildings together with surface water from paved areas of land appurtenant to those buildings. Land and highway drainage have no right of connection to the public sewer network. No land drainage to be connected/discharged to public sewer.

As a last resort, highway drainage may be accepted under certain circumstances. If it can be demonstrated, through satisfactory evidence, that SUDS are not a viable option, there are no watercourses or highway drains available and if capacity is available within the public sewer network, highway drainage discharges to the public sewer network may be permitted. In this event, the developer may be required to enter into a formal agreement with Yorkshire Water Services under Section 115 Water Industry Act 1991 to discharge non-domestic flows into the public sewer network.

Any new connection to an existing public sewer will require the prior approval of Yorkshire Water. You may obtain an application form from our website (www.yorkshirewater.com) or by telephoning 0845 120 84 82.

All the above comments are based upon the information and records available at the present time. The information contained in this letter together with that shown on any extract from the Statutory Sewer Map that may be enclosed is believed to be correct and is supplied in good faith. Please note that capacity in the public sewer network is not reserved for specific future development. It is used up on a 'first come, first served' basis. You should visit the site and establish the line and level of any public sewers affecting your proposals before the commencement of any design work.

Yours faithfully

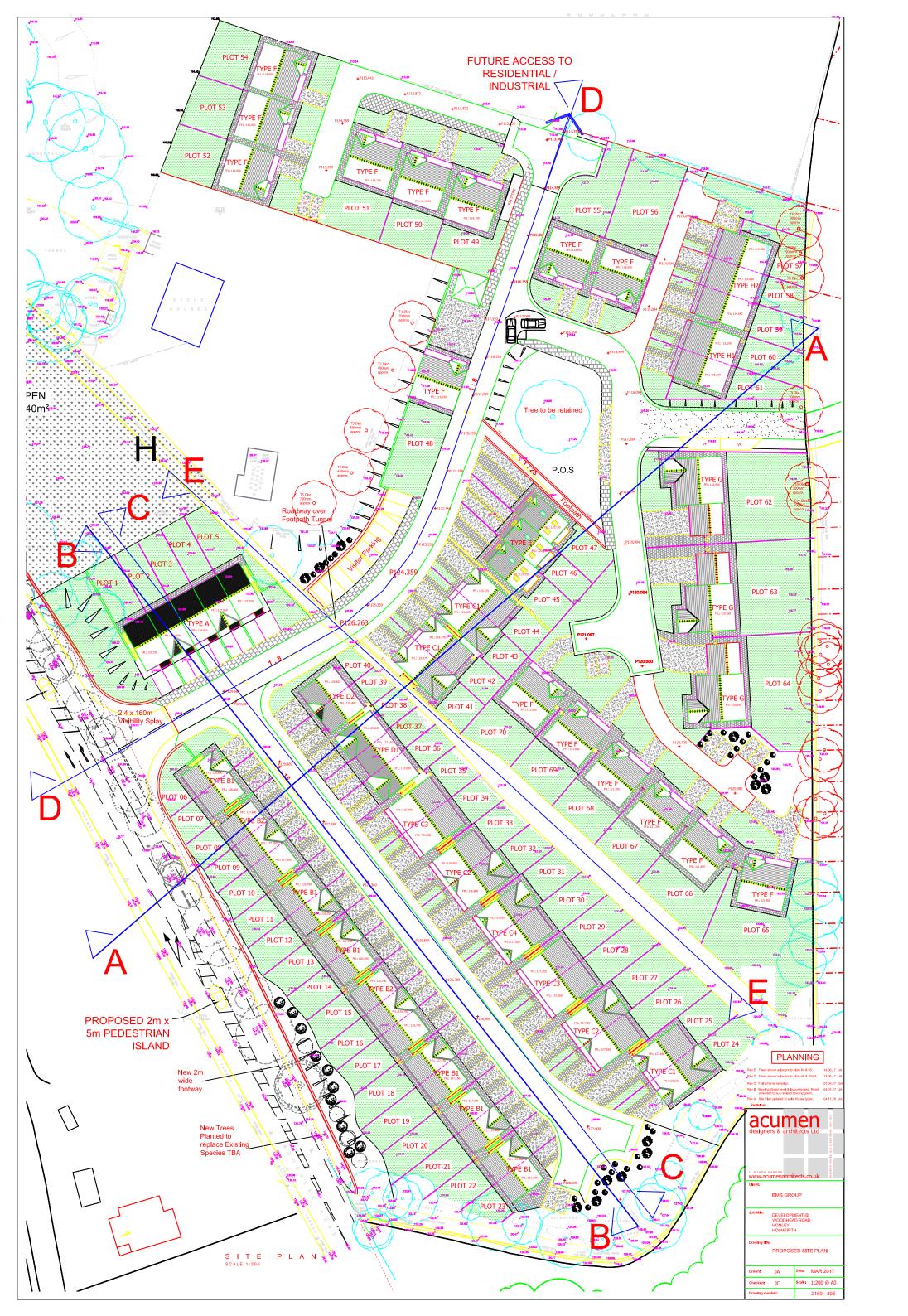
Developer Services Team





APPENDIX E

Proposed Site layout





APPENDIX F

Greenfield Run off rates

Avie Consulting Ltd		Page 1
Suite 55 The Sugar Refinery Leeds LS11 7HL	WOODHLAD ROAD	Micro
Date 19/12/2013 15:45	Designed by User	D) Ratinace
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Micro Drainage	Source Control 2013.1.1	

IH 124 Mean Annual Flood

Input

Return Period (years) 2 Soil 0.500 Area (ha) 50.000 Urban 0.000 SAAR (mm) 882 Region Number Region 3

Results

1/s QBAR Rural 361.8 QBAR Urban 361.8 Q2 years 341.4 Q1 year 311.1 Q2 years 341.4 Q5 years 452.3 Q10 years 524.6 Q20 years 594.2 Q25 years 617.2 Q30 years 636.0 Q50 years 685.3 Q100 years 752.5 Q200 years 853.9 Q250 years 886.4 Q1000 years 1099.9

PEO RATA TO 0-891 HA flow 16 G.1 els

Avie Consulting Ltd		Page 1
Suite 55 The Sugar Refinery Leeds LS11 7HL	WOSDYLLAS LO	Micro
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Micro Drainage	Source Control 2013.1.1	

ICP SUDS Mean Annual Flood

Input

 Return Period (years)
 2
 Soil
 0.500

 Area (ha)
 0.890
 Urban
 0.000

 SAAR (mm)
 882
 Region Number
 Region 3

Results 1/s

QBAR Rural 6.4 QBAR Urban 6.4

Q2 years 6.1

Q1 year 5.5 Q30 years 11.3 Q100 years 13.4

Avie Consulting Ltd		Page 1
Suite 55 The Sugar Refinery Leeds LS11 7HL	WOODKLAD RD	Micro
Date 19/12/2013 15:49	Designed by User	D) Parinace
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Micro Drainage	Source Control 2013.1.1	

ADAS 345 Mean Annual Flood

Input

Area (ha) 0.890 Soil Type Factor (St) 0.500
Length (m) 182.000 Paved Area (%) 0.000
Average Slope (1:X) 9.0 Region Number Region 3
AAR (mm) 882

1/s

Results

Q0 - Peak Flood Flow 6.5 Total Q0 6.5 QBAR 6.9 Q2 years 6.5 Q1 year 5.9 Q2 years 6.5 Q5 years 8.6 Q10 years 10.0 Q20 years 11.3 Q25 years 11.8 Q30 years 12.1 Q50 years 13.1 Q100 years 14.3 Q200 years 16.3

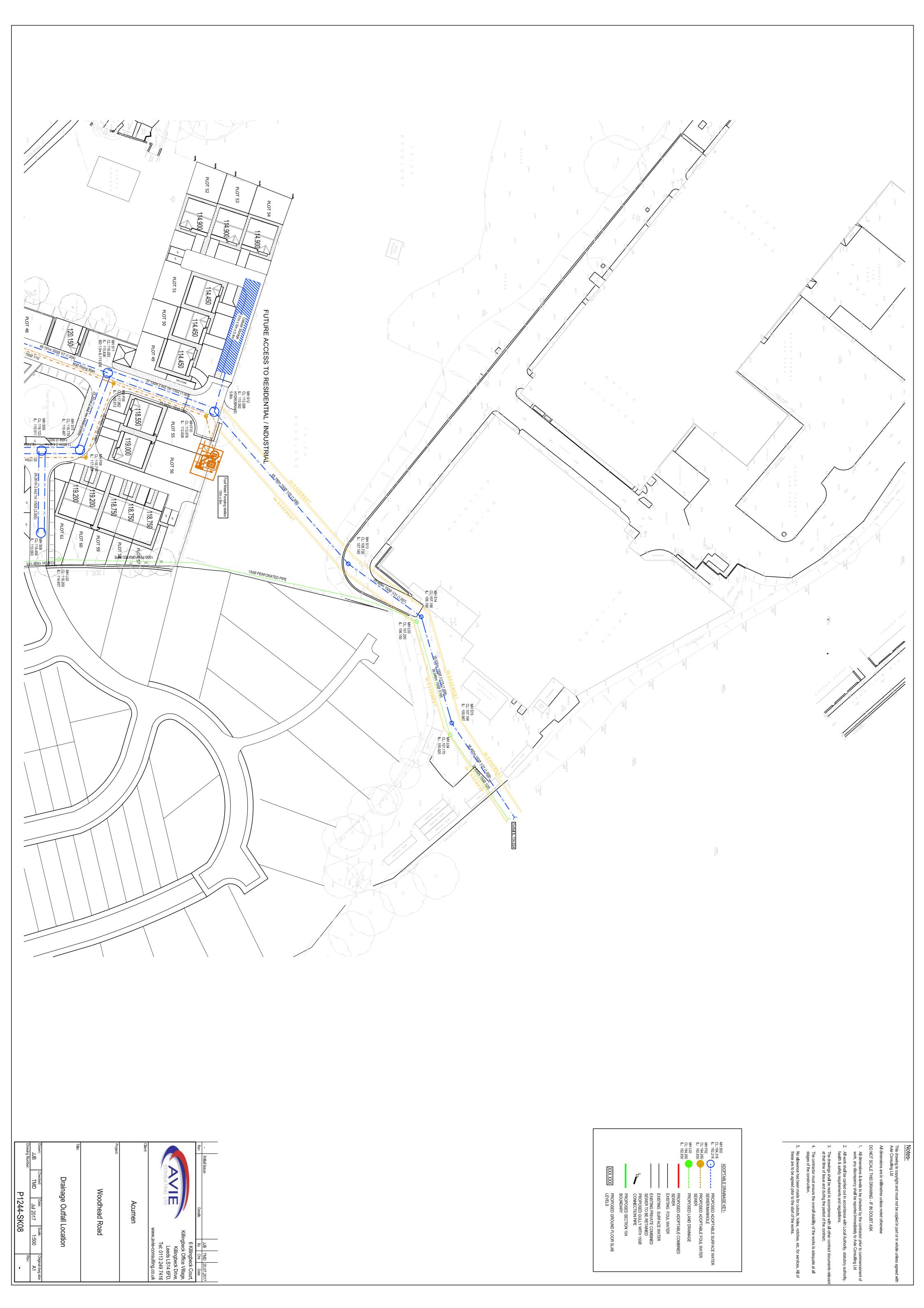
Q250 years 16.9 Q1000 years 21.0



APPENDIX G

Indicative Drainage Layout / Storage Calculations





Avie Consulting Ltd		Page 1
6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro
Date July 2017 File P1244 Woodhead Road 29	Designed by TMD Checked by	Drainage
Micro Drainage	Network 2016.1	

Existing Network Details for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	k (mm)	HYD SECT	DIA (mm)	Section Type	
1.000	56.214	0.112	501.9	0.228	3.00	0.600	0	1500	Pipe/Conduit	
1.001	46.825	0.094	498.1	0.155	0.00	0.600	0	1500	Pipe/Conduit	
1.002	32.882	1.086	30.3	0.111	0.00	0.600	0	300	Pipe/Conduit	
1.003	17.924	2.241	8.0	0.000	0.00	0.600	0	300	Pipe/Conduit	
1.004	48.191	6.583	7.3	0.108	0.00	0.600	0	300	Pipe/Conduit	
2.000	20.661	2.066	10.0	0.179	3.00	0.600	O	150	Pipe/Conduit	
2.001	18.743	0.037	506.6	0.000	0.00	0.600	[]	-8	Pipe/Conduit	2-4×2·1
3.000	26.261	0.052	505.0	0.020	3.00	0.600	[]	- 8	Pipe/Conduit	2.4×.21
2,002	11.853	0.024	493.9	0.027	0.00	0.600	[]	-8	Pipe/Conduit	2-4×2-1
2.003	25.291	0.051	495.9	0.018	0.00	0.600	[]		Pipe/Conduit	
1.005	37.130	0.074	501.8	0.080	0.00	0.600	[]	- 8	Pipe/Conduit	2.4×2.1
1.006	65.184	3,222	20.2	0.195	0.00	0.600	0	150	Pipe/Conduit	
1.007	28.989	0.950	30.5	0.000	0.00	0.600	0	150	Pipe/Conduit	
1.008	35.530	0.203	175.0	0.000	0.00	0.600	0	150	Pipe/Conduit	
1.009	36.497	1.363	26.8	0.000	0.00	0.600	0	150	Pipe/Conduit	

PN	US/MH Name	US/CL (m)	US/IL (m)	US C.Depth (m)	DS/CL (m)	DS/IL (m)	DS C.Depth (m)	Ctrl	US/MH (mm)
1.000	1	127.937	124.051	2.386	129.374	123.939	3.935		2400
1.001		129.374	123.939		130.507	123.845	5.162		2400
1.002			123.845		126.528	122.759		Hydro-Brake®	
1.003	4	126.528	122.759	3.469	124.359	120.518	3.541	-	1200
1.004	5	124.359	120.518	3,541	118.283	113.935	4.048		1200
2.000	6	120.094	116.114	3.830	119.581	114.048	5.383		1200
2.001	7	119.581	110.548	6.933	119.123	110.511	6.512		3000
3.000	8	118.456	110.563	5.793	119,123	110.511	6.512		3000
2.002	9	119.123	110.511	6.512	118.779	110.487	6.192		3000
2.003	10	118.779	110.487	6.192	118.283	110.436	5.747		3000
1.005	11	118.283	110.436	5.747	113.588	110.362	1.126		3000
1.006	12	113.588	110.362	3.076	108.730	107.140	1.440	Hydro-Brake®	3000
1.007	13	108.730	107.140	1.440	107.198	106.190	0.858	•	1200
1,008	14	107.198	106.190	0.858	107.166	105.987	1.029		1200
1.009	1.5	107.166	105.987	1.029	105.000	104.624	0.226		1200

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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro
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Micro Drainage	Checked by Network 2016.1	

Simulation Criteria for Storm

Volumetric Runoff Coeff	0.750	Additional Flow - % of Total Flow	0.000
Areal Reduction Factor	1.000	MADD Factor * 10m3/ha Storage :	2.000
Hot Start (mins)	0	Inlet Coefficient	0.800
Hot Start Level (mm)	0	Flow per Person per Day (1/per/day)	0.000
Manhole Headloss Coeff (Global)	0.500	Run Time (mins)	60
Foul Sewage per hectare (1/s)	0.000	Output Interval (mins)	1

Number of Input Hydrographs 0 Number of Storage Structures 0 Number of Online Controls 2 Number of Time/Area Diagrams 0 Number of Offline Controls 0 Number of Real Time Controls 0

Synthetic Rainfall Details

	Rainfal	ll Model			FSR		Prof:	ile Type	Summer
Return	Period	(years)			2		Cv	(Summer)	0.750
		Region	England	and	Wales		Cv	(Winter)	0.840
	M5-	-60 (mm)			19.700	Storm	Duration	n (mins)	30
		Ratio R			0.281				

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Online Controls for Storm

Hydro-Brake Optimum® Manhole: 3, DS/PN: 1.002, Volume (m3): 108.6

Unit Reference MD-SHE-0098-5000-1500-5000 Design Head (m) 1.500 Design Flow (1/s) 5.0 Flush-Flo** Calculated Objective Minimise upstream storage Application Surface Sump Available Yes Diameter (mm) Invert Level (m) 123.845 Minimum Outlet Pipe Diameter (mm) 150 Suggested Manhole Diameter (mm) 1200

 Control Points
 Head (m)
 Flow (1/s)

 Design Point (Calculated)
 1.500
 5.0

 Flush-Flo™
 0.431
 4.9

 Kick-Flo®
 0.878
 3.9

 Mean Flow over Head Range
 4.3

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (1/s)	Depth (m) F	rlow (1/s)	Depth (m)	Flow (1/s)	Depth (m)	Flow (1/s)
0.100	3.2	1.200	4.5	3.000	6.9	7.000	10.3
0.200	4.4	1.400	4.8	3.500	7.4	7.500	10.7
0.300	4.8	1.600	5.1	4.000	7.9	8.000	11.0
0.400	4.9	1.800	5.4	4.500	8.4	8.500	11.3
0.500	4.9	2.000	5.7	5.000	8.8	9.000	11.6
0.600	4.8	2.200	6.0	5.500	9.2	9.500	11.9
0.800	4.3	2.400	6.2	6.000	9.6		
1.000	4.1	2.600	6.5	6.500	10.0		

Hydro-Brake Optimum[®] Manhole: 12, DS/PN: 1.006, Volume (m³): 194.8

Unit Reference MD-SHE-0089-5000-2300-5000 Design Head (m) 2.300 Design Flow (1/s) Flush-Flo™ Calculated Objective Minimise upstream storage Application Surface Sump Available Yes Diameter (mm) 89 Invert Level (m) 110.362 Minimum Outlet Pipe Diameter (mm) 150 Suggested Manhole Diameter (mm) 1200

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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro
Date July 2017 File P1244 Woodhead Road 29	Designed by TMD Checked by	Drainage
Micro Drainage	Network 2016.1	

Hydro-Brake Optimum® Manhole: 12, DS/PN: 1.006, Volume (m3): 194.8

Control	Points	Head (m)	Flow (1/s)
Design Point	(Calculated)	2.300	5.0
	Flush-Flo™	0.384	3.8
	Kick-Flo®	0.790	3.1
Mean Flow ove	r Head Range	(5)	3.8

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum 0 as specified. Should another type of control device other than a Hydro-Brake Optimum 0 be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (1/s)	Depth (m) Fl	low (1/s)	Depth (m) Fl	low (1/s)	Depth (m)	Flow (1/s)
0.100	2.7	1.200	3.7	3.000	5.7	7.000	8.4
0.200	3.6	1.400	4.0	3.500	6.1	7.500	8.7
0.300	3.8	1.600	4.2	4.000	6.5	8.000	9.0
0.400	3.8	1.800	4.5	4.500	6.8	8.500	9.3
0.500	3.8	2.000	4.7	5.000	7.2	9.000	9.5
0.600	3.7	2.200	4.9	5.500	7.5	9.500	9.8
0.800	3.1	2.400	5.1	6.000	7.8		
1.000	3.4	2.600	5.3	6.500	8.1		

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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro
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Micro Drainage	Network 2016.1	

Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
Hot Start Level (mm) 0 Inlet Coefficient 0.800
Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (1/per/day) 0.000
Foul Sewage per hectare (1/s) 0.000

Number of Input Hydrographs 0 Number of Storage Structures 0 Number of Online Controls 2 Number of Time/Area Diagrams 0 Number of Offline Controls 0 Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FSR Ratio R 0.281
Region England and Wales Cv (Summer) 0.750
M5-60 (mm) 19.700 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0 DVD Status ON
Analysis Timestep Fine Inertia Status ON
DTS Status ON

Profile(s) Summer and Winter
Duration(s) (mins) 15, 30, 60, 120, 180, 240, 360, 480, 600,
720, 960, 1440, 2160, 2880, 4320, 5760,
7200, 8640, 10080
Return Period(s) (years) 30
Climate Change (%) 30

	US/MH			Return	Climate	First	(X)	First	(Y)	First	(Z)	Overflow
PN	Name	S	torm	Period	Change	Surch	arge	Floo	bd	Overf	low	Act.
1.000	1	360	Winter	30	+30%	30/240	Winter					
1.001	2	360	Winter	30	+30%	30/180	Winter					
1.002	3	360	Winter	30	+30%	30/15	Summer					
1.003	4	360	Winter	30	+30%							
1.004	5	15	Summer	30	+30%							
2.000	6	15	Summer	30	+30%	30/15	Summer					
2.001	7	2880	Winter	30	+30%	30/2880	Winter					
3.000	8	2880	Winter	30	+30%	30/2880	Winter					
2.002	9	2880	Winter	30	+30%	30/2160	Winter					
2.003	10	2880	Winter	30	+30%	30/2160	Winter					
1.005	11	2880	Winter	30	+30%	30/1440	Winter					
1.006	12	2880	Winter	30	+30%	30/15	Summer					
1.007	13	2880	Winter	30	+30%							
1.008	14	2880	Winter	30	+30%							
1.009	15	2880	Winter	30	+30%							

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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro
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Micro Drainage	Network 2016.1	

Summary of Critical Results by Maximum Level (Rank 1) for Storm

	US/MH	Water Level	Surcharged Depth	Flooded Volume	Flow /		Pipe Flow		Level
PN	Name	(m)	(m)	(m ³)	Cap.	(l/s)	(1/s)	Status	Exceeded
1.000	1	125.635	0.084	0.000	0.01		14.8	SURCHARGED	
1.001	2	125.635	0.196	0.000	0.00		9.6	SURCHARGED	
1.002	3	125.635	1.490	0.000	0.03		5.4	SURCHARGED	
1.003	4	122.782	-0.277	0.000	0.02		5.4	OK	
1.004	5	120.589	-0.229	0.000	0.13		49.7	OK	
2.000	6	117.605	1.341	0.000	1.25		66.7	SURCHARGED	
2.001	7	112.686	0.038	0.000	0.00		2.6	SURCHARGED	
3.000	8	112.686	0.023	0.000	0.00		0.2	SURCHARGED	
2.002	9	112.686	0.075	0.000	0.00		2.7	SURCHARGED	
2.003	10	112.686	0.099	0.000	0.00		2.4	SURCHARGED	
1.005	11	112.687	0.151	0.000	0.00		5.4	SURCHARGED	
1.006	12	112.687	2.175	0.000	0.13		5.0	SURCHARGED	
1.007	13	107.180	-0.110	0.000	0.16		5.0	OK	
1.008	14	106.255	-0.085	0.000	0.39		5.0	OK	
1.009	15	106.026	-0.111	0.000	0.15		5.0	OK	



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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro
Date July 2017 File P1244 Woodhead Road 29	Designed by TMD Checked by	Drainage
Micro Drainage	Network 2016.1	

Simulation Criteria for Storm

Volumetric Runoff Coeff	0.750	Additional Flow - % of Total Flow	0.000
Areal Reduction Factor	1.000	MADD Factor * 10m3/ha Storage	2.000
Hot Start (mins)	0	Inlet Coefficient	0.800
Hot Start Level (mm)	0	Flow per Person per Day (1/per/day)	0.000
Manhole Headloss Coeff (Global)	0.500	Run Time (mins)	60
Foul Sewage per hectare (1/s)	0.000	Output Interval (mins)	1

Number of Input Hydrographs 0 Number of Storage Structures 0 Number of Online Controls 2 Number of Time/Area Diagrams 0 Number of Offline Controls 0 Number of Real Time Controls 0

Synthetic Rainfall Details

	Rainfal	1 Model		FS	2	Profi	le Type	Summer
Return	Period	(years)			2	Cv (Summer)	0.750
		Region	England	and Wales	3	Cv (Winter)	0.840
	M5 -	60 (mm)		19.70	Storm	Duration	(mins)	30
		Ratio R		0.28	L			

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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro		
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Micro Drainage	Network 2016.1			

Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000

Hot Start (mins) 0 MADD Factor * 10m3/ha Storage 2.000

Hot Start Level (mm) 0 Inlet Coefficient 0.800

Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (1/per/day) 0.000

Foul Sewage per hectare (1/s) 0.000

Number of Input Hydrographs 0 Number of Storage Structures 0 Number of Online Controls 2 Number of Time/Area Diagrams 0 Number of Offline Controls 0 Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FSR Ratio R 0.281
Region England and Wales Cv (Summer) 0.750
M5-60 (mm) 19.700 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0 DVD Status ON
Analysis Timestep Fine Inertia Status ON
DTS Status ON

Profile(s) Summer and Winter

Duration(s) (mins) 15, 30, 60, 120, 180, 240, 360, 480, 600,
720, 960, 1440, 2160, 2880, 4320, 5760,
7200, 8640, 10080

1 Period(s) (years) 100

Return Period(s) (years) Climate Change (%)

30

	US/MH			Return	Climate	First	(X)	First	(Y)	First (Z) Overflow
PN Name		Storm		Period	Change	Surcharge		Flood		Overflow	Act.
1.000	1	360	Winter	100	+30%	100/60	Winter	100/180	Winter		
1.001	2	180	Winter	100	+30%	100/60	Winter				
1.002	3	180	Winter	100	+30%	100/15	Summer				
1.003	4	240	Winter	100	+30%						
1.004	5	15	Summer	100	+30%						
2.000	6	15	Summer	100	+30%	100/15	Summer				
2.001	7	1440	Winter	100	+30%	100/480	Winter				
3.000	8	1440	Winter	100	+30%	100/480	Winter				
2.002	9	1440	Winter	100	+30%	100/480	Winter				
2.003	10	1440	Winter	100	+30%	100/480	Winter				
1.005	11	1440	Winter	100	+30%	100/480	Winter				
1.006	12	1440	Winter	100	+30%	100/15	Summer	100/960	Winter		
1.007	13	1440	Winter	100	+30%						
1.008	14	1440	Winter	100	+30%						
1.009	15	1440	Winter	100	+30%						
										+1	

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6 Killingbeck Court Killingbeck Drive Leeds LS14 6FD	Woodhead Road Surface Water	Micro Drainage	
Date July 2017 File P1244 Woodhead Road 29	Designed by TMD Checked by		
Micro Drainage	Network 2016.1		

Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow /	Overflow (1/s)	Pipe Flow (1/s)	Status	Level Exceeded
1.000	1	127.968	2.417	32.170	0.01		21.3	FLOOD	7
1.001	2	128.194	2.755	0.000	0.01		17.5	SURCHARGED	
1.002	3	128.201	4.056	0.000	0.04		8.0	SURCHARGED	
1.003	4	122.790	-0.269	0.000	0.02		8.0	OK	
1.004	5	120.598	-0.220	0.000	0.16		62.7	OK	
2.000	6	118.945	2.681	0.000	1.48		79.2	SURCHARGED	
2.001	7	113.648	1.000	0.000	0.00		5.4	SURCHARGED	
3.000	8	113.648	0.985	0.000	0.00		2.1	SURCHARGED	
2.002	9	113.648	1.037	0.000	0.00		5.1	SURCHARGED	
2.003	10	113.648	1.061	0.000	0.00		4.4	SURCHARGED	
1.005	11	113.648	1.112	0.000	0.00		9.6	SURCHARGED	
1.006	12	113.648	3.136	60.069	0.15		5.9	FLOOD	6
1.007	13	107.184	-0.106	0.000	0.19		5.9	OK	
1.008	14	106.261	-0.079	0.000	0.46		5.9	OK	
1.009	15	106.029	-0.108	0.000	0.18		5.9	OK	

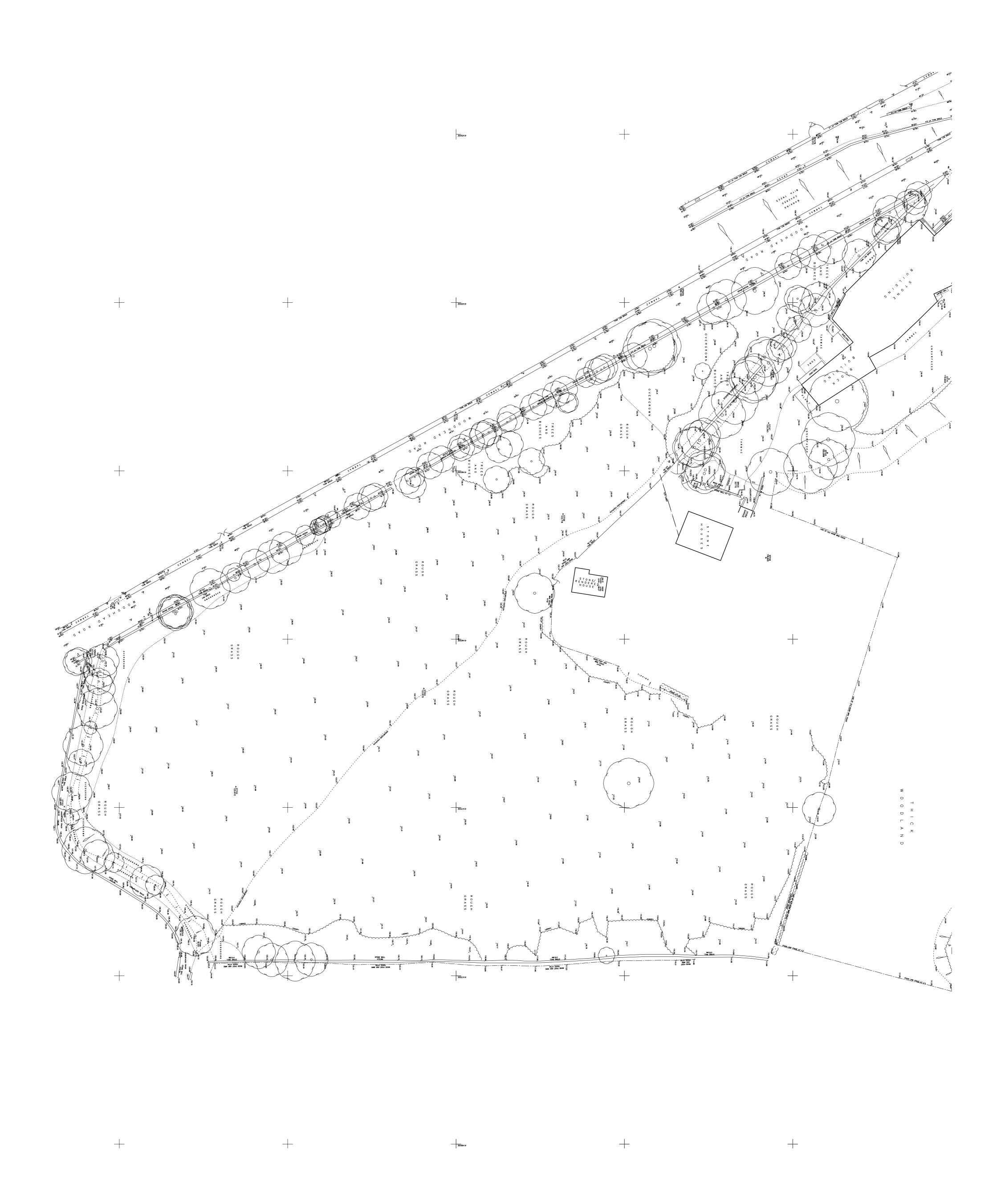
ADDITIONAL CELLULAR STOCKER
AN THE following LEG'S TO BE
PROVIDED

LEG 1.000 - 33M3

LEG 1.006 - 61M3



APPENDIX H Topographical Survey



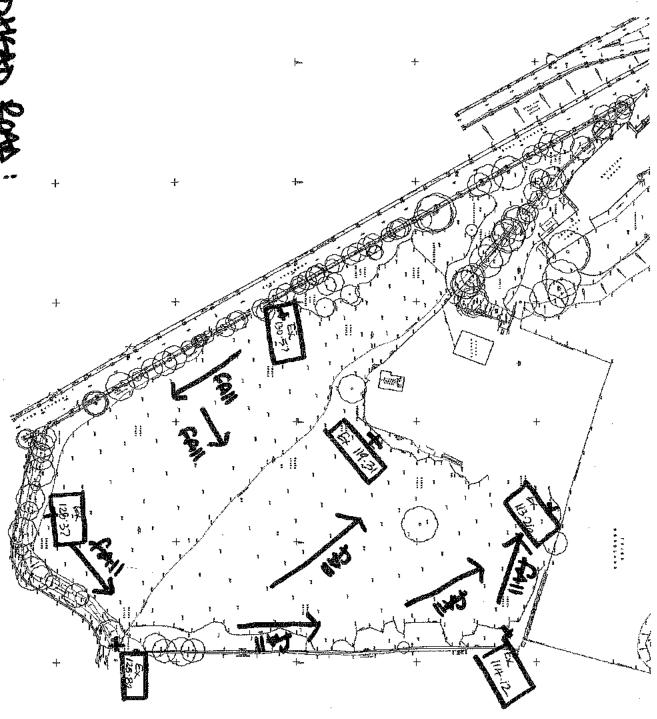


APPENDIX I

Flood Routing Plan and Existing Site Falls Plan

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